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STAGE 2

REMEDIAL INVESTIGATION

FOR THE FLIGHTLINE AREA

CARSWELL AFB, TEXAS

RADIAN CORPORATION 8501 MO-PAC BOULEVARD P. O. BOX 201088 AUSTIN, TEXAS 78720-1088

FEBRUARY 1991

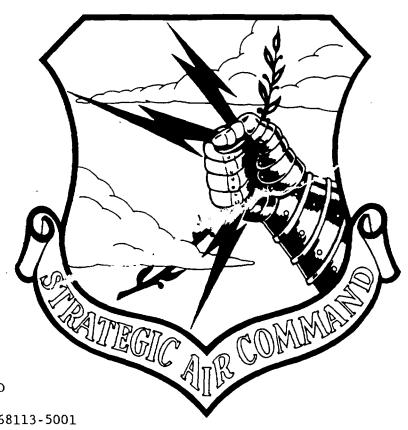
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PREPARED FOR

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REMEDIAL INVESTIGATION FOR THE FLIGHTLINE AREA

DRAFT REPORT
FOR
CARSWELL AIR FORCE BASE, TEXAS

HEADQUARTERS, AIR FORCE LOGISTICS COMMAND COMMAND SURGEON'S OFFICE (HQ/AFLC/SGPB)

FEBRUARY 1991

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EXECUTIVE SUMMARY

A Remedial Investigation (RI) was performed by Radian under the U.S. Air Force Installation Restoration Program (IRP) to characterize environmental contamination present in the Flightline Area of Carswell AFB, Texas; the existence of which was documented in preceding IRP studies. The affected environmental media include soil, surface water, and ground water present in the surficial alluvial aquifer (Upper Zone). The main contaminants are volatile organic compounds (principally trichloroethene (TCE)) associated with waste chlorinated solvents. The RI was conducted in stages from 1988 to 1991. Radian also performed the earlier IRP Phase II Stage 1 investigation (1986); the IRP Phase I Records Search was performed by CH2M Hill (1984).

The most recent field and analytical effort was conducted in 1990 to provide additional information necessary to support a Feasibility Study (FS) of remedial alternatives applicable to the Flightline Area. The 1990 effort was limited to further characterization of four of the Flightline Area IRP sites:

- Site LF04 Landfill 4;
- Site LF05 Landfill 5;
- Site WP07 Waste Burial Area; and
- Site FT09 Fire Department Training Area 2.

The locations of these, and other Flightline Area IRP sites that are addressed in separate project reports and documents, are shown in Figure ES-1.

Four major tasks were accomplished to address the existing data gaps:

 Drilling and logging of 29 soil borings to identify the distribution of paleochannel deposits, suspected as preferential pathways for migration of contaminants in Upper Zone ground water;

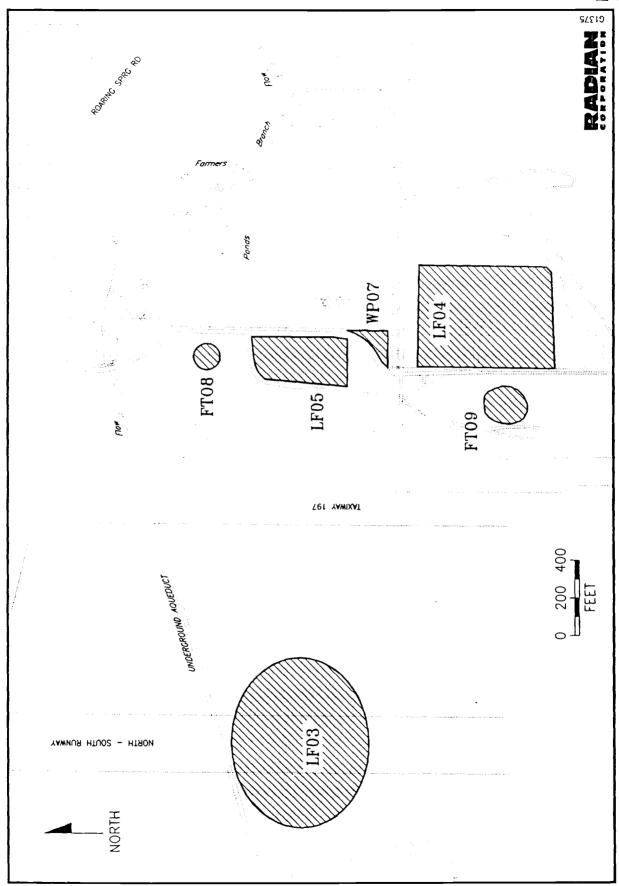


Figure ES-1. Location of Flightline Area Sites, Carswell AFB, Texas

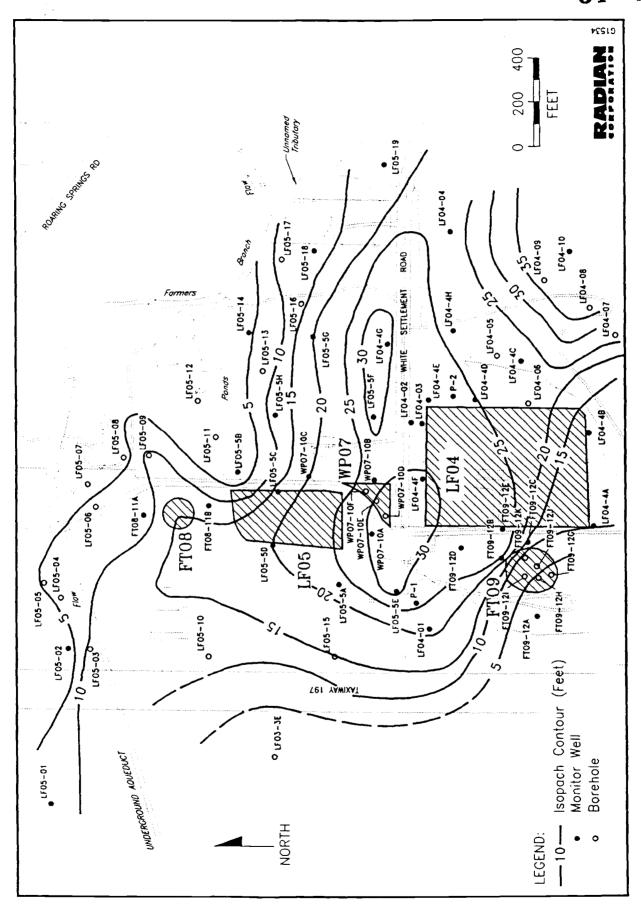
- Installation of 10 additional monitor wells, screened to the base of the Upper Zone Aquifer to provide additional information on the areal and vertical extent of ground-water contamination and possible existence of DNAPL;
- Ground-water and surface water sampling, analysis and static water level measurement; and
- Aquifer testing to determine Upper Zone hydraulic properties in the Flightline Area.

Based on all available data, ground-water contamination appears to be limited to the shallowest water-bearing zone, known as the Upper Zone Aquifer. In the Flightline Area, as well as across Carswell AFB and the adjoining area of Air Force (AF) Plant 4, the Upper Zone consists of unconsolidated Quaternary and Recent alluvial deposits (sand, gravel, silt and clay) that contain ground water under unconfined conditions. The Upper Zone deposits in the Flightline Area vary from approximately 5 to 49 feet thick, and are underlain by low permeability limestones and shales of the Cretaceous Goodland and Walnut Formations which form a basal aquiclude. Ground water in the Upper Zone Aquifer is encountered at depths ranging from approximately 4 to 30 feet below ground level (bgl) and ground-water flow in the Flightline Area is generally toward Farmers Branch. A series of hydrogeologic cross-sections through the Flightline Area was prepared from boring logs and synoptic water level measurements. They are included in Section 3 of this report to illustrate the local subsurface conditions.

The main surface water bodies located in the Flightline Area are Farmers Branch, an unnamed tributary that flows into Farmers Branch, and two small ponds on the base golf course. Farmers Branch eventually discharges to the Trinity River, which is located along the eastern boundary of Carswell AFB. The Upper Zone ground water and surface water bodies in the Flightline Area are hydraulically related, with ground water discharging to surface water.

Trichloroethene (TCE), vinyl chloride, tetrachloroethene (PCE), and the cis- and trans- isomers of 1,2-dichloroethene (1,2-DCE) are the main contaminants detected in the ground water and surface water in the Flightline Area. Based on the concentrations and distribution of these compounds in ground water, most recently determined in the 1990 sampling and analysis program, the four former waste disposal areas (Sites LF04, LF05, WP07, and FT09) appear to be sources for some of the ground-water contaminants detected downgradient of the sites. However, all of these compounds were also detected in samples from monitor wells located hydraulically upgradient of all Carswell AFB IRP sites in the Flightline Area, indicating that additional off-base sources must also be contributing to the existing Upper Zone ground-water contamination. The occurrence of volatile organic contaminants in the Upper Zone ground water on the AF Plant 4 property, upgradient of the Flightline Area, has been documented (Hargis and Associates, 1989). The source(s) of the contamination on AF Plant 4 have thus far not been identified. However, it is likely that they are also the source(s) for the contamination detected in the upgradient Flightline Area wells, and are contributing some component to the contaminant plumes that exist downgradient of the Flightline Area IRP sites.

In conjunction with lithologic logs obtained in previous drilling efforts, logs from the new soil borings were used to delineate the thick accumulations of sand and gravel deposited in paleochannels eroded into the surface of the underlying bedrock. Figure ES-2 is the resulting sand and gravel isopach map of the Flightline Area. The areas of thickest sediment correspond well with the highest concentrations of TCE determined in 1988, suggesting that TCE (and other ground-water contaminants) may be preferentially migrating along these relatively permeable deposits in the Upper Zone. The locations of existing Carswell AFB monitor wells and wells installed in the Flightline Area by Hargis and Associates for AF Plant 4 were reviewed to determine the optimum locations for the new wells installed in 1990. Locations were selected to assess the preferential pathway hypothesis, as well as to better determine the areal extent of contamination, and the



Sand and Gravel Isopach Map, Flightline Area, Carswell AFB, Texas Figure ES-2.

degree of continuity of the on-site contaminant plume with documented ground-water contamination present upgradient on the adjacent AF Plant 4 property. The latter objective could not be achieved because no AF Plant 4 wells were sampled concurrently with the Carswell AFB Flightline Area wells.

The monitor wells installed in 1990 were completed to intercept the base of the Upper Zone Aquifer to determine if dense non-aqueous phase liquid contaminant (DNAPL) is present in the Flightline Area. None was detected.

The results of the 1990 sampling and analytical effort confirmed that migration of the volatile organic contaminant plumes in the Upper Zone ground water does occur preferentially within the eroded bedrock paleochannels. A secondary component of movement is in the direction of ground-water flow, generally toward Farmers Branch. The maximum downgradient limit of vinyl chloride contamination was defined by the existing well network, which was also adequate to identify multiple sporadic occurrences of PCE. However, the areal extent of TCE and total 1,2-DCE in ground water was not determined. Samples from monitor wells located along the downgradient limit of the well network contained concentrations from 1300 to 2700 ug/L, and 280 to 540 ug/L, respectively.

In contrast to findings and interpretations from previous investigations, the ground-water and surface water analytical results for samples collected in 1990 provide little evidence of a metals contamination problem. No metals were detected in concentrations above MCLs in any samples analyzed for dissolved metals and there is no apparent pattern to the few detected concentrations above MCLs in the total metals analyses. In previous sampling events, only the total metals fractions were analyzed.

A pumping well and observation well for evaluation of Upper Zone Aquifer properties were installed just north of the northeast corner of Landfill 4, near the axis of a major paleochannel. The observation well was located approximately 50 feet north of the pumping well. Seven additional monitor wells were included in the observation well network, but the measured water levels showed no response to pumping after 20 hours of pumping at the

optimum rate determined in the preceding step test (approximately 20 gallons/minute). Data from the pumping test and subsequent recovery test were analyzed using the Cooper-Jacob method, and the computer Well Hydraulics Interpretation Program (WHIP^M). The resulting calculated aquifer properties of transmissivity, hydraulic conductivity, and storage coefficient are summarized in Table ES-1. The values all fall within the range expected for clean sands and gravels (Freeze and Cherry, 1979).

Upper Zone ground water in the Flightline Area was determined to discharge to surface water, based on synoptic water level measurements in the monitor wells and at a staff gauge in Farmers Branch. This interpretation is supported by the similarity in ground-water and surface water contaminant distributions and concentrations in samples collected in 1990. The chemistry of surface water in the unnamed tributary to Farmers Branch suggests the water is virtually equivalent to the ground-water plume composition at the sample collection point. Volatile organic contaminants, most notably TCE, in concentrations above MCLs were detected in samples collected from both the upgradient and farthest downgradient sampling points on Farmers Branch, suggesting contributions from off-base sources, as well as the potential for off-base migration of contaminants. Estimated concentrations of TCE and total 1,2-DCE leaving the Flightline Area via Farmers Branch are 45 ug/L and 8.4 ug/L, respectively.

A baseline risk assessment, incorporating the 1990 analytical results, was performed for the Flightline Area. Indicator chemicals, contaminant release, transport and fate mechanisms, and potential receptors and exposure pathways, specific to the Flightline Area were identified and evaluated. The Flightline Area was determined to pose no significant human health threat, based on evaluation of carcinogenic and noncarcinogenic (chronic) risks. Environmental (terrestrial wildlife and aquatic organisms) risks were determined to be minimal.

SUMMARY OF UPPER ZONE AQUIFER PUMPING TEST RESULTS, FLIGHTLINE AREA, CARSWELL AFB, TEXAS (JUNE, 1990) TABLE ES-1.

Well Number	Type of Test Analyses	Distance From Pumping Well (ft)	Transmissivity	Hydraulic Conductivity	Storage Coefficient (Dimensionless)
LF04-02	Drawdown	50	9771 ft²/day	835 ft/day (2.9 x 10 ⁻¹ cm/sec)	1.2 x 10 ⁻²
	Recovery	50	8260 ft²/day	705 ft/day (2.5 x 10 ⁻¹ cm/sec)	
LF04-03	Recovery	Pumping Well	9501 ft²/day	812 ft/day $(2.9 \times 10^{-1} \text{ cm/sec})$	
		Average Values	9177 ft²/day	784 ft/day (2.8 x 10 ⁻¹ cm/sec)	1.2 × 10 ⁻²

Using all available information generated in the IRP, the Flightline Area (combined Sites LF04, LF05, WP07 and FT09) was evaluated using the
Defense Priority Model (DPM). The Flightline Area received a total score of
19,381 and ranked second among the five Carswell AFB IRP sites/areas evaluated
with the model. While the Flightline Area contamination poses no immediate
human health threat, remedial action is indicated to prevent continuing
contaminant release and migration. Recommendations for addressing remaining
data needs for design and implementation of a remedial action are provided in
Section 7. It is anticipated that all of the required data can be obtained
within the detailed design phase of the selected remedial action, and no
additional separate remedial investigation effort is proposed.

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1.0 INTRODUCTION

1.1 Purpose of Study

The purpose of this study is to provide a sufficiently detailed description of existing environmental conditions in the Flightline Area (Sites LF04, LF05, WP07, and FT09) of Carswell AFB, Texas such that the impacts of documented ground-water contamination beneath the base can be determined and a remedial action can be designed and implemented.

Previous IRP studies documented soil and ground-water contamination, especially with trichloroethene (TCE) and chromium (Cr), in the Flightline Area. Previous investigations detected contamination of soils and ground water only in the "Upper Zone," a term used to describe the surface deposits of alluvium and fill in the Flightline Area (Hargis and Montgomery, Inc., 1983). However, the complete areal and vertical extent of the contaminant plume(s) were not defined.

Previously available evidence suggested multiple sources of the contamination, including source(s) located upgradient of all potential sources in the Flightline Area of the base. The monitoring network existing at that time was insufficient to identify and determine the relative contributions from these other sources. This report, based on additional IRP RI/FS Stage 2 field and analytical efforts performed between 5 March and 22 June 1990, addresses these data gaps and presents a summary of the current understanding of the hydrogeologic setting and Upper Zone ground-water characteristics of the Flightline Area.

Four major field tasks were designed to address existing data gaps. Soil borings were drilled and sampled to better define the distribution of basal gravels deposited in ancient river channels (paleochannels) which might serve as preferential pathways for contaminant migration. Monitor wells were installed to provide additional sampling sites to better characterize the vertical and lateral extent of ground-water contamination and potential or existing contamination sources. A comprehensive sampling of all Upper Zone

wells and numerous surface water sites was conducted to determine the nature and extent of contamination present. Finally, aquifer testing was performed to define the hydraulic conditions in the Flightline Area to aid in a more accurate characterization of contaminant transport.

1.2 <u>Site</u> Description

Carswell AFB is located six miles west of the center of Fort Worth in Tarrant County, Texas (Figure 1-1). The focus of this investigation is on an area near the southern end of the flightline at Carswell AFB, hence the name "Flightline Area" is used to describe the location of the study area.

The Flightline Area includes six discrete sites that were identified as potential sources of contaminants in previous IRP studies (Figure 1-2). They are:

- LF03 Landfill 3;
- LF04 Landfill 4:
- LF05 Landfill 5;
- WPO7 Waste Burial Area;
- FT08 Fire Department Training Area 1; and
- FT09 Fire Department Training Area 2.

Data obtained in the earlier IRP investigations provided no evidence that Sites LFO3 and FTO8 have released hazardous waste or waste constituents to the environment. Therefore, it was concluded that they do not pose an environmental or human health risk (Radian, 1989; 1990a,b). The monitor wells installed at Site FTO8 were, however, included in this most recent Stage 2 ground-water sampling effort because it is likely that they are intercepting ground water that has been contaminated by one or more upgradient, potentially off-base sources. In the following subsections, Sites LFO4, LFO5, WPO7 and FTO9 are described in terms of their physical features, historical uses, and the significant hydrogeologic findings from previous investigations performed in the Flightline Area. Historical descriptions of

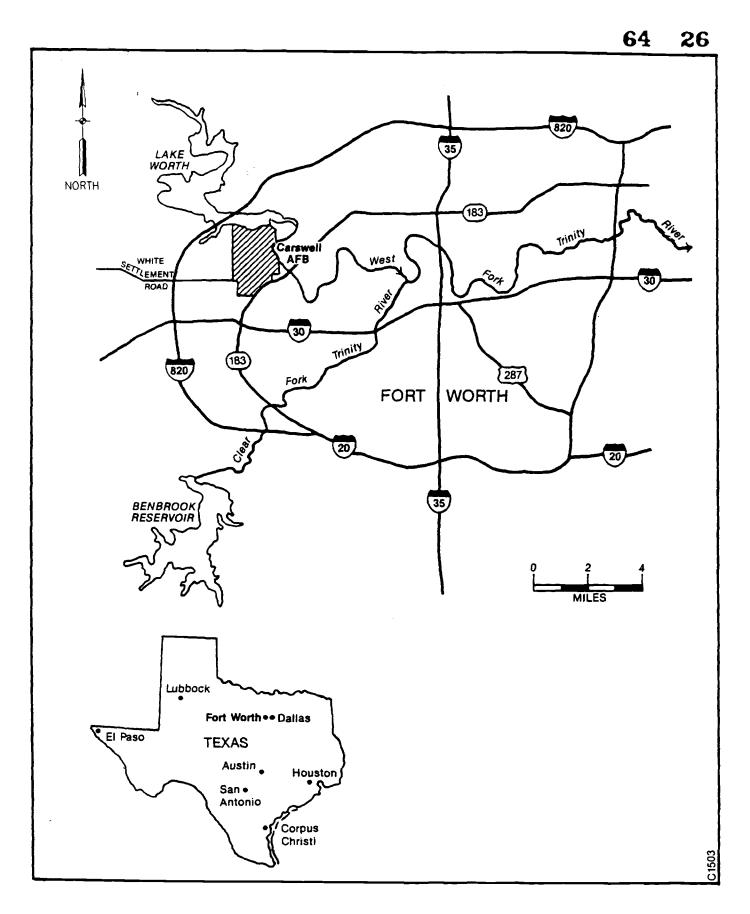


Figure 1-1. Regional Setting of Carswell AFB, Texas

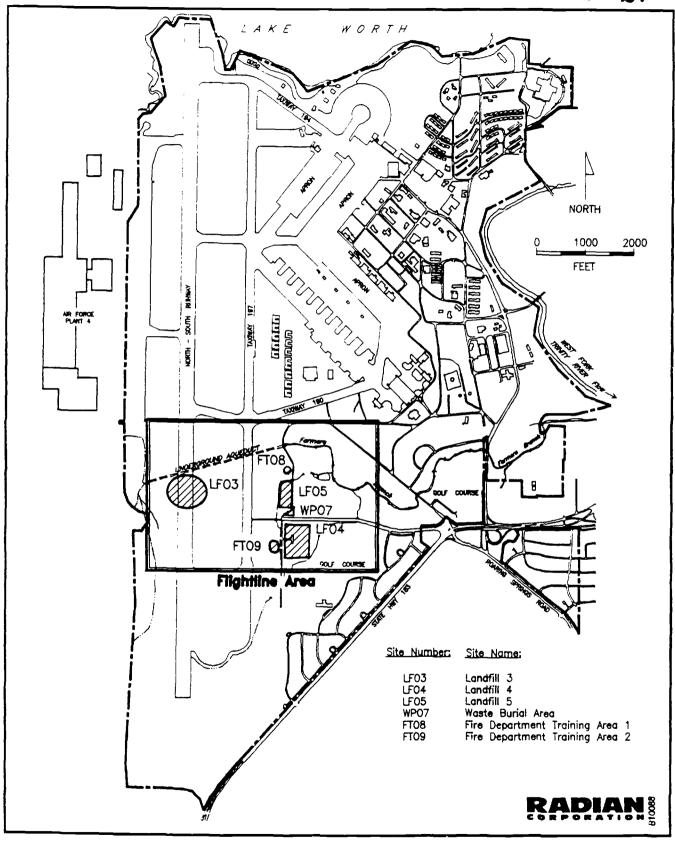


Figure 1-2. Location of Six Sites Included in the Flightline Area, Carswell AFB, Texas

these sites and the wastes disposed of in each are taken from the Phase I Records Search (CH2M Hill, 1984).

1.2.1 Site LF04 - Landfill 4

Landfill 4 includes approximately 10 acres of land located east of the south end of Taxiway 197. It was the main landfill during much of the history of Carswell AFB. While in active use, at least six large pits, approximately 12 feet deep, were filled with refuse which was burned and buried. Various potentially hazardous wastes were reported disposed of at this site, including drums of waste liquids, partially full paint cans, and cadmium batteries.

1.2.2 <u>Site LFO5 - Landfill 5</u>

Landfill 5 is located northwest of Landfill 4, adjacent to a small tributary to Farmers Branch. The landfill was constructed by building a clay berm along the creek and filling the area behind the berm up to the existing level. The landfill received all types of flightline wastes and refuse. Flightline wastes typically include such substances as oils, thinners, strippers, and paints. Waste materials in the landfill were burned regularly and buried.

1.2.3 <u>Site WPO7 - Waste Burial Area</u>

Site WPO7 is located adjacent to and north of White Settlement Road where it comes to a dead end at the taxiway. The area was used for burial of wastes during the 1960s. Various types of hazardous wastes, including drums of cleaning solvents, leaded sludge, and possibly ordnance were reportedly disposed of at this site.

1.2.4 Site FT09 - Fire Department Training Area 2

Site FT09 is located between Taxiway 197 and the radar facility. This site, with only slight modifications, has been used for fire department

training exercises since 1963. The fire pit is lined with gravel and is enclosed by a low earthen berm. In the past, a second pit was present at the site to collect run-off from the training exercises, but it no longer exists.

1.3 Summary of Previous Flightline Area Investigations

The Flightline Area has been the subject of field investigations performed during two separate Stages of the IRP Phase II; the Stage 1 Preliminary Assessment (PA) and Stage 2 Site Inspection (SI). The Phase II Stage 1 investigation (Radian, 1986) documented contamination of shallow ground water and soils in the Flightline Area. The initial Phase II Stage 2 investigative activities helped define contaminants in the Flightline Area, both qualitatively and quantitatively. Radian conducted a second episode of field activities during the Phase II Stage 2 investigation (Radian, 1990c) to fill data gaps remaining after the initial Phase II Stage 2 effort (Radian, 1989). Most notably, further characterization efforts included:

- Source definition;
- Determination of surface water ground water relationships;
- Definition of vertical and lateral extent of contamination;
 and
- Estimation of Upper Zone Aquifer hydraulic properties.

With information obtained from the additional Phase II Stage 2 activities, more complete characterization of contaminant source(s), surface water, geology, and ground water in the Flightline Area was achieved.

The following paragraphs summarize the activities performed throughout the Phase II IRP to characterize the contaminant sources and environmental media of concern in the Flightline Area at Carswell AFB. All field and analytical data from these investigations are contained in the various reports, including the Phase I investigation (CH2M Hill, 1984), the

Phase II Stage 1 investigation (Radian, 1986), and the previous Phase II Stage 2 investigation (Radian, 1989).

1.3.1 <u>Contaminant Source Characterization</u>

The following activities were performed to characterize the source(s) of contamination identified in the Flightline Area:

- Determining the locations of the IRP hazardous waste sites in the Flightline Area;
- Delineating the lateral and vertical extent of the waste areas; and
- Assessing the chemical and physical characteristics of wastes disposed of in the Flightline Area IRP sites.

These activities were accomplished by completing the following tasks:

- Reviewing the Phase I Records Search and personnel interviews;
- Performing geophysical surveys to accurately define the lateral and vertical extent of the former waste disposal areas;
 and
- Collecting environmental samples (soil, ground water, and surface water) to determine the types and amounts of contaminants associated with individual waste disposal units within the Flightline Area.

1.3.2 <u>Surface Water Characterization</u>

The major surface water features associated with the Flightline Area are:

- Farmers Branch;
- · An unnamed tributary that flows into Farmers Branch; and
- Two ponds located on the Carswell AFB golf course.

The following tasks were performed to characterize these surface water features:

- Chemical analysis of surface water samples collected from Farmers Branch, the unnamed tributary to Farmers Branch, and the two ponds located on the golf course;
- Estimating flow volumes at several locations on Farmers Branch and the small tributary; and
- Installing and surveying a staff gage in Farmers Branch to help determine ground-water/surface water relationships in the Flightline Area.

1.3.3 Geologic Characterization

The objectives of the geologic characterization activities performed in the Flightline Area were to:

- Determine the location of paleochannel(s) to assist in placement of Upper Zone monitor wells;
- Determine the depth to the shallow aquitard (Goodland/Walnut Formation) in the Flightline Area;
- Identify the thickness of the shallow aquitard under the Flightline Area; and
- Determine the depth to the uppermost regional potable water supply aquifer (Paluxy Aquifer) beneath the study area.

Radian accomplished these activities by completing the following tasks:

- · Borehole drilling, sampling, and lithologic logging; and
- Performance of geophysical surveys.

1.3.4 Ground-Water Characterization

Investigations of the ground water occurring under the Flightline Area were limited to the Upper Zone and the Paluxy Aquifers. Previous investigations focused on these two aquifers because deeper aquifers are unlikely to be affected by downward migrating contaminants. This is due to the several hundred-foot thick section of low permeability Glen Rose Limestone that acts as a basal aquitard to the Paluxy Aquifer in this area. Activities were focused on defining ground-water quality, both upgradient and downgradient of former waste disposal units in the Flightline Area, and on estimating aquifer properties. Characterization efforts were directed toward:

- Determining the physical and hydraulic properties of the aquifers;
- Identifying and quantifying the concentrations of contaminants in ground water from the Upper Zone and Paluxy Aquifer; and
- Delineating the lateral and vertical extent of ground-water contamination.

Radian performed the following tasks to characterize ground-water conditions in the Flightline Area:

- Test well installation in both the Upper Zone and Paluxy Aquifers;
- Sampling and describing the sediments that contain the ground water;

- Synoptic water-level surveys and potentiometric surface contouring;
- Performing in situ permeability tests (slug tests) and a pump test of the Upper Zone Aquifer;
- Ground-water sampling and analysis for waste-specific indicator parameters; and
- Mapping of ground-water contamination in the Flightline Area.

1.3.5 <u>Findings of Previous Flightline Area Investigations</u>

Geology

Based on the results of previous investigations (CH2M Hill, 1984; Radian, 1986, 1989, 1990c), the Flightline Area of Carswell AFB is characterized by surficial alluvial deposits of gravel, sand, silt and clay which are unconformably underlain by limestone and shale bedrock of the Cretaceous Goodland and Walnut Formations. The alluvium includes flood-plain and fluviatile terrace deposits which together constitute the Upper Zone, as defined by Hargis and Montgomery, Inc., 1983.

The base of the Upper Zone sediments was encountered during drilling activities performed in both RI/FS Phase II Stage 1 and Stage 2. In the Flightline Area, the Upper Zone varies from approximately 13 feet to greater than 40 feet thick. In general, silt and clay, with variable amounts of sand and gravel, dominate the upper five to 10 feet of the section. Below this depth, sand and gravel occur in increasing proportions, and in general, tend to increase in grain size with depth. Basal gravel deposits also occur in paleochannel features eroded into the surface of the underlying bedrock. The gravel consists mainly of limestone and shell fragments that range in size from fine gravel to cobbles.

The bedrock was penetrated during drilling of the Paluxy Aquifer monitor wells in the Stage 2 study, and was encountered at the base of a number of the Upper Zone monitor wells installed in Stage 1 and Stage 2. Bedrock in the Flightline Area consists of interbedded fossiliferous limestone and calcareous shale of the Goodland and the Walnut Formations. These units are generally dry, although small amounts of water were occasionally observed in the shale and clay units during drilling activities.

The bedrock surface is level across most of the Flightline Area east of Taxiway 197, but rises sharply near the southwest part of Site FT09 and the southern part of Site LF04, in the vicinity of the outcrop south of the study area. The locally irregular topography of the bedrock surface is typical of an erosional surface modified by fluvial processes.

Ground Water

Ground water occurs in the Upper Zone and in the Paluxy Aquifer beneath the Flightline Area. The potentiometric surface of ground water in the Upper Zone tends to mirror the configuration of the alluvium/bedrock contact. The position of the water table also reflects to a lesser degree the land surface topography. Downgradient is generally to the east toward a tributary of Farmers Branch, parallel to the surface slope. The hydraulic gradient is very low (on the order of 16 feet per mile) beneath most of the Flightline Area, except in the extreme southwestern area where it is notably steeper.

IRP Stage 1 ground-water analytical results revealed Upper Zone contamination by several volatile organic compounds, most notably TCE at concentrations ranging up to approximately 5000 micrograms per liter (μ g/L). Soil samples from the Flightline Area also contained detectable concentrations of TCE. Most of the detected contamination was apparently centered to the east of the Flightline Area at the golf course, but TCE concentrations up to nearly 3300 μ g/L were also detected in samples from wells located upgradient of Landfill 5, within 900 feet of the flightline. No contaminants were detected in the Paluxy Aquifer monitor wells.

During the Stage 2 effort, flightline monitor wells were sampled in January-February, and again in April, 1988. The following analytes were detected in concentrations above their respective EPA Maximum Contaminant Levels (MCLs) in one or more samples: arsenic, barium, cadmium, chromium, lead, selenium; and trichloroethylene, vinyl chloride, and benzene. Of the metals detected in concentrations exceeding their MCLs, chromium was the most widespread. However, all metals analyses were performed on unfiltered groundwater samples, and therefore reflect total, rather than dissolved metals concentrations.

As determined in Stage 1, the dominant organic contaminant identified in Stage 2 Upper Zone ground-water samples was TCE. The extent of the TCE plume in the Flightline Area was not completely defined upgradient (west) or downgradient (north and east) of the flightline IRP sites. Based on the generally west-to-east shallow ground-water flow direction, the existence of TCE in samples from monitor wells located west of the IRP sites was interpreted as indicating one or more additional upgradient sources not related to the sites subject to ongoing investigation. Also, TCE contamination of Upper Zone ground water in the area east of Air Force Plant 4 (i.e., upgradient of the Carswell AFB Flightline Area) is documented (Hargis and Associates, 1989).

Additional Stage 2 activities in the Flightline Area were recommended to: 1) determine to what extent, if any, the TCE-contaminated Upper Zone ground water east of Plant 4 and that beneath the Flightline Area constitute a contiguous plume; 2) determine to what extent, if any, the IRP sites on Carswell AFB are contributing to the existing Upper Zone ground-water contamination; 3) define the maximum lateral, downgradient, and vertical extent of the contaminant plume on Carswell AFB; and 4) define the site-specific hydrogeological characteristics of the Upper Zone in the Flightline Area in sufficient detail to design and implement an appropriate remedial action.

1.4 Report Organization

Following this Introduction, the field activities performed to characterize the Flightline Area are described in Section 2. The techniques and methodologies used to accomplish the field program are presented in detail with respect to the contaminant source, surface water, geological, and ground-water investigations that were included in the comprehensive Phase II scope of work. Section 3 presents a detailed description of the physical environmental setting of the Flightline Area based on interpretation of data from the current investigation and from previous studies. The nature and extent of surface water and ground-water contamination, determined from the most recent round of sampling and analysis (May-June 1990) are discussed in Section 4, and Section 5 addresses contaminant fate and transport. Section 6 summarizes the baseline risk assessment methodology and results of the evaluation; and presents the Defense Priority Model (DPM) ranking of the Flightline Area. Section 7 summarizes the major findings of the RI and presents the conclusions regarding data limitations and recommendations for additional activities.

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2.0 FIELD TECHNIQUES AND ANALYTICAL METHODS

Several field techniques were used to obtain information on the environmental conditions of the Flightline Area. The following subsections describe the techniques for drilling and soil sampling (including analytical methods, holding times, and collection and preservation requirements), the methods for conducting geophysical surveys, the methods and specifications for well construction and development, the techniques for collecting water samples (including analytical methods, holding times, and collection and preservation requirements), aquifer test methods, and surveying requirements.

2.1 Drilling and Soil Sampling

Drilling at Carswell AFB was accomplished using a hollow-stem auger rig for the Upper Zone monitor wells and soil borings and a rotary drilling rig (using both mud and air) for the Paluxy monitor wells. These methods were selected based on site-specific conditions and data requirements; i.e., the anticipated depth of completion, the need for water-level observations during drilling, and the expected geologic conditions.

After each borehole was completed, the drilling rig, auger flights, and equipment were decontaminated with a high temperature, high pressure steam-sprayer using base potable water.

Cuttings suspected of being contaminated on the basis of visual evidence and organic vapor analyzer (OVA) or photoionization detector (HNu) readings were placed in steel 55-gallon drums. Selected samples of cuttings were collected and submitted for analysis of EP Toxicity.

The following paragraphs describe the drilling and soil sampling procedures.

2.1.1 Hollow-Stem Augering

A Mobile Drill B-61 or a CME-75 hollow-stem auger drilling rig was used to perform shallow soil borings and installation of the Upper Zone monitor wells. The hollow-stem auger method allows for recovery of relatively undisturbed subsurface soil cores, determination of subsurface lithologies and structures, and accurate identification of the position of the water table. The boreholes were drilled dry; no drilling fluids or additives were used. Samples of soil were collected with either a split-spoon sampler, a thin-wall sampler (Shelby tube), or a CME 5-foot continuous core sampler.

The soil samples were described in terms of lithology, moisture content and any evidence of contamination. Lithologic logs of boreholes drilled during the most recent field activities are provided in Appendix A. Photographs of selected soil cores showing lithologic characteristics were also taken.

Selected samples were shipped on ice to Radian's laboratory for chemical analysis. Analytical parameters for soil samples are listed in Table 2-1. No soil samples were collected for chemical analysis in the most recent Stage 2 effort.

2.1.2 Air and Mud Rotary Drilling

Air and mud rotary drilling was performed during the Phase II Stage 1 program (Radian, 1986) with a Gardner-Denver 1500 CD truck-mounted rig. A 6-inch bit was used to advance a pilot borehole through the Upper Zone alluvial material to a depth of at least five feet into the underlying Goodland Limestone. The borehole was then reamed to a diameter of 14 inches. In order to seal off different water bearing zones, a 10-inch diameter steel casing was installed to the full depth of the borehole and the annular space was grouted. Upon achieving a positive seal, the borehole was advanced using a 6-inch diameter bit to the final depth at the shale unit separating the upper and lower Paluxy Formation. Bentonite drilling fluid was used while

TABLE 2-1. SUMMARY OF RI/FS PHASE II SOIL SAMPLING AND ANALYSIS REQUIREMENTS, CARSWELL AFB, TEXAS

EPA 6010 M	Parameter	Detection Limit	Method Type ¹	Container Type, No. and Volume	Preservation and Storage Requirements	Sample Extraction Procedures	Maximum Holding Time (Preparation) ²	Maximum Holding Time (Analysis)
	Metals	0.2 - 90 μ9/9	ICP	250 mL glass bottle	Refrigerated at 4°C	Acid digestion (3050R)	N/S	6 months
EPA 7060 A	As	0.5 µ9/9	Furnace AA	250 mL glass bottle	Refrigerated at 4°C	Acid digestion (3050R)	S/N	6 months
EPA 7740 Se	Se Se	0.5 49/9	Furnace AA	250 mL glass bottle	Refrigerated at 4°C	Acid digestion (3050R)N/S	s/	6 months
EPA 7471 H	F.G.	0.5 49/9	Cold Vapor	250 mL glass bottle	Refrigerated at 4°C	Acid digestion (3050R)	N/A	28 days
EPA 7420 PI	g.	0.5 mg/g	AA (furnace)	250 mL glass bottle	Refrigerated at 4°C	Acid digestion (3050R)	N/S	6 months
EPA 413.2 0	Oil and Grease	10 µ9/9		250 mL glass bottle	Refrigerated at 4°C	Freon extraction by sonication (2550)	S/N	28 days
EPA 418.1 P	Petroleum Hydrocarbons	8/8# 05	IR	250 mL glass bottle	Refrigerated at 4°C	Sonication extraction (3550) with freon	S/N	28 days
EPA 8240 V	Volatile Organic Compounds	0.1 49/9	GC/MS	250 mL glass bottle	Refrigerated at 4°C	Purge and trap (5030)	14 days	14 days
EPA 8270 S	Semi-Volatile Organic Compounds	1 49/9	GC/NS	250 mL stainless steel sleeve or 250 mL glass bottle	Refrigerated at 4°C	Sonication (3550)	14 days	40 days
EPA 8150 CI	Chlorinated Phenoxy Herbicides	0.1 - 160 µg/g	GC/EC0	250 mL glass bottle	Refrigerated at 4°C	Extraction, hydrolysis, GC	7 days	40 days
EPA 8080 O	Organochloride 0 Pesticides and PCB's	0.01 - 0.2 µg/g GC/ECD 3's	GC/ECD	250 mL glass bottle	Refrigerated at 4°C	Sonication extraction (3550)	7 days	40 days

Notes:

ICP = Inductively Coupled Plasma Emission Spectro
 AA = Atomic Absorption
 Infrared Spectroscopy
 GC/PID = Gas Chromatograph/Photoionization Detector
 GC/HSD = Gas Chromatograph/Halide Specific Detector
 A/A = Not Applicable
 N/S = Not Specified
 SM = Standard Method

TABLE 2-1. (Continued

Reference Method	Parameter	Method Detection Limit	Method Type ¹	Container Type, No. and Volume	Preservation and Storage E Requirements P	Sample Extraction Procedures	Maximum Holding Time (Preparation) ²	Maximum Holding Time (Analysis)
40 CFR 261.21 (EPA 1310)	EP Toxicity	0.002-0.5 mg/L AA,	AA, 1CP	250 mL glass bottle	Refrigerated Extraction at 4°C	Extraction	S/N	28 days
EPA 8140	Organophosphorus Pesticides	0.5 - 5 μ9/9	29	250 mL glass bottle	Refrigerated at 4°C	Sonication, extraction 7 days (2550) with freon	7 days	40 days
ASTM D2216	ASTM D2216 Soil Moisture							

Notes: 1. ICP = Inductively Coupled Plasma Emission Spectroscopy

AA = Atomic Absorption
IR = Infrared Spectroscopy
GC/PID = Gas Chromatograph/Photoionization Detector
GC/HSD = Gas Chromatograph/Photoionization Detector
CC/HSD = Gas Chromatograph/Halide Specific Detector
Z. N/A = Not Applicable
N/S = Not Specified
SM = Standard Method

drilling in the Paluxy Formation owing to borehole instability during air rotary operations.

As the borehole was advanced, the cuttings discharged at the surface were described by lithology, moisture content (air rotary-drilled section), evidence of contamination, and other features useful in characterizing the geologic section. Drilling conditions, such as relative rate and ease of penetration, were noted by the driller. Water encountered during drilling was noted with respect to depth of occurrence and rate of production. As needed, drilling was suspended temporarily to allow for recovery of water in the borehole.

2.2 <u>Geophysical Surveys</u>

Geophysical surveys were performed to define the vertical and lateral extent of waste-disposal activities, to provide a clearer picture of the subsurface conditions around the sites, and to investigate the potential existence of buried objects at several locations. Most geophysical tasks were performed during Phase II Stage 1; only a magnetometer survey of WPO7 (formerly Site 10) was performed during the initial Stage 2 investigation.

All survey grids were laid out using a compass and measuring chain. Stations were marked with labelled pin flags or spray paint. The geophysical techniques employed in the Flightline Area characterization efforts were earth resistivity, magnetic and magnetic gradient, and fixed frequency electromagnetic profiling (EMP) conductivity. The Earth Technology Corporation of Golden, Colorado performed the geophysical surveys in the Flightline Area. Following are brief descriptions of the various geophysical techniques used to characterize the Flightline Area.

2.2.1 <u>Electrical Resistivity</u>

Earth resistivity was measured by direct current Schlumberger soundings (vertical electrical soundings - VES) at all IRP sites in the Flightline Area. The Bison Model 2350 Earth Resistivity meter was utilized

for the VES measurements. Current electrode separations used were (in meters): 1, 2, 3, 4, 6, 10, 14, 20, 30, 40, and 50 (1 meter equals 3.28 feet). Due to variable ground conductivity, potential electrode separations varied slightly from site to site. The sounding data were processed using the ABEM VES iteration process to obtain a best fit curve and were plotted logarithmically as resistivity in ohm-meters versus half the current electrode separation in meters. The plot also includes the layered earth model giving the best match. At most VES sites, orthogonal electrode arrays were used to test for distortions of the data due to lateral inhomogeneities in the ground.

2.2.2 <u>Electromagnetic Surveys</u>

Electromagnetic profiling (EMP) surveys were conducted at Flight-line Area Sites LFO3, LFO4, LFO5, WPO7, FTO8, and FTO9 using two devices: the Geonics EM31 and the Geonics EM34-3 ground conductivity sensors. Both ground conductivity sensors are designed for rapidly obtaining data over large areas. The meters employ magnetic dipoles or magnetic induction loops for transmission and reception of low frequency electromagnetic waves. The effective depth of investigation of the EM31 is six meters; the depth of investigation provided by the EM34-3 depends on the coil separation and orientation, applied frequency, and to some extent, the conductivity profile of the subsurface. The techniques and conditions at Carswell AFB resulted in an effective investigation depth of 50 feet with the EM34-3. The resulting data are reported in units of millimhos/meter.

2.2.3 Magnetometer Surveys

Magnetometer surveys were accomplished using either an EDA PPM500 proton magnetometer or a Geometrics G856AX magnetometer. Magnetometer surveys were performed because the over-burden at Carswell has a low magnetic susceptibility; the buried objects were believed to contain a significant amount of iron that would create a noticeable magnetic anomaly. Readings of the total field and magnetic gradient were taken at each location. The units for these readings are gammas and gammas per one-half meter (1.64 feet), respectively. The magnetometer survey of WPO7 during Phase II Stage 2 activities was

performed to determine if metal objects were buried at any of the proposed drilling locations.

2.3 <u>Monitor Well Construction and Development</u>

During the Phase II activities in the Flightline Area, a total of 35 Upper Zone monitor wells and two Paluxy Aquifer monitor wells were installed. The construction specifications and well development procedures are described in the following sections. One aquifer (pump) test well and an observation well were also completed in the Upper Zone. The construction of these wells is described in Section 2.5 (Aquifer Pumping Test).

2.3.1 <u>Upper Zone Well Construction</u>

Upper Zone monitor wells were installed either immediately after completion of the drilling operations or after the borehole produced enough water to warrant a well. Construction specifications for the Upper Zone monitor wells are presented in Table 2-2. Well completion summaries for Flightline Area monitor wells completed in the most recent (1990) investigation are provided in Appendix B. Construction methods were generally consistent with the specifications provided in the SOW. Any changes necessitated by unanticipated field conditions were made with the knowledge and approval of the HSD/YAQ Technical Program Manager. Decisions regarding the setting of the screen and casing, length of screen, amount of sand pack and bentonite were made in the field by the Radian Supervising Geologist based on the static water level and saturated thickness of Upper Zone sediments. Monitor wells were installed using the following procedures:

1. Prior to installation, the casing and screen sections were thoroughly washed using a high temperature, high-pressure steam sprayer, with base potable water.

TABLE 2-2. UPPER ZONE MONITOR WELL CONSTRUCTION SPECIFICATIONS, FLIGHTLINE AREA, CARSWELL AFB, TEXAS

- 1. Casing: Two-inch diameter, threaded and flush jointed, Schedule 40 PVC.
- 2. Screen: Two-inch diameter, threaded and flush-jointed factory-slotted, Schedule 40 PVC, 0.020 inch slot. Normal screen length is 10 feet. Some well screens were wrapped with filter fabric material.
- 3. Sand/gravel pack: Washed and bagged, rounded sand/gravel with grain size compatible with screen slot and formation (Coarse, No. 8-20). A sand pack was placed from the bottom of the borehole to two to five feet above the top of the well screen. Sand was placed at a controlled rate to avoid bridging within the auger.
- 4. Bentonite seal: Two feet (minimum) of pelletized bentonite placed above the sand pack.
- 5. Grout: Type II Portland cement grout poured into the annular space from the top of the bentonite seal to land surface. A grout mixture consisting of approximately four pounds of bentonite to 94 pounds of cement was used. The grout was allowed to set for at least 24 hours before any well development activities.
- 6. Surface completion: PVC casing cut off to provide a 2- to 3-foot stickup with a solid cap placed on the casing. A 4- to 6-inch square steel well protector, four to five feet in length, was placed over the exposed PVC casing, and seated in the cement. A locking cap is incorporated in the well cover. Steel guard posts were installed as described in (8) below. The steel well protector and steel guard posts were painted for corrosion control and visibility.
- 7. Alternate flush completion: PVC casing cut off two to three inches below land surface, with a cast-iron valve box cemented in place. To prevent any surface water infiltration, the valve box is slightly elevated above land surface and the surrounding concrete is sloped away from the well. The lid to the valve box is secured with allen bolts. Most wells located on the heavy traffic areas of the Carswell AFB golf course were completed flush with the land surface.
- 8. Guard pipes or posts: Three 3-inch diameter steel posts, six feet in length, with a minimum of two feet below ground, installed radially four feet from the wellhead (not emplaced for flush surface completion).

- 2. Screen and casing sections were assembled, then lowered carefully into the borehole. As the string of screen and casing was lowered, additional sections of casing were added until the bottom of the screen reached the bottom of the borehole. The top of the casing was capped to prevent any completion materials (sand, bentonite pellets, and grout) from entering the casing during well construction activities. Where heaving or flowing sand was encountered, some well screens were wrapped in a filter fabric and installed using a natural, rather than artificial, sand pack. These wells were LF04-4F and -4H, and LF05-5F, -5G, and -5H.
- 3. Except as previously noted, clean sand (Coarse, No. 8-20) was poured carefully inside the annular space as the augers were slowly withdrawn from the borehole. The sand pack was regularly measured by the supervising geologist until the level of the sand was at least 2 feet above the top of the screen. Bentonite pellets were placed above the sand to form a 2-foot thick seal (minimum). If necessary, water bailed from the borehole was poured down the annular space to hydrate the bentonite.
- 4. Neat cement grout containing approximately four percent bentonite was either emplaced through the augers as they were withdrawn, or slowly poured down the borehole, if the formation was sufficiently consolidated to remain open.
- 5. After completion of grouting, the casing was cut two to three feet above land surface and a protective 4- to 6-inch diameter steel casing protector with a lockable lid was cemented into place. Three steel guard posts were then placed around the well. If above-ground stickups were of concern in an area, the well was completed flush with the land surface. For flush completions, the lid to the valve box was secured with allen bolts.

After all wells were completed, well locations and elevations were professionally surveyed. Table 2-3 presents the elevations of the ground surface, the wellhead, and the screened interval of the Upper Zone monitor wells in the Flightline Area.

2.3.2 Paluxy Formation Well Construction

After drilling operations were completed as described in Section 2.1, two Paluxy Aquifer monitor wells were installed as follows: Screen and casing, consisting of 5-inch diameter Schedule 80 PVC, were installed into the 10-inch diameter borehole. Screen length was 37.5 feet. Gravel pack material (Texas Blast Sand No. 1A) was placed in the annular space to a level of five feet above the top of the screen. Bentonite pellets were added to form a 2-foot thick seal, and the remaining annular space was sealed to the surface by the tremie method using bentonite-cement grout. After the grout was allowed to set for a minimum of 24 hours, the well was developed by bailing until a sediment-free discharge was produced. A 1/3 horsepower stainless steel submersible pump was installed after development. Protective casing, surface electrical connections, and a concrete well pad were placed after the pump was installed.

2.3.3 Well Development

After allowing the cement grout to set-up for a minimum of 24 hours, the Upper Zone wells were developed by either bailing using a bottomentry bailer or pumping with a Triloc® hand pump (1.7-inch diameter). As previously stated, Paluxy Aquifer monitor wells were developed by bailing.

Water levels in some of the Upper Zone wells recovered slowly and the wells were bailed dry several times. Other wells produced sufficient water and were developed in a single effort, without a recovery period. Development was considered complete when the water in the well was as sediment free as possible. The pH, temperature and conductivity of the development discharge water were measured and recorded at frequent intervals. The ground water removed from the wells was placed in steel 55-gallon drums, sealed and

(continued)				top of casing. .vel Surface	<pre>feasured from Mean Sea Le Below Land</pre>	Notes: 1. MSL MSL BLS
	603.1-593.3	17.0-26.7	620.0	622.69	NA	ļ
25.2	-594	15.0-24.7	619.3	21.	NA	
25.6	. 6-583	13.9-24.6	7.809	610.62	5н	2H
27.0	586.	5,3-2	612.0	615.39	56	LF05-5G
37.0	.4-583	23-36	619.4	618.95	5F	LF05-5F
39.1	.8-585	25.1-38.1	623.9	626.89	5E	LF05-5E
20.5	.0-589	10.5-19.5	608.5	611.71	2Ω	LF05-5D
22.0	.8-584	7-22	8.909	608.68	2C	LF05-5C
0.6	.4-588	6-7	597.4	600.45	5B	LF05-5B
32.0	-4.	18-28	619.4	623.18	5A	LF05-5A
49.5	7-577.	39.2-49.0	679	626.54	NA	LF04-10
25.2	594.2-584.5	15.2-24.9	7.609	612.07	NA	LF04-04
37.6	1-583.	22.4-36.7	620.5	623.25	NA	LF04-03
37.7	9-583	23.1-37.5	621.0	623.68	NA	LF04-02
40.1	5-586	30.0-39.7	626.5	629.24	NA	LF04-01
28.0	.5-583	14-27	610.5	613.43	Н7	LF04-4H
6.	1-58	22-35	619.1	620.02	97	LF04-4G
	588	21-34	622.8	625.36	4F	LF04-4F
	602.5-582.5	15-35	617.5	618.54	4E	LF04-4E
	1-585	18-28	613.1	615.35	40	LF04-4D
29.5	.4-582	18.5-28.5	610.9	613.04	27	LF04-4C
	605.4-595.4	13-23	618.4	619.90	4B	LF04-4B
24.0	.6-600	14-24	624.6	625.76	4 4	LF04-4A
15.4	613.1-607.2	8.5-14.4	621.6	625.25	3D	LF03-3D
(feet BLS)	(feet MSL)	(feet BLS)	(feet MSL)	(feet MSL)	Well Number	Number
Depth	Elevations	Interval	Elevation	Elevation	Monitor	Well
Total	Screen	Screened	Ground Level	Measuring Point	Previous	Monitor

TABLE 2-3. (Continued)

Monitor Previous Measuring Point ¹ Ground Level Screened Screen Total Well Monitor Elevation Elevation Interval Elevations Depth LF05-14 NA 602.98 603.2 5.1-13.0 598.1-590.2 13.3 LF05-18 NA 601.98 603.2 5.1-13.0 598.1-580.2 13.9 LF05-19 NA 606.08 606.3 10.3-20.0 598.1-588.5 23.95 LF05-19 NA 606.08 606.3 10.3-20.0 598.1-588.5 20.75 WP07-10A 10A 626.7 626.7 27-37 599.7-589.7 39.0 WP07-10B 10B 624.46 621.1 23-33 598.1-588.1 36.0 WP07-10B 10C 617.24 615.4 20-30 595.4-585.4 32.5 WP07-10B 11A 608.14 608.14 604.8 4-14 600.3-590.3 14.5 FT09-12A 12B 635.66 622.6 <			TABLE	TABLE 2-3. (Continued)			
NA 602.98 603.2 5.1-13.0 598.1-590.2 NA 611.84 612.1 13.9-23.7 598.2-588.5 NA 611.84 612.1 13.9-23.7 598.2-588.5 10A 626.7 626.7 27-37 599.7-589.7 10B 624.46 621.1 23-33 598.1-588.1 10C 617.24 615.4 20-30 595.4-585.4 11A 608.22 604.8 4-14 600.8-590.8 608.14 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 63.8 3.5-13.5 598.1-588.1 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.6 27.5-37.5 598.0-588.0 12D 627.48 624.5 24-27.5 600.5-597.0	lonitor Well umber	Previous Monitor Well Number	Measuring Point ¹ Elevation (feet MSL)	Ground Level Elevation (feet MSL)	Screened Interval (feet BLS)	Screen Elevations (feet MSL)	Total Depth (feet BLS)
NA 611.84 612.1 13.9-23.7 598.2-588.5 NA 606.08 606.3 10.3-20.0 596.1-586.3 10A 626.7 626.7 27-37 599.7-589.7 10B 624.46 621.1 23-33 598.1-588.1 10C 617.24 615.4 20-30 595.4-585.4 11A 608.22 604.8 4-14 600.8-590.8 608.14 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 625.6 27.5-37.5 598.1-588.1 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 624.8 21.4-34.4 603.4-590.4 12D 627.45 24-27.5 600.5-597.0	05-14	NA	602.98	603.2	5.1-13.0	598.1-590.2	13 3
NA 606.08 606.3 10.3-20.0 596.1-586.3 10A 626.7 27-37 599.7-589.7 10B 624.46 621.1 23-33 598.1-588.1 10B 624.46 621.1 20-30 595.4-588.1 10C 617.24 615.4 600.8-590.8 608.22 604.8 4-14 600.8-590.8 608.14 608.14 600.3-590.3 12A 635.66 632.0 13-23 619.0-609.0 627.55 625.6 27.5-37.5 598.1-588.1 12B 627.45 625.6 27.5-37.5 598.0-588.0 12D 628.05 625.5 27.5-37.5 598.0-588.0 12B 627.45 624.8 21.4-34.4 603.4-590.4 627.48 627.48 624.5 24-27.5 600.5-597.0	05-18	NA	611.84	612.1	13.9-23.7	598.2-588.5	23.95
10A 626.7 626.7 27-37 599.7-589.7 10B 624.46 621.1 23-33 598.1-588.1 10C 617.24 615.4 20-30 595.4-585.4 11A 608.22 604.8 4-14 600.8-590.8 11B 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 632.0 13-23 619.0-609.0 627.55 625.6 27.5-37.5 598.0-588.0 12B 627.45 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 24.5 24.27.5 600.5-597.0	05-19	NA	80'909	606.3	10.3-20.0	596.1-586.3	20.75
10B 624.46 621.1 23-33 598.1-588.1 10C 617.24 615.4 20-30 595.4-585.4 11A 608.22 604.8 4-14 600.8-590.8 11B 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 632.0 13-23 619.0-609.0 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0	07-10A	10A	626.7	626.7	27-37	599.7-589.7	39.0
10C 617.24 615.4 20-30 595.4-585.4 11A 608.22 604.8 4-14 600.8-590.8 11B 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 632.0 13-23 619.0-609.0 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0	07-10B	10B	624.46	621.1	23-33	598,1-588,1	36.0
11A 608.22 604.8 4-14 600.8-590.8 11B 608.14 603.8 3.5-13.5 600.3-590.8 12A 635.66 632.0 13-23 619.0-609.0 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 24-27.5 600.5-597.0	07 - 10C	10C	617.24	615.4	20-30	595.4-585.4	32.5
11B 608.14 603.8 3.5-13.5 600.3-590.3 12A 635.66 632.0 13-23 619.0-609.0 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0)8-11A	11A	608.22	604.8	4-14	600.8-590.8	14.5
12A 635.66 632.0 13-23 619.0-609.0 12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0	08-11B	118		603.8	3.5-13.5	600.3-590.3	15.0
12B 627.55 625.6 27.5-37.5 598.1-588.1 12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24.5 600.5-597.0	9-12A	12A	635.66	632.0	13-23	619.0-609.0	25.0
12C 628.05 625.5 27.5-37.5 598.0-588.0 12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0	J9-12B	12B	627.55	625.6	27.5-37.5	598.1-588.1	0.07
12D 627.45 624.8 21.4-34.4 603.4-590.4 12E 627.48 624.5 24-27.5 600.5-597.0	09-12C	12C	628.05	625.5	27.5-37.5	598.0-588.0	38.0
12E 627.48 624.5 24-27.5 600.5-597.0	09-12D	12D	627.45	624.8	21.4-34.4	603 4-590 4	35.0
)9-12E	12E	627.48		24-27.5	600,5-597.0	38.5

1. Measured from top of casing. MSL - Mean Sea Level BLS - Below Land Surface Notes:

appropriately labeled, based on field observations. Well development logs for the most recently installed (1990) monitor wells in the Flightline Area are provided in Appendix C.

2.4 Water Sampling

Both ground-water and surface water samples were collected from the Flightline Area. The following subsections describe the sampling techniques and methodologies for the various water samples collected during IRP Phase II investigations. Ground-Water and Surface Water Quality Sampling Records for the most recent round of Stage 2 sampling, including measurements of pH, conductivity, and temperature; and information such as volumes of water purged prior to sampling are provided in Appendix D.

2.4.1 Surface Water Sampling

Surface water grab samples were collected directly in the clean sample containers to minimize sample handling (and possible cross-contamination). The samples were collected approximately six inches below the water surface, or half-way between the water surface and the bed of the stream if the stream was not six inches deep. During the most recent (1990) field activities, surface water samples were collected at Farmers Branch, a small tributary that runs into Farmers Branch, and two ponds located on the Carswell AFB golf course. Additionally, during the most recent Stage 2 investigation (1990), estimates of flow volume were made at each surface water sample location at the time of collection.

Specific conductance, pH and temperature were measured on an aliquot of each sample. Specific conductance and pH were measured with a DSPH-1 meter and the temperature was taken with a mercury thermometer. Alkalinity measurements were made in the field using a Hach Alkalinity Test Kit (Model AL-DT) and digital titrator. Prior to obtaining the field measurements, the pH meter was calibrated with pH 4, 7, and 10 standard solutions and the conductivity meter was calibrated using either a 1413 or a 1504 umhos/cm KCl conductivity standard solution.

2.4.2 Ground-Water Sampling

Prior to sample collection, water levels were measured in each of the monitor wells with an Olympic Actat water level meter, and were recorded in a field notebook or on appropriate IRPIMS data collection forms. Measurements were taken from the surveyed mark point at the top of the casing, and read to the nearest 0.01-foot. Between measurements, the probe and associated electrical line were washed with laboratory grade detergent, rinsed with potable water, and then rinsed with deionized water to reduce the possibility of cross-contamination.

Before samples were collected, a minimum of three well volumes of water were bailed from the well using a bottom-entry Teflon™ bailer attached to a nylon monofilament line. This procedure ensured that representative formation water was collected. Purged water was placed in 55-gallon drums for final disposal pending the outcome of chemical analyses (provided to the Base Environmental Coordinator). Between wells, all equipment used for bailing operations was cleaned with laboratory grade detergent (Alconox), rinsed with potable water, ASTM Type II Reagent Water (or approved equivalent), pesticidegrade methanol, and finally pesticide-grade hexane. The equipment was allowed to air dry completely before reuse. The nylon line was replaced between wells.

Specific conductance, pH, temperature, and alkalinity were determined as described for surface water. On a few occasions, field measurements could not be made due to instrument malfunction.

After each well was purged of the required volume of water, ground-water samples were collected using a Teflon bailer. After collection, samples were placed directly into prelabeled sample bottles and preserved according to the requirements listed in Table 2-4. Ground-water samples for dissolved metals were filtered in the field. Samples were placed in ice chests with ice and were shipped for overnight delivery to Radian's laboratories in Sacramento, California, or Austin, Texas; or were hand delivered to the laboratory in

SUMMARY OF FLIGHTLINE AREA WATER SAMPLING AND ANALYSIS REQUIREMENTS, CARSWELL AFB, TEXAS TABLE 2-4.

EPA 120.1 Specific (Field Test) EPA 120.1 Specific (Field Test) Conductance (Field Test) EPA 170.1 Temperature (Field Test) EPA 200.7 Metals 0.00 EPA 270.3 Se 2 #5 EPA 270.3 Se 2 #6 EPA 270.3 Se 0.00	10 mg/L	Method Type	Container Type, No. and Volume	and Storage Requirements	Extraction Procedures	Holding Time (Preparation) ²	Holding Time (Analysis)
120.1 Specific Conductance (Field Test) 150.1 pH (Field Test) 170.1 Temperature (Field Test) 200.7 Metals 206.3 As 270.3 Se 245.1 Hg		Titration	(1) 1-Liter Polyethylene or Borosilicate glass bottle	Refrigerated at 4°C	None	N/S	Analyze immediately
150.1 pH (Field Test) 170.1 Temperature (Field Test) 200.7 Metals 206.3 As 270.3 Se 245.1 Hg	ري د	Wheatstone Bridge-type conductivity meter	None	None	None	N/A	Analyze immediately
170.1 Temperature (Field Test) 200.7 Metals 206.3 As 270.3 Se 245.1 Hg	S	Electrometric pH meter	None	None	None	N/A	Analyze immediately
200.7 Metals 206.3 As 270.3 Se 245.1 Hg 239.2 Pb	<	Thermometric	(1) 500 mL plastic bottle	None	None	N/A	Analyze immediately
206.3 As 270.3 Se 245.1 Hg 239.2 Pb	0.002-0.9 mg/L	d 1 1	(1) 500 mL polyethylene bottle	pH<2 w/HNO3	HNO ₃ /HCl digestion	N/S	6 months
270.3 Se 245.1 Hg 239.2 Pb	7/6# 5	AA (furnace)	(1) 500 mL	PH<2 W/HNO3	HNO ₃ digestion	S/N	6 months
g d	2 µg/L	AA (furnace)	Polyethylene	pH<2 W/HNO3	HNO ₃ digestion	S/N	6 months
Pb	0.2 µg/L	AA (vapor)	(1) 500 mL polyethylene bottle	PH<2 W/HNO3	KMnO4, HNO3, H ₂ SO ₄ digestion	N/S N/S	6 months 28 days
	0.005 µg/L	AA (furnace)	(1) 500 mL Polyethylene	4°C, pH < 2 W/HNO3	HNO ₃ digestion	S/N	6 months
EPA 413.2 Oil and Grease 0.2	0.2 µg/L	<u>«</u>	(1) 1000 mL glass bottle	pH<2 w/HCl refrigerated at 4°C	Freon extraction	N/S	28 days
EPA 418.1 Petroleum 1 m Hydrocarbons	1 mg/L	<u>π</u>	(1) 1-L glass bottle	4°C, pH<2 W/HCl	Freon extraction	S/N	28 days
EPA 160.1 Total Dissolved 10 Solids	10 mg/L	Gravimetric	(1) 1000 mL plastic bottle	Refrigerated at 4°C	N/A	None	14 days

A = Aranic Absorption

IR = Infrared Spectroscopy

GC/PID = Gas Chromatograph/Photoionization Detector

GC/HSD = Gas Chromatograph/Halide Specific Detector

Z. N/A = Not Applicable

N/S = Not Specified

SM = Standard Method

2-15

TABLE 2-4. (Continued)

Reference Method	Parameter	Method Detection Limit	Method Type ¹	Container Type, No. and Volume	Preservation and Storage Requirements	Sample Extraction Procedures	Maximum Holding Time (Preparation) ²	Maximum Holding Time (Analysis)
EPA 8020	Purgeable Aromatics	0.2-0.4 μg/L	GC/P10	(3) 40 mL VOA vial w/Teflon septa	pH<2, w/1:1 HCl, refrig- erated at 4°C	Nitrogen purge	N/S	14 days
EPA 601	Purgeable Halocarbons	0.02-5 µg/L	GC/HSD	(3) 40 mL VOA vial w/Teflon septa	Refrigerated at 4°C	Nitrogen purge	N/S	14 days
EPA 325.3	Chloride	1 mg/L	Titration	(1) 1-L Polyethylene	Refrigerated at 4°C	None	N/S	28 days
EPA 240.2	Fluoride	0.1 mg/L	Ion Selective Electrode	(1) 1-L Polyethylene	Refrigerated at 4°C	None	N/S	28 days
EPA 353.1	Nitrate	0.02 mg/L	Colorimetry	(1) 500 mL Polyethylene	4°C, pH<2 W/H2SO4	None	N/S	14 days
EPA 375.4	Sulfate	1 mg/L	Turbidimetry	(1) 1-L Polyethylene	Refrigerated at 4°C	None	N/S	28 days
EPA 365.1	0-Phosphate	0.02 mg/L	Colorimetry	(1) 500 mL Polyethylene	4°C, pH<2 W/H2SO4	None	N/S	28 days
EPA 604	Phenols	0.5 - 80 µg/L	၁၅	(2) 1-L glass bottle	Refrigerated at 4°C	Methylene chloride extraction	7 days	40 days
EPA 625	Priority Pollutants	50 µg/l	GC/MS	(2) 1000 mL glass; TFE- lined cap	Refrigerated at 4°C	Continuous extraction with methylene chloride	7 days	40 days
EPA 608	Organochloride Pesticides	0.05 - 1 µg/L	၁၅	(2) 1-L glass bottle	4°C pH 5 to 9	Methylene chloride extraction	7 days	40 days
SM509b	Chlorinated Phonoxy0.01 μg/L Acid Herbicides	ιγ0.01 μg/L	၁၅	1-L glass bottles 4°C w/TFE lined caps	4 °C	Hydrolyze, esterify	7days	40 days

Notes: 1. ICP = Inductively Coupled Plasma Emission Spectroscopy
As = Atomic Absorption
IR = Infrared Spectroscopy
GC/PID = Gas Chromatograph/Photoionization Detector
GC/HSD = Gas Chromatograph/Halide Specific Detector
Z. N/A = Not Applicable
N/S = Not Specified
SM = Standard Method

Austin. To ensure that sample integrity was maintained during shipping and handling, custody seals were affixed to each ice chest and chain-of-custody forms were completed and transmitted with the samples to each laboratory.

2.5 Aquifer Testing

Single-well in situ permeability aquifer tests (i.e., slug tests) and an aquifer pumping test were performed to determine the hydraulic properties of the Upper Zone Aquifer in the Flightline Area. Following is a discussion of the aquifer test methods.

2.5.1 Slug Tests

Slug tests were performed in 13 monitor wells (LF04-4A, -4B, -4D, -4E, -4G, LF05-5A, -5B, -5C, -5D, -5E, FT09-12A, -12B, and -12C) at the Flightline Area, and results were used to calculate the hydraulic conductivity of the Upper Zone Aquifer. The wells selected for slug testing represent a range of hydrogeologic conditions.

The slug test evaluates the response of water levels in a well when a "slug" (known volume) of water is instantaneously removed or added.

Typically, the response of the water level in a moderately permeable formation, such as the Upper Zone at Carswell AFB, is quite rapid. By determining the behavior of the water level in the well in response to the stress of the slug, the hydraulic conductivity of the aquifer material directly adjacent to the well screen can be calculated. To perform these calculations, the geometry of the well, aquifer boundary conditions, and initial water level must be known. The hydraulic conductivities were calculated using the method developed by Bouwer and Rice (1976).

The first step of the slug test was to measure the static water level in the well. Next, a known volume of water was removed by bailing and segregated for use as the slug. After the desired volume of water was removed from the well, a pressure transducer and attached cable were lowered into the well and suspended at a point just above the bottom of the well screen. The

pressure transducer was connected to an In-Situ, Inc. Hermit 1000B automatic data logger, capable of measuring and recording pressure changes on a logarithmic frequency, beginning every 0.2 seconds in the first few seconds of the test. Before introducing the slug, the water level in the well was allowed to return to static conditions. Then, as the slug was rapidly poured in the well, the data recorder was activated to measure the response of the water level. At least two slug tests were conducted at each well tested to determine the reproducibility of the results.

2.5.2 Aquifer Pumping Test

An aquifer pumping test was performed to evaluate the hydraulic characteristics of the Upper Zone deposits in the Flightline Area. One 6-inch diameter well (LF04-03) was installed during field activities performed under D.O. 4 Modification 0004 to accommodate the 4-inch submersible pump used in the test. The pumping well was constructed of Schedule 80 PVC (slot size 0.020 inches) and was screened over the entire saturated thickness of the Upper Zone. In order to measure the aquifer's response to pumping, a 2-inch diameter observation well (LF04-02) was also installed. The observation well was installed about 50 feet north of the pumping well and was also screened over the entire saturated thickness of the Upper Zone. All other construction details were the same as for the Upper Zone monitor wells.

Pumping tests usually provide the means to stress an aquifer to such a degree that reliable estimates of transmissivity, storativity, and hydraulic conductivity can be made. These values are calculated using drawdown and recovery data recorded in the pumping well and observation wells. Each of these calculated parameters can ultimately be used to estimate groundwater flow rates and contaminant plume migration.

Step Pumping Test

Prior to the start of the pumping test, a step test was performed to assess aquifer response at multiple incremental pumping rates to determine the optimum pumping rate for the aquifer test. The optimum pumping rate for

the Flightline Area pumping test was determined to be the full capacity of the submersible pump (Gould 1/2 HP, Model 10 EJ) or approximately 20 gallons-perminute (gpm). The pump was rated at approximately 25 gpm with the amount of hydraulic head encountered in the pumping well. However, travel of discharge water through over 300 feet of polyethylene pipe before ultimate discharge to the City of Fort Worth sewer system reduced discharge rates because of friction losses. Background water-level data in the pumping well and the near observation well were collected electronically (at 10 minute intervals) with a Hermit brand model SE1000B data logger for approximately 40 hours prior to the step test. The background data are useful for defining natural trends (i.e., variability) in the Upper Zone Aquifer water level, such as increases from recharge or decreases due to evapotranspiration. The background data can also be useful in preventing misinterpretation of a water level decline as being caused by pumping, rather than by natural factors.

Pumping Test

The pumping test was conducted on 21 and 22 June 1990, and ran for 20 hours. The pumping test began about 16 hours after the end of the step test, when the measured water levels had recovered to over 99 percent of their pre-step test levels. The 4-inch submersible pump (used in the pump and step test) was powered by a 3500 watt portable generator. Pump test discharge water underwent aeration before being discharged to the City of Fort Worth sewer system, with air for the aeration provided by a portable 125 cfm air compressor. During the step and pump tests, the pumping rate was determined by timing discharge into a 5-gallon container with a stopwatch. All required data from the aquifer test were recorded on IRPIMS Pump/Recovery Test Data Collection Forms, included in Appendix F.

Because drawdown is more rapid at the beginning of a pumping test, electronic recording of water levels (in the pumping well and nearest observation well) was in a logarithmic progression. Manual water level measurements of seven additional Upper Zone monitor wells were also made at more frequent intervals during the early stages of the test. During the test, pH, conductivity, temperature and the visual characteristics of the discharge

water were recorded at regular intervals. In addition, the pumping rate and drawdown of the pumping well were periodically checked to ensure consistency throughout the test, as wells will typically show a slow decline in discharge with time as drawdown increases.

Electronic data logging equipment was periodically downloaded by hand during the test. This allowed for construction of time-drawdown plots, or hydrographs, in the field for all wells being monitored during the test. These plots were used for preliminary determination of aquifer characteristics. Discharge water was pumped into a temporary holding tank to allow observation of water characteristics and recording of water quality data. Periodically during the pump test, water samples going into the holding tank (pre-aeration) and exiting the holding tank (post-aeration) were collected. These samples were collected in 40 mL VOA vials, filling each approximately two-thirds full with water. These water samples were allowed to sit in the direct sunlight for several hours prior to a headspace analysis for volatile organic content. During the time spent in the sunlight, volatile organics in the ground-water volatilized to the overlying air column. The volatile organic content of the headspace was measured with an HNu photoionization detector (PID). This was accomplished by cutting a small slit in the Teflon $^{ t w}$ septum in the cap of the vial and quickly inserting the probe of the HNu PID. Comparison of the pre-aeration and post-aeration volatile organic concentrations allowed for gross determination of the aeration system efficiency.

At the conclusion of the 20-hour ground-water pumping period, water level monitoring and observations continued during the recovery period. Recovery data were included on the hydrographs for each well. Data from the aquifer pumping test were used to calculate hydraulic parameters for the Upper Zone Aquifer.

A more complete description of the aquifer pumping test procedures and methods of analysis is provided in Appendix F.

2.6 <u>Surveying</u>

Land surveying activities were conducted by Brittain & Crawford, Inc., Registered Land Surveyors, of Fort Worth. These activities consisted of measurements of the horizontal location of wells, boreholes, hand-auger holes, and surface water sampling locations in terms of State Plane Coordinates; and of measurements of reference point elevations to an accuracy of \pm 0.01 foot. The survey was conducted to an accuracy needed for a second order survey. All of the data were provided as values posted on a map, and in tabular form (Appendix E).

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3.0 PHYSICAL CHARACTERISTICS OF THE FLIGHTLINE AREA

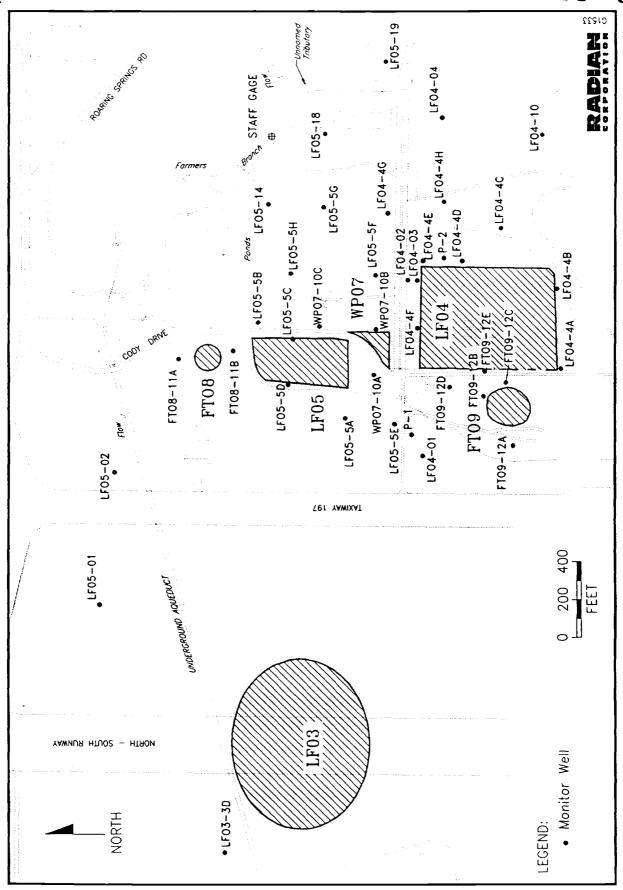
This section describes the physical characteristics of the Flight-line Area, with respect to local surface features, surface water bodies, geology, and ground-water occurrence. The primary basis of this characterization is interpretation of field and laboratory data obtained from the Installation Restoration Program (IRP) at Carswell AFB, Texas. Radian maintains a database containing all environmental data from the Flightline Area developed during the Phase II Stage 2 field program using the U.S. Air Force required Installation Restoration Program Information Management System (IRPIMS) format.

3.1 <u>Topographic Surface Features</u>

The area in the vicinity of the flightline ranges from an essentially level surface near the main (north-south) runway to gently rolling land near tributaries of Farmers Branch at the golf course. Figure 3-1 shows the location of the various surface features associated with the Flightline Area (buildings, roads, IRP sites, surface water bodies, etc.).

The Soils Conservation Service has identified four soil associations at Carswell AFB, however, only the Sanger-Purves-Slidell association occurs in the Flightline Area (USDA, 1981). The Sanger-Purves-Slidell soils range in thickness from 8-80 inches and are predominantly composed of clay loam. These are nearly level to gently sloping clayey soils with a permeability ranging from $<4.2 \times 10^{-5}$ to 3×10^{-4} cm/sec.

All of the land is underlain by terrace deposits of the Trinity River and fill material associated with the construction of the base runway and taxiways. The terrace deposits have been moderately dissected by tributaries of Farmers Branch. Elevations in the area range from approximately 625 feet mean sea level (MSL) at Landfill 3 (LFO3) to 580 feet MSL at the northern end of Landfill 5 (LFO5) and at Site 11 (FTO8).



Prominent Surface Features in Flightline Area, Carswell AFB, Texas Figure 3-1.

3.2 <u>Surface Water</u>

The main surface water bodies in the Flightline Area are Farmers Branch, an unnamed tributary that flows into Farmers Branch, and two ponds on the Carswell AFB golf course (Figure 3-1). Surface drainage in the Flightline Area is generally to the north and east toward Farmers Branch. During the Stage 2 investigation performed in 1990, water was present in tributaries to Farmers Branch at 1) the southwest side of Landfill 4 (LFO4), 2) the eastern side of Landfill 5 (LFO5) and Fire Department Training Area 2 (FTO9), and 3) the eastern edge of the Flightline Area (see unnamed tributary, Figure 3-1). Southwest of Landfill 4 (LFO4), the unnamed tributary flows over limestone and shale outcrop, but becomes an influent stream as water percolates into terrace (Upper Zone) deposits south and east of the landfill. The tributary west of Landfill 5 (LFO5) and Site 12 (FTO9) becomes effluent at Cody Drive where terrace deposits are relatively thin. Farmers Branch ultimately discharges to the Trinity River, located on the eastern boundary of Carswell AFB. The evaluation of ground-water flow at the Flightline Area suggests that the surface water bodies may receive ground-water inflow, and possibly contaminants associated with the ground water. A staff gage was installed in Farmers Branch (Figure 3-1) and professionally surveyed during the additional Stage 2 field activities. Synoptic ground-water and surface water-level measurements made in June 1990 were used to evaluate Upper Zone groundwater/surface water communication. A detailed discussion of this communication is provided in Section 4 (Nature and Extent of Contamination) of this report.

Estimates of flow volume in Farmers Branch and the unnamed tributary were made. Flow volumes were calculated by measuring the width and average depth of the stream(s), and then multiplying the resulting cross-sectional area by the estimated flow rate. The flow rate was estimated by measuring the length of time required for a floating object to travel a known distance. Estimated flow volumes at the time of sampling (April, 1990) were 6.0 cubic feet/second (cfs) for the four locations on Farmers Branch and 0.2 cfs for the unnamed tributary. Water in the two ponds appeared stagnant at the time of

sampling. Observed flow in Farmers Branch during field activities was extremely variable, ranging from <5 to >100 cfs (following heavy rains).

3.3 Geology

Carswell AFB is located on the relatively stable Texas craton, west of the faults that lie along the Ouachita Structural Belt. No major faults or fracture zones have been mapped near the base. The regional dip of the rocks beneath Carswell AFB is between 35 and 40 feet per mile in an easterly to southeasterly direction. From youngest to oldest, the major geologic formations found in the Flightline Area of Carswell AFB are as follows: 1) Quaternary Alluvium, 2) Cretaceous Goodland Limestone, 3) Cretaceous Walnut Formation, 4) Cretaceous Paluxy Formation, 5) Cretaceous Glen Rose Formation, and 6) Cretaceous Twin Mountains Formation.

Subsurface geologic conditions in the Flightline Area were characterized using indirect methods (geophysical surveys) and direct subsurface sampling and lithologic logging during drilling operations. Most of the IRP activities focused on the Upper Zone. The Goodland/Walnut Aquitard and the Paluxy Aquifer in the Flightline Area were the deepest (oldest) units penetrated, and by only two monitor wells installed during the initial Stage 2 effort. The following subsections contain discussions of the geology in the Flightline Area.

3.3.1 Quaternary Alluvium

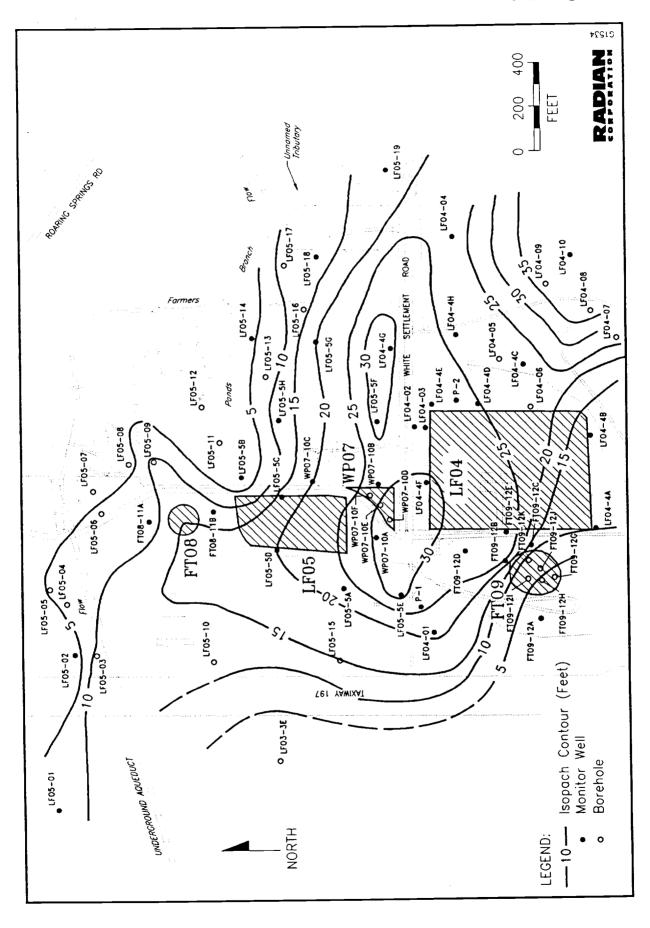
Quaternary alluvium, deposited by the Trinity River, is found at the surface throughout the Flightline Area site, as well as over most of the base. The alluvium consists of floodplain and fluviatile terrace deposits of gravel, sand, silt, and clay that occur as a veneer on the eroded surface of the Goodland Limestone. The unconsolidated alluvial deposits and fill are referred to as the "Upper Zone," a term initially applied to similar alluvial deposits at AF Plant 4 (Hargis and Montgomery, Inc., 1983). The Upper Zone is a hydrogeologic unit at Carswell AFB that is a mixture of clay, silt, sand, and gravel of variable thickness and degree of saturation.

Drilling on the base indicates that the alluvial deposits (and fill) range from a few feet to greater than 45 feet of interbedded clay, silt, sand, and gravel. The irregular thickness of the alluvium is due to depositional events, stream channeling, and erosion. In general, silt and clay with variable amounts of sand and gravel occur at the land surface down to depths of five to 10 feet. Underlying the silt and clay is a sand and gravel unit that normally increases in grain size with increasing depth. These strata appear to be relatively continuous across the area of investigation, although coarse gravel deposits occur in limited areas generally east of the Fire Department Training Areas 1 (FTO8) and 2 (FTO9). The sand deposits are fine-grained to coarse-grained, tan to rust in color, and composed predominantly of quartz grains. Gravel is mostly limestone and shell fragments ranging in size from fine gravel to cobbles. A sand and gravel isopach map of the Flightline Area is presented in Figure 3-2.

During the most recent drilling activities in the Flightline Area, efforts were made to characterize the paleochannels (old stream channel patterns) believed to exist in the area. Examination of Figure 3-2 shows thick sand and gravel sequences, indicative of channel deposits, to occur east of Taxiway 197 and roughly paralleling White Settlement Road. Sand and gravel thicknesses greater than 20 feet occur in an approximately 800 feet-wide area, with White Settlement Road serving as the approximate median to the pattern. Additional evidence of the channel pattern is seen in the eroded nature of the bedrock in this area and the extensive limestone gravels (scoured bedrock). The gravels were deposited as channel lag deposits on the scoured upper surface of the underlying bedrock (Goodland/Walnut Formations).

3.3.2 <u>Cretaceous Goodland Limestone and Walnut Formation</u>

Underlying the alluvium are the Cretaceous-age Goodland and Walnut Formations. Both formations consist of interbedded, fossiliferous, hard limestone and calcareous shale, and are thus discussed together. The rock is fractured and there is considerable jointing and flaking, which gives the limestone a fractured appearance. These strata are generally dry, although small amounts of water are occasionally present in the shale and clay units.



Sand and Gravel Isopach Map, Flightline Area, Carswell AFB, Texas Figure 3-2.

The erosional surface of the bedrock is generally level across most of the Carswell AFB area, with a pronounced rise in the southwest portion of the base corresponding to the outcrop of limestone and shale. Table 3-1 shows the depth (and corresponding elevation) to bedrock (Goodland/Walnut Formation) at all drilling locations in the Flightline Area. Figure 3-3 is a contour map of the elevation (MSL) of the top of the bedrock surface. The locally irregular topography of the top of the bedrock is characteristic of an erosional surface modified by fluvial processes, which is recorded by the overlying sequence of interbedded fluviatile gravel, sand, silt, and clay.

The thickness of the Goodland/Walnut Formations, as observed during the drilling of Paluxy wells P-1 and P-2 (Figure 3-1), is approximately 30-40 feet beneath the Flightline Area. However, because the top of the Goodland/Walnut Formations is an erosional surface, the thickness in isolated areas may be less than originally deposited. It has been reported that the Quaternary alluvium and the cretaceous Paluxy Formation are in direct contact at the eastern boundary of AF Plant 4, where the Goodland/Walnut Formations were completely eroded away (Hargis and Associates, 1985).

3.3.3 <u>Cretaceous Paluxy Formation</u>

Beneath the Goodland and Walnut Formations lies the Cretaceous-age Paluxy Formation, often referred to as the Paluxy Sand. The Paluxy Formation is the deepest unit penetrated in the Flightline Area during the IRP efforts. Regionally, the Paluxy Sand is divided into upper and lower sand members by an intervening shale unit. The sands in the upper part of the Paluxy are reported by drillers to be fine-grained and shaley. The lower sand member generally consists of two separate and distinct sand strata, but the individual sand beds do not maintain constant thickness or lithology over long distances. About one-half to three-fourths of the Paluxy is sand; the remainder consists of clay, sandy clay, shale, lignite, silicified wood fragments, and nodules of pyrite. In general, coarse-grained sand is in the lower part of the Paluxy which grades upward into fine-grained sand with variable amounts of shale and clay.

TABLE 3-1. ELEVATION OF BEDROCK IN FLIGHTLINE AREA, CARSWELL AFB, TEXAS

Location ID	Ground Level Elevation (Ft, MSL)	Depth to Bedrock (Ft)	Elevation of Bedrock (Ft, MSL)	Sand and Gravel Thickness (Ft)
 LF03-3A	633.47	18.0	615.5	0
LF03-3B	633.84	19.5	614.3	0
LF03-3C	635.39	12.0	623.4	0
LF03-3D	621.6	15.0	606.6	0
LF03-3E	622.87	16.0	606.9	0
LF04-4A	624.6	18.0	606.6	11.0
LF04-4B	618.4	17.5	600.9	10.0
LF04-4C	610.9	29.0	581.9	23.0
LF04-4D	613.1	29.0	584.1	25.0
LF04-4E	617.5	33.5	584.0	28.0
LF04-4F	622.8	>35.5	<587.3	>29.5
LF04-4G	619.1	39. 5	579.6	30.5
LF04-4H	610.5	27.0	583.5	23.0
LF04-01	626.5	40.0	586.5	20.7
LF04-02	621.0	37.0	584.0	26.0
LF04-03	620.5	37.5	583.0	25.4
LF04-04	609.4	25.0	584.4	23.5
LF04-05	608.8	25.8	583.0	17.0
LF04-06	613.3	29.5	583.8	24.1
LF04-07	630.4	38.2	592.2	28.4
LF04-08	630.0	47.0	583.0	38.9
LF04-09	627.4	47.0	580.4	37.4
LF04-10	626.9	49.0	577.9	36.3
LF05-5A	619.4	31.0	588.4	13.5
LF05-5B	597.4	8.0	589.4	3.0
LF05-5C	606.8	21.0	585.8	16.0
LF05-5D	608.5	24.0	584.5	20.0
LF05-5E	623.9	>40.0	<583.9	>31.0
LF05-5F	619.4	>37.0	<582.4	>33.0
LF05-5G	612.0	29.0	583.0	21.0
LF05-5H	608.4	25.0	583.4	11.0
LF05-01	619.3	25.0	594.3	6.9
LF05-02	620.0	27.0	593.0	2.1
LF05-03	620.6	27.4	593.2	12.2
LF05-04	617.3	28.0	589.3	5.3
LF05-05	616.1	26.0	590.1	6.0
LF05-06	598.3	7.0	591.3	6.5
LF05-07	598.0	5.8	592.2	4.0
LF05-08	606.8	14.5	592.3	2.5
LF05-09	604.9	14.0	590.9	10.5

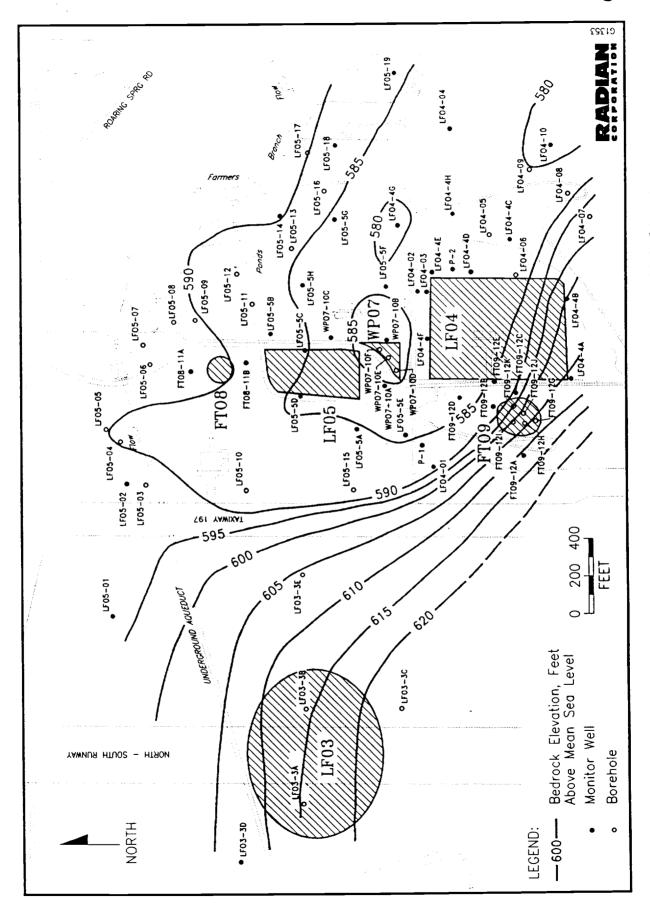
(continued)

TABLE 3-1. (Continued)

Location ID	Ground Level Elevation (Ft, MSL)	Depth to Bedrock (Ft)	Elevation of Bedrock (Ft, MSL)	Sand and Gravel Thickness (Ft)
LF05-10	623.9	36.0	587.9	12.0
LF05-11	597.6	10.0	587.6	3.0
LF05-12	594.4	9.0	585.4	0.5
LF05-13	605.0	17.0	588.0	7.7
LF05-14	603.2	13.0	590.2	4.8
LF05-15	626.5	40.5	586.0	15.0
LF05-16	612.3	23.0	589.3	14.0
LF05-17	606.5	16.5	590.0	12.0
LF05-18	612.1	23.2	588.9	12.2
LF05-19	606.3	20.5	585.8	17.7
WP07-10A	624.2	>39.0	<585.2	26.5
WP07-10B	621.1	33.0	588.1	27.0
WP07-10C	615.4	31.0	584.4	20.0
WP07-10D	623.3	>29.0	<594.3	>13.0
WP07-10E	622.5	>29.0	<593.5	>17.0
WP07-10F	621.5	>29.0	<592.5	>20.0
FT08-11A	604.8	13.5	591.3	9.5
FT08-11B	603.8	14.0	589.8	11.0
FT09-12A	632.0	18.0	614.0	7.0
FT09-12B	625.6	39.0	586.6	26.0
FT09-12C	625 .5	31.0	594.5	15.0
FT09-12D	624.8	>36.0	<588.8	>21.0
FT09-12E	624.5	39.0	585.5	26.0
FT09-12G	629.2			
FT09-12H	629.1	25.0	604.1	6.0
FT09-12I	629.2	24.0	605.2	5.0
FT09-12J	628.7	23.0	605.7	4.0
FT09-12K	626.7	>25.0	<601.7	>5.0

⁻⁻ Not Determined

MSL - Mean Sea Level



Contoured Elevation of Bedrock Surface in Flightline Area, Carswell AFB, Texas Figure 3-3.

In the two Paluxy monitor wells (P-1 and P-2) installed during the initial Stage 2 effort, drilling progressed through the upper sand member to the intervening shale unit. The upper sand member ranged from 30 to 35 feet in thickness and consisted of varying amounts of sand, sandstone, clay, and shale. The shale unit separating the upper and lower Paluxy "sands" was encountered at approximately 105 feet, below land surface in both P-1 and P-2.

3.3.4 <u>Cretaceous Glen Rose Formation</u>

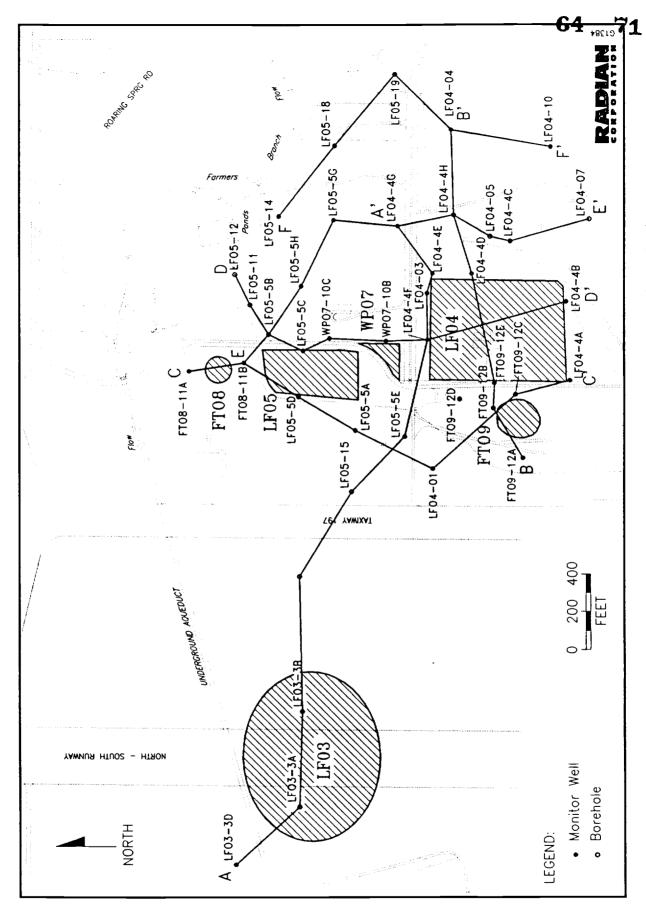
Underlying the Paluxy Sand is the Glen Rose Formation, which represents the seaward facies of part of the Twin Mountains Formation, being deposited simultaneously to the north. The Glen Rose was not penetrated during drilling in the Flightline Area, but typically consists primarily of calcareous sedimentary rocks (limestone) and some sands, clays, and anhydrite.

3.3.5 <u>Cretaceous Twin</u> Mountains Formation

The Twin Mountains Formation, with the Glen Rose Formation capping it, is the oldest Cretaceous-age formation reported in the vicinity of Carswell AFB. In ascending order, the Twin Mountains Formation is divided into the Sycamore Sand Member, the Cow Creek Limestone Member, and the Hensell Sand Member. The Twin Mountains Formation does not crop out in Tarrant County. The Twin Mountains Formation consists of a basal conglomerate of chert and quartz, grading upward into coarse- to fine-grained sand interspersed with varicolored shale.

3.3.6 Flightline Area Cross-Sections

Following the recent drilling activities at the Flightline Area, six geologic cross-sections were constructed, showing borehole lithologies (as well as the static water levels in the Upper Zone measured on 18 June 1990). A location map for the newly constructed cross-sections through the site is provided in Figure 3-4.



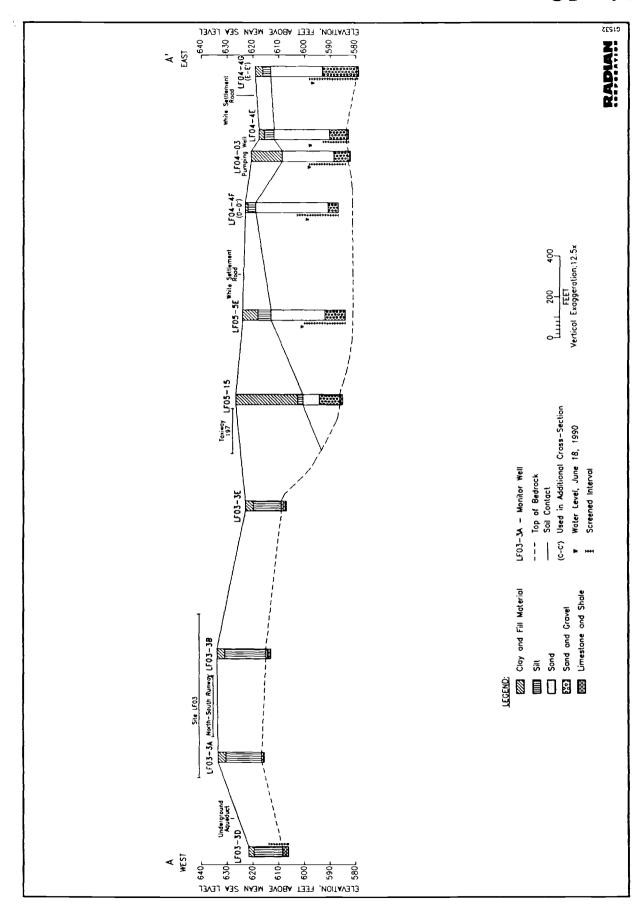
Location Map for Geologic Cross-Sections Through the Flightline Area, Carswell AFB, Texas Figure 3-4.

Two of the cross-sections (A-A' and B-B') are oriented roughly westeast and the remaining four are oriented roughly north-south (C-C' through F-F') through the site. All of the cross-sections intersect the relatively thick sand and gravel sequence observed at the site (Figure 3-2).

Cross-section A-A' (Figure 3-5) depicts the subsurface from the Landfill 3 (LFO3) area to the area just east of Landfills 4 (LFO4) and 5 (LFO5) and the Waste Burial Area (WPO7). An important feature in this crosssection is the lack of sand and gravel in the borings completed in the Landfill 3 area. There is a steep incline in the upper surface of the bedrock (Goodland/Walnut Formations) between borings LF03-3E and LF05-15. Coincident with the lower bedrock elevation in the vicinity of LFO5-15 is the appearance of relatively thick sands and gravels of the Upper Zone. This cross-section is oriented through the thickest sands and gravels encountered in the Flightline Area (Figure 3-2). Boring locations from LFO5-15 eastward all display a fining-upwards sequence in the Upper Zone deposits, which is consistent with alluvial deposition. The lower bedrock surface observed in the eastern half of the cross-section is probably the result of stream erosion, as rounded limestone and chert gravels (typical of channel lag deposits) rest directly on the bedrock surface. These deposits are believed to coincide with the location of a former channel (paleochannel) of what is now Farmers Branch.

In cross-section B-B' (Figure 3-6), another steep incline is observed in the bedrock topography between monitor well locations FT09-12A and FT09-12B. Paralleling the inclined bedrock surface is a steeply-dipping Upper Zone water table. Fining-upwards sequences are seen in all borings included in this cross-section, with gravels occurring on the eroded bedrock surface east of FT09-12A.

Shown in Figure 3-7 is cross-section C-C'. Gravels only occur in the middle area of the cross-section, with a relatively higher bedrock surface occurring in the northern and southern reaches of the section. The steeply inclined bedrock surface seen at location FTO9-12A (B-B') is also reflected



Geologic Cross-Section A-A', Flightline Area, Carswell AFB, Texas Figure 3-5.

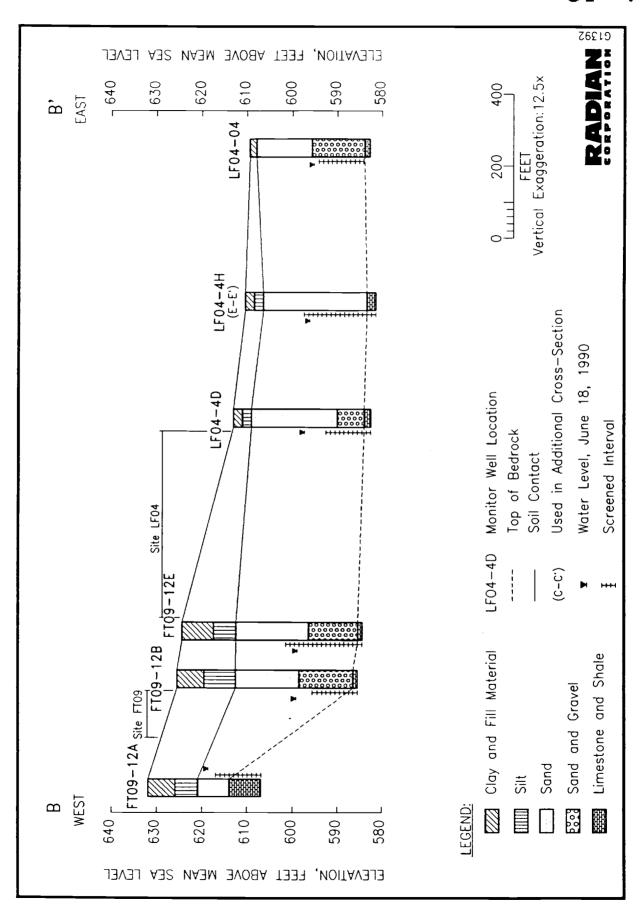


Figure 3-6. Geologic Cross-Section B-B', Flightline Area, Carswell AFB, Texas

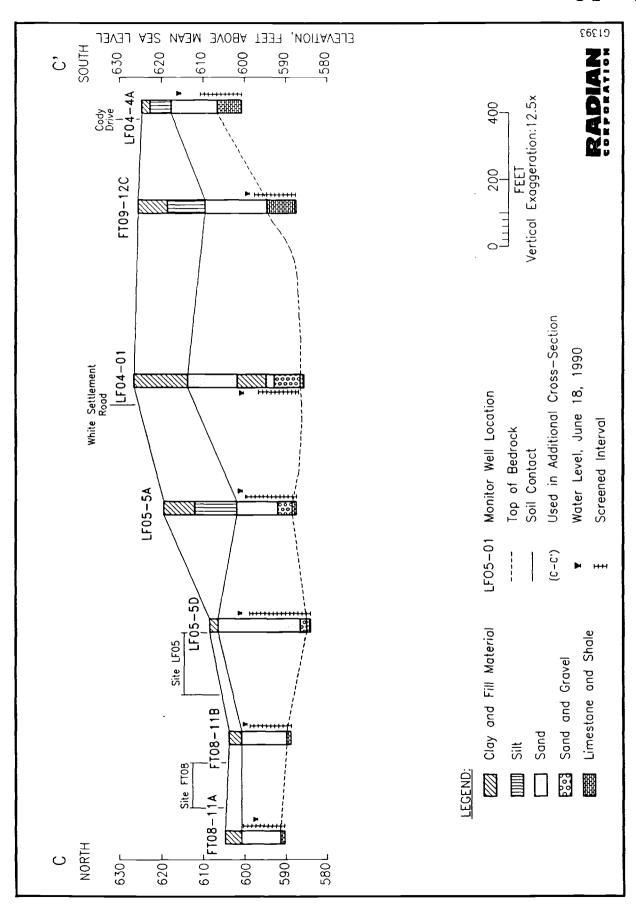


Figure 3-7. Geologic Cross-Section C-C', Flightline Area, Carswell AFB, Texas

on this cross-section at location LF04-4A. Monitor well FT09-12C occurs at approximately the southern edge of the paleochannel deposits observed in the Flightline Area.

Cross-section D-D' is shown on Figure 3-8. Again, a relatively thick sequence of coarse-grained materials occurs through the middle portion of the cross-section. Southward from boring LF05-12, the coarse-grained Upper Zone deposits thicken, with the thickest deposits occurring in the vicinity of LF04-4F. Monitor well LF04-4F is the only location on this section where gravels were found. Location LF04-4B, like LF04-4A (C-C'), is located on a relative high on the bedrock surface.

Geologic cross-section E-E' (Figure 3-9) shows the thickest sequence of Upper Zone sands and gravels occurring in the vicinity of LF04-4G. Monitor well LF04-4G occurs within the trend of the thickest Upper Zone sands and gravels observed in the Flightline Area. The trend axis is situated approximately on White Settlement Road.

The easternmost cross-section through the Flightline Area, F-F' (Figure 3-10), includes five newly installed ground-water monitor wells. Although monitor well boring LF04-10 encountered the thickest sequence of Upper Zone coarse-grained sediments, the potentiometric surface (derived from water-level measurements taken on June 18, 1990) indicates ground-water flow toward the location of LF05-19, rather than parallel to the depositional trend, as might be expected.

3.4 <u>Hydrogeology</u>

Five major hydrogeologic units exist beneath Carswell AFB. From shallowest to deepest they are: 1) an Upper Zone of unconfined ground water occurring within the alluvial terrace deposits associated with the Trinity River; 2) an aquitard of predominantly dry limestone of the Goodland and Walnut Formations; 3) an aquifer in the Paluxy Sand; 4) an aquitard of relatively impermeable limestone in the Glen Rose Formation; and 5) a major

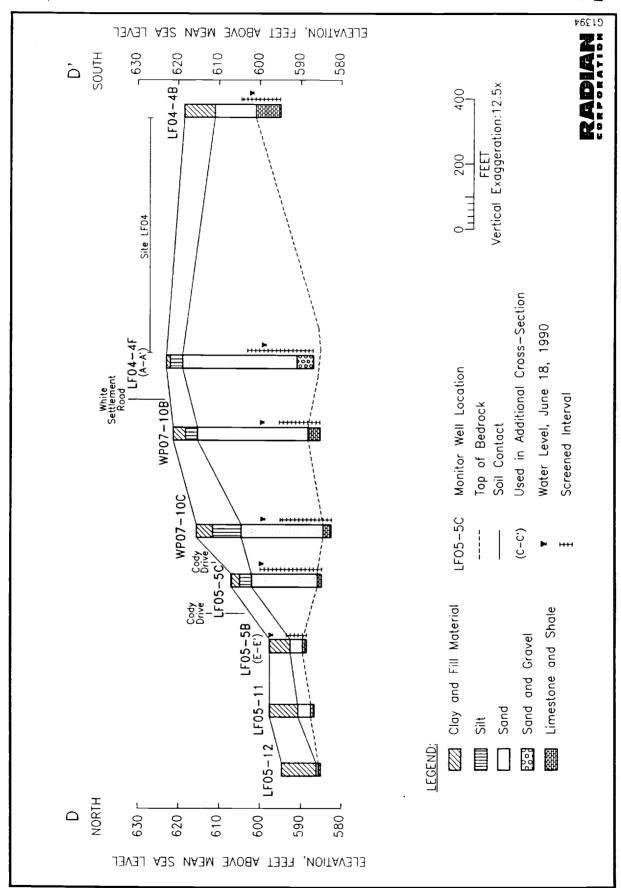


Figure 3-8. Geologic Cross-Section D-D', Flightline Area, Carswell AFB, Texas

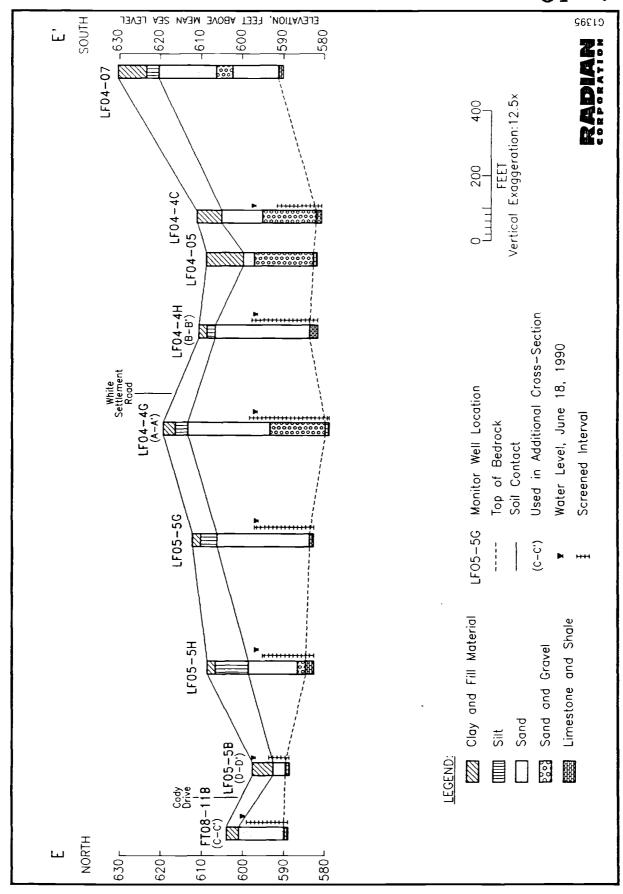


Figure 3-9. Geologic Cross-Section E-E', Flightline Area, Carswell AFB, Texas

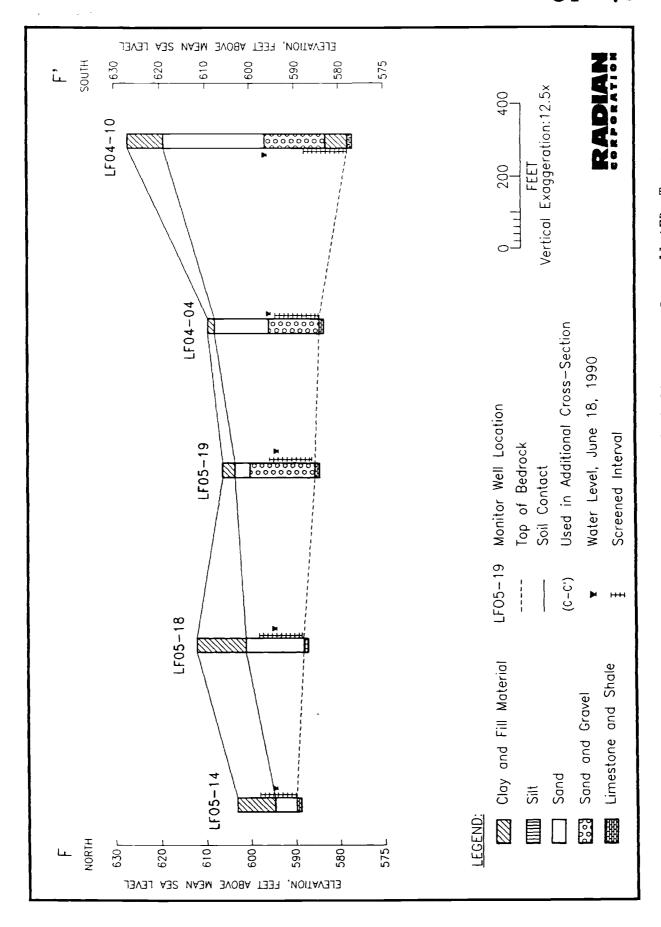


Figure 3-10. Geologic Cross-Section F-F', Flightline Area, Carswell AFB, Texas

aquifer in the sandstone of the Twin Mountains Formation. Only the first three units were investigated in the Flightline Area during the IRP, with the primary focus being on the Upper Zone. The Upper Zone was the only unit studied in this most recent Stage 2 (1990) effort. Figure 3-11 shows the general depth of occurrence and thickness of each of the major hydrogeologic units expected in the Flightline Area. Descriptions and properties of the hydrogeologic units are summarized in Table 3-2. The following subsections present the hydrogeologic characteristics of each unit based on field data and literature sources.

3.4.1 <u>Upper Zone Aquifer</u>

The Upper Zone ground water occurs within the alluvial deposits at Carswell AFB. Low permeability is typical of this alluvium because of the large amounts of clay and silt. However, there are zones of greater permeability in the sands and gravels of former channel deposits. Recharge to the water-bearing deposits is local, from rainfall and infiltration from stream channels and drainage ditches. The direction of ground-water flow is generally controlled by the bedrock topography of the Walnut Formation.

3.4.1.1 Ground-Water Occurrence and Flow

Table 3-3 shows the results of the synoptic water-level survey performed on 18 June 1990. Figure 3-12 is the resulting potentiometric surface map of the Upper Zone Aquifer. Ground-water flow in the Upper Zone is generally northeastward, toward Farmers Branch, a tributary to the West Fork of the Trinity River.

From the outlet of Farmers Branch from the underground aqueduct (which conveys the stream under the Flightline) the stream flows over bedrock at the Goodland/Walnut Formation until it flows into the Trinity River on the eastern boundary of Carswell AFB. The Upper zone ground-water flow through the Flightline Area, being generally northeastward, intercepts Farmers Branch in the northern and northeastern portion of the Flightline Area site. The

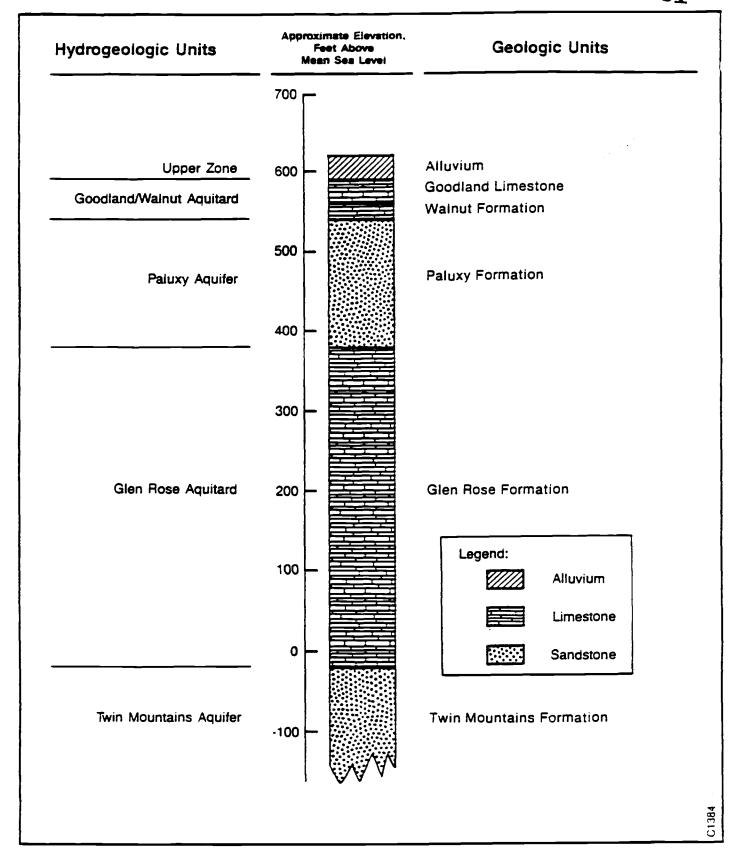


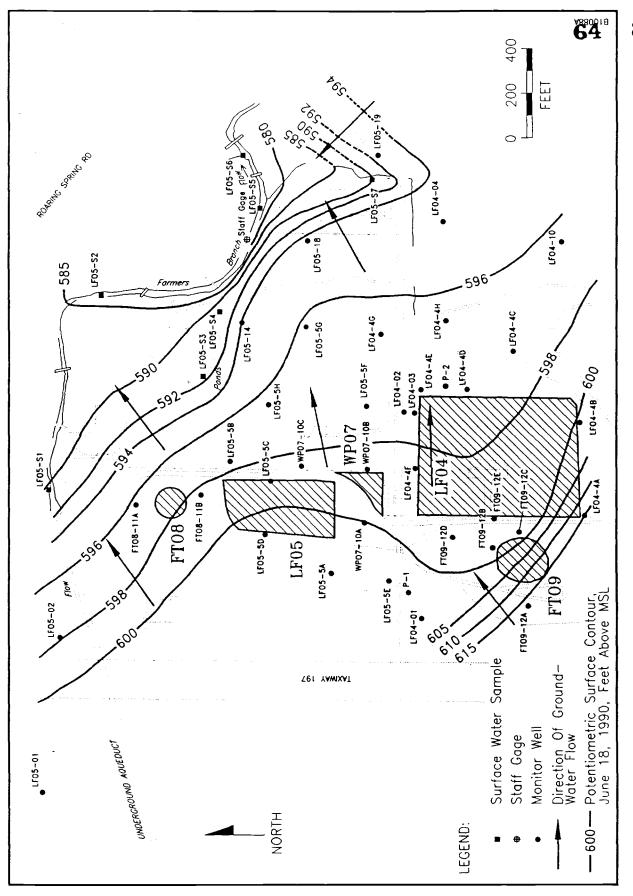
Figure 3-11. Generalized Hydrogeologic Units at Flightline Area, Carswell AFB, Texas

TABLE 3-2. GEOLOGIC FORMATIONS IN THE VICINITY OF CARSWELL AFB, TEXAS

System	Series and Group	Formation and Member	Thickness (ft)	Character of Rocks	Topographic Expression	Water-Bearing Properties
Quaternary	Recent and Pleistocene	Alluvium	0-45	Sand, gravel, clay, and silt.	Terrace and flood-plain deposits.	Smalt to moderate yields. Water unsatisfactory for use unless treated.
Cretaceous	Comanche Series Washita Group	Duck Creek Formation	06-0	Impure limestone and marl, which is blue when fresh and straw- colored when weathered. Fossiliferous with distinctive ammonites.	Bench topography produced by lower limestone unit. Upper marl forms slope separating the Duck Creek from Fort Worth limestone.	Small to moderate yields. Water unsatisfactory for use unless treated.
	Comanche Series Fredericksburg Group	Kiamichi Formation	07-0	Blue and brownish-yellow marl, thin limestone and sandstone flags.	Grassy slope separating scarps of Goodland and Duck Creek Formations.	Small to moderate yields. Water unsatisfactory for use unless treated.
		Goodland Limestone	0-130	Chalky-white fossil- iferous limestone, and blue to yellowish brown marl.	Prominent glaring-white escarpment along streams.	Small to moderate yields. Water unsatisfactory for use unless treated.
		Walnut Clay	0-28	Shell agglomerate fossiliferous clay and limestone, sandy clay, and black shale.	Forms conspicuous escarpment and waterfalls in western Cross Timbers belt.	Not known to yield water to wells in Tarrant County.
				UNCONFORMITY		
Cretaceous	Commanche Series Trinity Group	Paluxy Sand	140-190	Fine-grained sand, shale, sandy shale, lignite and pyrite.	Sandy soil, hummocky top- ography, heavily wooded with oaks.	Source of supply for most households, smaller cities, and some industries.
		Glen Rose Limestone	250-450	Fine-grained limestone, shale, marl, and sand- stone.	Not exposed in Tarrant County.	Sands yield small supplies to wells in fort Worth and western Tarrant County. Water too highly
mineralized	mineralized east of Fort					Worth.
	9	Twin Mountains Formation (formerly Travis Peak Formation)	250-450	Coarse to fine-grained sandstone, red shale, red shale,	Not exposed in Tarrant County.	Principal aquifer in Tarrant County. Yields large supplies for base.
and colonic						purposes. Water in upper sands east of Fort Worth may be highly mineralized.
						•

TABLE 3-3. RESULTS OF FLIGHTLINE AREA UPPER ZONE SYNOPTIC WATER LEVEL SURVEY CONDUCTED ON JUNE 18, 1990

Location ID	Time	Measuring Point Elevation (Ft, MSL)	Depth to Water (Ft)	Water Level Elevation (Ft, MSL)
LF04-01	1553	629.24	28.98	600.26
LF04-02	1738	623.68	26.23	597.45
LF04-03	1735	623.25	25.67	597.58
LF04-04	1756	612.07	16.75	595.32
LF04-10	1801	626.54	30.49	596.05
LF04-4A	1813	625.76	10.48	615.28
LF04-4B	1818	619.90	18.27	601.63
LF04-4C	1809	613.04	16.42	596.62
LF04-4D	1749	615.35	18.06	597.29
LF04-4E	1746	618.54	21.35	597.19
LF04-4F	1731	625.36	26.96	598.40
LF04-4G	1740	620.02	23.69	596.33
LF04-4H	1752	613.43	17.15	596.28
LF05-01	1545	621.96	18.14	603.82
LF05-02	1549	622.69	24.86	597.83
LF05-14	1700	602.98	8,84	594.14
LF05-18	1834	611.84	17.73	594.11
LF05-19	1650	606.08	12.54	593.54
LF05-5A	1618	623.18	22.67	600.51
LF05-5B	1708	600.45	3.73	596.72
LF05-5C	1627	608.68	9.56	599.12
LF05-5D	1624	611.71	10.98	600.73
LF05-5E	1615	626.89	26.60	600.29
LF05-5F	1721	618.95	21.83	597.12
LF05-5G	1714	615.39	19.31	596.08
LF05-5H	1711	610.62	14.54	596.08
FT09-12A	1557	635.66	17.10	618.56
FT09-12B	1603	627.55	28.38	599.17
FT09-12C	1601	628.05	29.23	598.82
FT09-12D	1611	627.45	28.13	599.32
FT09-12E	1606	627.48	28.68	598.80
FT08-11A	1634	608.22	11.23	596.99
FT08-11B	1630	608.14	8.63	599.51
WP07-10A	1620	626.70	26.68	600.02
WP07-10B	1728	624.46	25.63	598.83
WP07-10C	1726	617.24	18.59	598.65
Staff Gage	1840	579.44	0.57	579.01
_		(1.0 ft mark on gage)	(water reading or	n gage)



Potentiometric Surface Map of Upper Zone Aquifer, Flightline Area, Carswell AFB, Texas Figure 3-12.

Upper Zone sediments, which are up to 40 feet thick in areas west and southwest of Farmers Branch, either thin to their eventual disappearance at the stream or are exposed as sheer cliffs (cut-banks) near the stream. Field reconnaissance revealed Upper Zone ground water seeping from the face of the exposed banks.

The potentiometric surface map (Figure 3-12) includes water level information from both the ground water and the surface water (surveyed at six locations along Farmers Branch). Farmers Branch is shown to be a point of discharge for ground water, as the Upper Zone hydraulic gradient is shown to be toward the stream.

The area north of Farmers Branch in the Flightline Area has not been investigated. However, visual observation has shown the area to be relatively flat in the vicinity of the stream. Upper Zone deposits are probably thin in this area. With Farmers Branch being a zone of ground-water discharge in the Flightline Area, Upper Zone ground-water flow in the area north of Farmers Branch would locally be toward the stream.

3.4.1.2 Hydraulic Characteristics of Upper Zone Aquifer

Slug tests were performed in twelve Flightline Area wells (April, 1988) and an aquifer pumping test was conducted (June, 1990) to determine the hydraulic properties of the Upper Zone aquifer in the Flightline Area at Carswell AFB. The following section presents a discussion of the characteristics of the Upper Zone aquifer as determined from this testing. A more thorough description of the aquifer pumping test procedures and analysis is provided in Appendix F.

Slug Test Results

The ability of the Upper Zone alluvial deposits to transmit ground water was initially characterized based on the results of single-well aquifer tests (slug tests). These tests were performed as described in Section 2.2.5, and analyzed according to the Bouwer and Rice (1976) method.

The calculated hydraulic conductivity values ranged from 22.6 ft/day $(7.98 \times 10^{-3} \text{ cm/sec})$ at well LF04-4D to 1.2 ft/day $(4.1 \times 10^{-4} \text{ cm/sec})$ at well LF04-4A. The lowest calculated hydraulic conductivities were from wells known to be located outside the main pattern of channel deposits observed in the Flightline Area. The lowest calculated values were from test wells LF04-4A and FT0-12A (Figure 3-12).

The main limitation on slug tests is that they are heavily dependent on a high-quality well intake (screened interval). If well development is inadequate, measured values may be highly inaccurate (decreased conductivities); conversely, if development is very thorough, the measured values may reflect the increased conductivities in the artificially induced gravel pack around the screen. In any case, slug tests usually provide aquifer parameter values that are fairly representative of a small volume of porous media in the immediate vicinity of the well. Aquifer pumping tests, however, usually provide measurements of aquifer parameters that are averaged over a much larger aquifer volume.

Aquifer Pumping Test Results

The data obtained during the June, 1990 Upper Zone aquifer pumping test were analyzed by several methods. Following field plotting of time-drawdown and distance-drawdown measurements, hand plotted observation well drawdown and pumping well recovery data were analyzed by the Cooper-Jacob method. In addition, a computer aquifer analysis program was used. The well hydraulics interpretation program used was WHIP^M, which can simulate and analyze both drawdown and recovery tests.

The diagnostic procedures use semilog drawdown (Cooper-Jacob) analyses and Theis recovery analyses to obtain preliminary estimates of the transmissivity and storage coefficient. Theis curves are generated using these values and are graphically compared to the observed data. Portions of the generated curves can be "windowed" so only reliable data are used for the generation of final transmissivity and storage coefficient values. The

equations used in the Cooper-Jacob analysis of hand-plotted drawdown and recovery data is provided in Appendix F.

In addition to standard semilog and loglog plots, the effects of various time transformations on the data as well as first and second derivatives of the drawdowns were performed. Observing the derivative drawdown plots was useful for determining that portion of the test data displaying Theis behavior. Additionally, the Dupuit correction for water table conditions was applied to all computer analyses and the initial estimates of transmissivities and storage coefficients were optimized using an ordinary least squares fitting criterion. The Dupuit correction allows for the minimization of the irregularities inherent in field data and applies a more sophisticated mathematical approach to the calculation of transmissivities and storage coefficients.

Three different computer generated plots and analyses were determined to best represent the Upper Zone aquifer hydraulic properties of transmissivity and storage coefficient. These were the observation well (LFO4-02) drawdown and recovery analyses and the pumping well (LFO4-03) recovery analysis.

Seven additional monitor wells were measured for response to the pumping well during the test. These wells did not respond to pumping. Water level measurements taken in these wells were plotted and are included in Appendix F.

Table 3-4 shows the summarized results of the Flightline Area aquifer pumping test analysis. Both the pumping well (LF04-03) and the observation well (LF04-02) are completed in the generally west to east trend of relatively thick sands and gravels observed in the Flightline Area, and both wells are screened across the entire saturated thickness of the Upper Zone aquifer. The calculated hydraulic conductivity and transmissivity values fall within the range for clean sands and gravels (Freeze and Cherry, 1979) which

SUMMARY OF UPPER ZONE AQUIFER PUMPING TEST RESULTS, FLIGHTLINE AREA, CARSWELL AFB, TEXAS (JUNE, 1990) TABLE 3-4.

Well Number	Type of Test Analyses	Distance From Pumping Well (ft)	Transmissivity	Hydraulic Conductivity	Storage Coefficient (Dimensionless)
LF04-02	Drawdown	50	9771 ft ² /day	835 ft/day (2.9 x 10 ⁻¹ cm/sec)	1.2×10^{-2}
	Recovery	50	8260 ft ² /day	705 ft/day (2.5 x 10 ⁻¹ cm/sec)	
LF04-03	Recovery	Pumping Well	9501 ft ² /day	812 ft/day (2.9 x 10^{-1} cm/sec)	
		Average Values	9177 ft ² /day	784 ft/day (2.8 x 10 ⁻¹ cm/sec)	1.2 × 10 ⁻²

is consistent with the lithology for the Upper Zone aquifer. The storage coefficient value calculated also falls within the range for clean, unconfined aquifers.

The hydraulic conductivity calculated from the pumping test analysis was significantly higher than that determined from prior slug testing. Based on the limitations of the slug testing discussed earlier, the aquifer pumping test results are more representative of the Upper Zone Aquifer characteristics.

3.4.2 Goodland/Walnut Aquitard

The ground water present in the alluvium is separated from the aquifers below by the low permeability limestones and shales of the Goodland Limestone and Walnut Formation. The aquitard is composed of moist clay and shale layers interbedded with dry limestone beds. Though the Formations are primarily dry, drillers in the area report that small amounts of water enter the borehole while drilling through the Walnut Formation, suggesting that ground water may be moving through the Walnut Formation along bedding planes (Hargis and Associates, 1985). The thickness of the Goodland/Walnut aquitard is approximately 30-40 feet beneath the Flightline Area at Carswell AFB. thickness is based on two monitor wells drilled through the aquitard and completed in the Paluxy Aquifer during the initial Stage 2 study (Radian, 1989). However, the top of the aquitard is an erosional surface and erosion may have reduced the thickness of the limestone or eroded it entirely in isolated areas, (e.g., at AF Plant 4 beneath Building 189 along Grants Lane, the Goodland Limestone is completely absent and only three feet of the Walnut Formation are present (Hargis and Associates, 1985)).

3.4.3 Paluxy Aquifer

The Paluxy Aquifer, the areal extent of which is shown in Figure 3-13, is the shallowest bedrock aquifer underlying Carswell AFB. In the Carswell AFB area, water in the uppermost part of the Paluxy Formation would

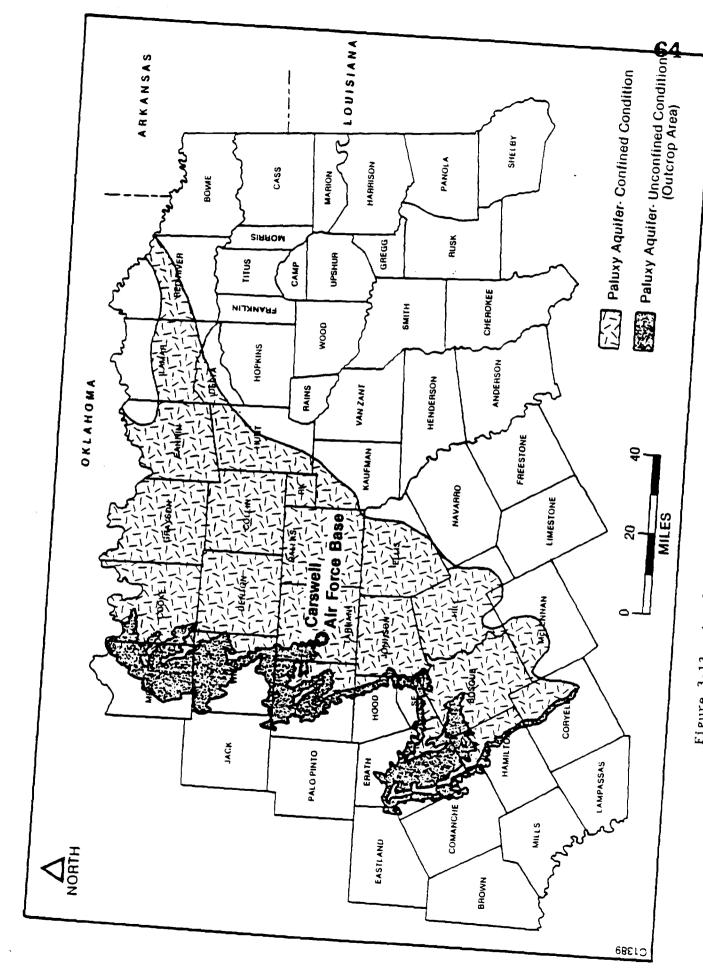


Figure 3-13. Areal Extent of the Paluxy Aquifer, North Texas

90

naturally occur under confined conditions beneath the Goodland/Walnut aquitard (except where the aquitard has eroded away, as discussed above). However, extensive ground-water pumping in the Fort Worth area, including the City of White Settlement, has lowered the Paluxy Aquifer potentiometric surface below the top of the formation, resulting in unconfined conditions beneath the base. Water-level measurements taken in the Flightline Area Paluxy wells (P-1 and P-2), found the water level to be about five feet below the top of the formation, or about 75 feet below land surface. With the Paluxy Formation having an upper and lower sand member, and the lower member having larger grain size and higher permeability, most water wells are completed in the lower section of the Paluxy Aquifer.

Recharge to the Paluxy Aquifer occurs where the formation crops out west of Carswell AFB in the AF Plant 4 area. The Paluxy Formation also crops out north of the base in the bed of Lake Worth. The lake is a major recharge point for the aquifer and creates a potentiometric high in its vicinity. Regional ground-water flow within the Paluxy Aquifer is southeastward in the direction of the regional dip. At Carswell AFB, ground-water flow is influenced by recharge from Lake Worth, which creates a potentiometric high, and by ground-water withdrawals by the community of White Settlement. This drawdown results locally in a more southerly flow direction within the Paluxy Aquifer.

Transmissivities in the Paluxy Aquifer range from 1,263 to 13,808 gallons per day per foot (gpd/ft), and average 3,700 gpd/ft (CH2M Hill, 1984). The Paluxy Formation thickness ranges from 140 to 190 feet, averaging 160 feet in Tarrant County. The actual water-bearing thickness in the Carswell AFB area probably approximates the formation thickness, but the aquifer is separated into two distinct water-bearing zones, denoted as the upper and middle/lower Paluxy. In some cases, the middle and lower Paluxy are also separated by low-permeability layers. The Paluxy dips uniformly at a rate ranging from 35 to 40 feet per mile and averaging 37 feet per mile. It is encountered at increasing depths eastward, reaching a maximum depth of about 900 feet. During the Phase II Stage 1 Flightline Area investigation (Radian, 1986), short-term aquifer tests (pumping and recovery) were conducted in the

Paluxy Aquifer monitor wells P-1 and P-2. Recovery test data analysis indicates the transmissivity of the upper Paluxy is approximately 1750 gallons per day per foot (235 square feet per day).

3.4.4 Glen Rose Aquitard

Below the Paluxy Aquifer are the fine-grained limestone, shale, marl, and sandstone beds of the Glen Rose Formation. The thickness of the formation in the vicinity of Carswell AFB reportedly ranges from 250 to 450 feet. Although the sands in the Glen Rose Formation yield small amounts of water to wells in Fort Worth and western Tarrant County, the relatively impermeable limestone is an aquitard restricting water movement between the Paluxy Aquifer above and the Twin Mountains aquifer below.

3.4.5 Twin Mountains Aquifer

The Twin Mountains Formation is, geologically, the oldest formation used for water supply in the Carswell AFB area. The formation occurs approximately 600 feet below Carswell AFB. The thickness of the formation ranges from 250 to 430 feet.

Recharge to the Twin Mountains Aquifer occurs west of Carswell AFB, where the formation crops out. Ground-water movement is eastward in the downdip direction. Like the ground water in the Paluxy Aquifer, Twin Mountains ground water occurs under water-table conditions in the recharge area and becomes confined as it moves downdip. Transmissivities in the Twin Mountains Aquifer range from 1,950 to 29,700 gpd/ft and average 8,450 gpd/ft in Tarrant County. Hydraulic conductivities range from 8 to 165 gpd/ft² and average 68 gpd/ft² in Tarrant County (CH2M Hill, 1984).

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4.0 NATURE AND EXTENT OF CONTAMINATION

The Carswell AFB IRP Phase II Stage 1 investigation (1984-85) detected concentrations of TCE and other halogenated hydrocarbons in the Upper Zone ground water in the vicinity of the flightline. In addition, concentrations of several metals exceeded federal drinking water standards in the ground water. During Stage 2 (1987-88), additional work was done to define the extent of the known contaminants present in the Flightline Area.

The primary objective of the addition (Modification 0004) to the original Stage 2 Statement of Work was to further characterize the nature and extent of various contaminants in the Upper Zone ground water beneath the Flightline Area. Specifically, the goal was to define the eastern and western boundaries of the known TCE plume under the Flightline Area, and to collect additional data such that a remedial action could be designed and implemented. In addition, an attempt to determine more conclusively the limits of the known inorganic contamination in the various Flightline Area sites was undertaken.

4.1 Summary of QA/QC

Carswell AFB ground water and surface water may be characterized by the primary data set generated from samples collected during April and May 1990. QA/QC results indicate this primary data set was generated under controlled analytical conditions. However, chemical concentrations should be qualified during site interpretation to incorporate uncertainty in terms of both measurement error and environmental variability. Qualifications to the data include:

Laboratory blanks indicate a potential for false-positive results due to laboratory contamination for the following analytes. Maximum concentrations found in laboratory blanks are presented with specific analytes.

EPA 601 - tetrachloroethene 0.17 μ g/L,

trichloroethene 1.3 μ g/L,

EPA 325.3 - chloride 1.5 mg/L,

SW6010	-	aluminum	0.53 mg/L,
		beryllium	0.0023 mg/L,
		copper	0.053 mg/L,
		nickel	0.021 mg/L,
		silver	0.051 mg/L,
		strontium	0.0047 mg/L,
		vanadium	0.025 mg/L,
		zinc	0.044 mg/L,
EPA 365.2		orthophosphate	0.012 mg/L,
SW7421		lead	0.0099 mg/L.

- Field blanks indicated a potential for false-positive results due to field contamination. Generally, field blanks contained very low level concentrations for common organics and inorganics. Natural sample results near laboratory and field blank concentrations may be considered false-positive results due to incomplete decontamination of sampling equipment or air-borne contamination.
- Variability due to environmental sources and measurement imprecision may be greater than expected for specific analytes. For instance, ICAP interference check samples indicated an interference for iron that caused 25% variability for check samples. Generally, measurement imprecision is greatest for results near the detection limit. As expected, relative variability (i.e., coefficient of variation (CV)) increases near detection limits even though absolute variability is very small.

The results of the recent ground-water sampling effort are discussed in the following subsections.

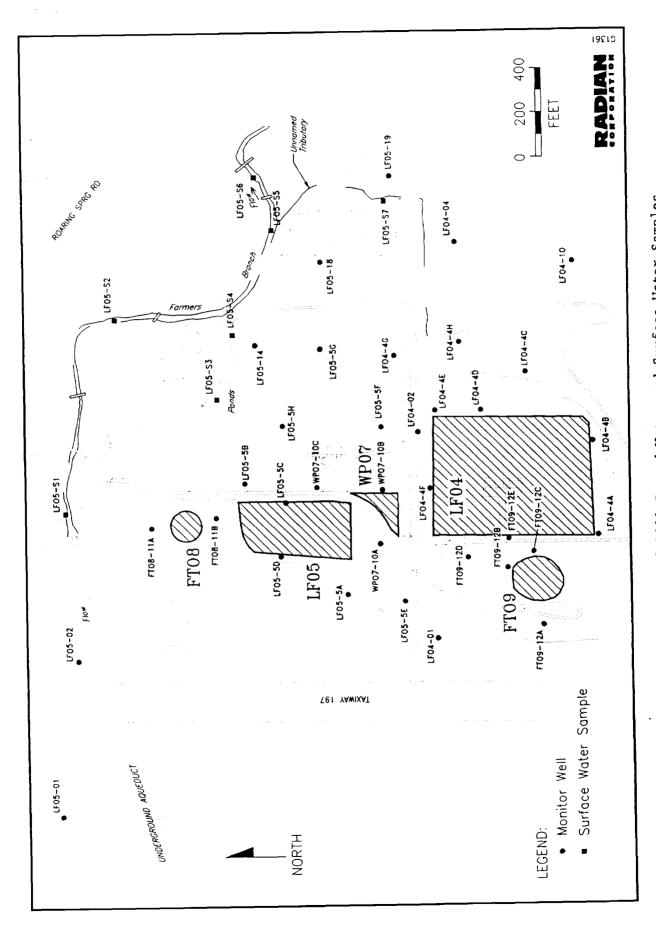
4.2 Results of Ground-Water and Surface Water Analyses

Ground-water samples from thirty-five wells were collected during April and May 1990 for laboratory analysis. Seven surface water samples were also collected. Since contamination was previously found to exist only in those wells screened in the Upper Zone Aquifer, all ground-water samples were collected from Upper Zone monitor wells. Figure 4-1 depicts the locations of all of the most recent water sampling sites at the Flightline Area. sample was submitted to Radian's laboratories for analysis of the organic and inorganic constituents listed in Table 4-1. Both organic and inorganic constituents exceeding EPA drinking water standards (Maximum Contaminant Levels, or MCLs) had been detected in the Flightline Area in past sampling efforts. An Informal Technical Information Report (ITIR) with analytical summary tables, QA/QC data, sample cross-reference tables and chain-of-custody forms for the recent ground-water investigation at the Flightline Area was provided to the U.S. Air Force HSD IRP Program Office in September 1990 (Radian 1990d). Following is a brief summary of the quality assurance/quality control (QA/QC) results for most recent Carswell AFB ground-water sampling.

4.2.1 Ground-Water Contamination

As indicated in previous Flightline Area sampling efforts, TCE was the principal contaminant detected which exceeded EPA primary standards. The only other organic constituent found to exceed federal standards was vinyl chloride. Two organic compounds were detected in ground water with concentrations exceeding EPAs proposed MCLs; these included tetrachloroethene and cis-1,2-dichloroethene.

Four inorganic compounds exceeded federal primary drinking water standards in the most recent water sampling. Chromium was found in excess of the respective MCL in three monitor wells. Lead, arsenic and mercury were found in concentrations exceeding the respective MCLs in one well each.



Locations of 1990 Ground-Water and Surface Water Samples, Flightline Area, Carswell AFB, Texas Figure 4-1.

TABLE 4-1. SUMMARY LISTING OF ORGANIC AND INORGANIC ANALYTES, FLIGHTLINE AREA, CARSWELL AFB, TEXAS

	Inorganic	Parameters
Organic Parameters	Metals	Non-Metals
l,l,l-Trichloroethane	Aluminum	Chloride
1,1,2,2-Tetrachloroethane	Antimony	Fluoride
1,1,2-Trichloroethane	Arsenic	Nitrate as N
1,1-Dichloroethane	Barium	Orthophosphate
1,1-Dichloroethene	Beryllium	Sulfate
1,2-Dichlorobenzene	Boron	Total Dissolved
1,2-Dichloroethane	Cadmium	Solids
1,2-Dichloropropane	Calcium	
1.3-Dichlorobenzene	Chromium	
1,4-Dichlorobenzene	Cobalt	
2-Chloroethylvinyl ether	Copper	
Bromodichloromethane	Iron	
Bromoform	Lead	
Bromomethane	Magnesium	
Carbon tetrachloride	Manganese	
Chlorobenzene	Mercury	
Chloroethane	Molybdenum	
Chloroform	Nickel	
Chloromethane	Potassium	
Dibromochloromethane	Selenium	
Methylene chloride	Silicon	
Tetrachloroethene	Silver	
Trichloroethene	Sodium	
Trichlorofluoromethane	Strontium	
Vinyl chloride	Thallium	
cis-1,2-Dichloroethene	Vanadium	
cis-1,3-Dichloropropene	Zinc	
trans-1,2-Dichloroethene		
trans-1,3-Dichloropropene		

Contamination detected in the ground water of the Flightline Area is limited to the Upper Zone Aquifer. The low permeability limestone of the underlying Goodland/Walnut aquitard underlies the Upper Zone Aquifer. No Flightline Area monitor wells are completed in the aquitard as past drilling in the Goodland and Walnut Formations has shown the formations to be non-water bearing. Ground-water samples from the Paluxy Aquifer, which underlies the Goodland/Walnut aquitard in the Flightline Area, have had no detections of contaminants. Therefore, the vertical extent of organic compound contamination in the Flightline Area corresponds to the upper surface of the Goodland/Walnut aquitard.

A detailed discussion of the pertinent organic and inorganic constituents and ground-water quality indicators follows.

4.2.1.1 Organic Ground-Water Contaminants

Table 4-2 summarizes the findings of the laboratory analyses for organic constituents in Flightline Area monitor wells, with respect to primary drinking water standards (MCLs). TCE exceeded the MCL in 27 of the 35 wells sampled. Vinyl chloride exceeded the MCL in seven wells.

Tetrachloroethene (PCE) was detected in a total of six wells, and exceeded the proposed MCL in three wells. The proposed MCL for cis-1,2-dichloroethene was exceeded in samples from 23 of the monitor wells in the Flightline Area. This compound was detected in 30 of 35 wells in the Flightline Area. Trans-1,2-dichloroethene, another isomer of dichloroethene, was also detected frequently in the Flightline Area, but at significantly lower concentrations than the cis- isomer. The proposed MCL (100 μ g/L) for the trans- isomer was never exceeded by Flightline Area water samples.

Following is a more detailed discussion of organic constituents detected in the ground water of the Flightline Area.

SUMMARY OF ORGANIC GROUND-WATER SAMPLING RESULTS, SPRING 1990, CARSWELL AFB, TEXAS TABLE 4-2.

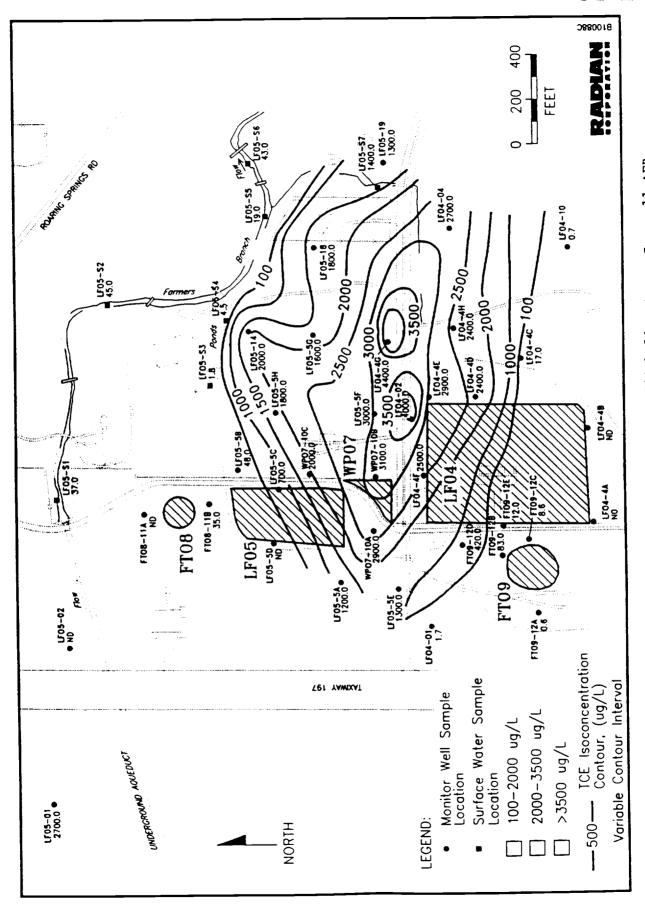
rameter bons (601) µg/L hane hane hane	EPA Standards or		Range of	7	112.11	
	111111111111111111111111111111111111111	Range	Concentrations	Analyses for Constituent	Detected and Second	Exceeding EPA MCL/PMCL
Purgeable Halocarbons (601) µg/L 1,1,1-Trichloroethane 1,1,2,2-Terrachloroethane 1,1,2-Trichloroethane 1,1,2-Trichloroethane 1,1,1-Dichloroethane	rroposed scandards (µ8/L)		or constituents Detected	Wells)	(No. of Wells)	Wells)
1,1,1-Trichloroethane 1,1,2,2-Terrachloroethane 1,1,2-Trichloroethane 1,1,2-Trichloroethane						
1,1,2,2-Tetrachloroethane 1,1,2-Trichloroethane 1,1-Dichloroethane	200 (M)	0.2-50	0.37-0.70	74 (35 + 2 dup)	3 (3)	0
1,1,2-Trichloroethane 1,1-Dichloroethane		0.15-38	QN	Ξ		0
1,1-Dichloroethane		0.2-50	QN	74 (35)	0	0
		0.5-120	1.1	74 (35)	1 (1)	0
1,1-Dichlorethene	7 (M)	0.2-50	1.3-1.5	74 (35)	2 (2)	0
1,2-Dichlorobenzene	600 (P)	0.5-120	QN	74 (35)	0	0
1,2-Dichloroethane	5 (H)	0.1-25	£		0	0
1,2-Dichloropropane	5 (P)	0.1-25	QN.	_	0	0
1,3-Dichlorobenzene		0.32-80	Ð	74 (35)	o	0
1,4-Dichlorobenzene	75 (M)	0.24-60	9.6	74 (35)	1 (1)	0
2-Chloroethylvinyl ether		0.5-130	QN QN	_	0	0
Bromodichloromethane		0.1-25	æ	_	0	0
Bromoform		0.5-130	QN	_	0	0
Bromomethane		1.2-300	QN	_	0	0
Carbon tetrachloride	5 (¥)	0.12-30	2	_	0	0
Chlorobenzene		0.25-63	2.3	74 (35)	1 (1)	0
Chloroethane		0.52-130	1.8	_	1 (1)	0
Chloroform		0.1-25	ð	_	0	0
Chloromethane		0.3-75	Q.	_	0	0
Dibromochloromethane		0.2-50	QN	74 (35)	0	0
Methylene chloride		0.4-100	06-79			
Tetrachloroethene	5 (P)	0.1-25	0.55-30	74 (35)		
Trichloroethene	S (M)	0.2-50	0.56-4400	_	32 (3)	29 (27)
Trichlorofluoromethane		0.2-50	QN QN		0	0
Vinyl chloride	2 (X)	0.2-50	6.2-170	_	8 (7)	8 (7)
cis-1,2-Dichloroethene	70 (P)	0.2-50	0.37-730	_	32 (30)	23 (22)
cis-1,3-Dichloropropene		0.2-50	£	74 (35)	0	0
trans-1,2-Dichloroethene	100 (P)	0.2-50	0.72-44	_	(9) 9	0
trans-1,3-Dichloropropene		0.34-85	QN	74 (35)	0	0
rrans-1,3-Dichlopene		0.44.0	Q.	_	•	

'EPA standards are designated: M - Maximum Contaminant Level (MCL) and P - Proposed Maximum Contaminant Level (PMCL).

Trichloroethene

Figure 4-2 depicts an isoconcentration contour map of the trichloroethene (TCE) plume as it was detected in the Spring, 1990 sampling effort in the Flightline Area. The concentration of TCE in the ground water was reported at maximum levels in monitor wells LF04-4G and LF04-02, with detected values of 4400 and 4000 micrograms per liter (μ g/L), respectively. The defined TCE plume has an aerial extent of approximately 50 acres, with most of the contamination underlying the base golf course. The limits of the plume are fairly well defined laterally, but not in the upgradient and downgradient directions (the extreme eastern and western portions of the Flightline Area). In the west, a concentration of 2700 μ g/L was detected in monitor well LF05-01, with no accompanying upgradient well analyses to allow for contaminant concentration contouring in the western direction. Detected concentrations of 1200 and 1300 μ g/L TCE in monitor well LF05-5A and LF05-5E, located hydraulically upgradient of Landfill 5 but with no near upgradient wells, prevents definition of the TCE plume along that upgradient edge. The ground-water flow direction (Figure 3-12) in the vicinity of monitor well LF05-01 is away from wells LF05-5A and LF05-5E, suggesting that contaminant plume migration deviates somewhat from the general ground-water flow pattern. Therefore, the contamination observed in monitor well LF05-01 could be continuous with that detected in LF05-5A and LF05-5E, but insufficient data from the intervening area make such a correlation speculative. Evidence of "black staining" at 39.5 feet in the log of borehole LFO5-15, located between wells LFO5-01 and LF05-5E, may be evidence of the TCE contamination being continuous between the wells. The TCE plume appears to intersect Farmers Branch (Figure 4-2) in the northeastern portion of the Flightline Area.

Figure 4-3 is a thickness map of the sand and gravel deposits in the Flightline Area. The thick sand and gravel sequences evident on a east-west linear trend through the Flightline Area are thought to represent a paleochannel, which is the depositional remains of a former stream channel. Past reports have suggested that, due to the greater density of TCE with respect to water, coupled with the increase in available porosity and permeability, the contamination will tend to migrate preferentially along



TCE Isoconcentration Contour Map, Flightline Area, Carswell AFB, Figure will be colored in Final Report Texas (Based on Spring, 1990 Water Sampling) Note: Figure 4-2.

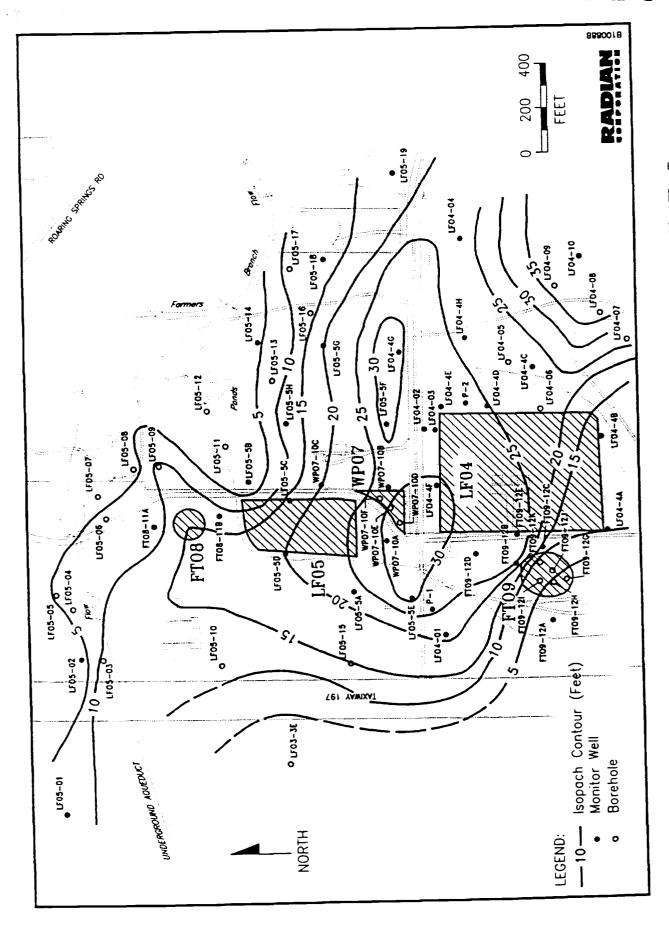
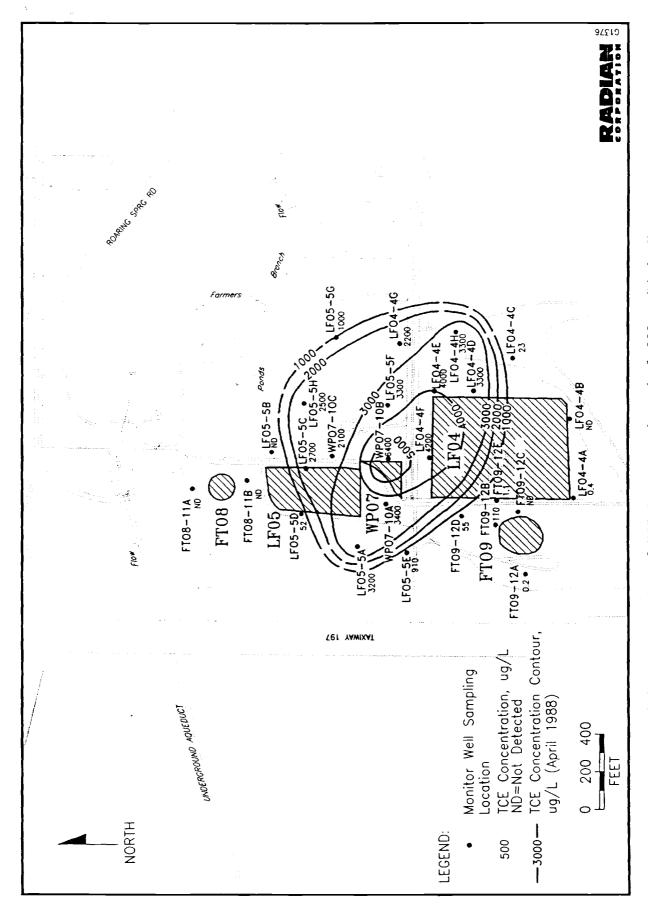


Figure 4-3. Sand and Gravel Isopach Map, Flightline Area, Carswell AFB, Texas

paleochannels filled with basal sands and gravels. When compared to the isoconcentration map of the TCE plume (Figure 4-2) this preferential migration is clearly evident, as the configuration of the plume and the zone of maximum concentrations closely resembles the location and configuration of the thickest Upper Zone sand and gravel sequences. Also of importance is the pattern of the relatively thick sand and gravels on the western side of the Flightline Area sites. Although data are sparse in the northwestern portion of Figure 4-3, it appears the thicker sands and gravels might trend westward on a line just south of LF05-01. The bedrock surface (Figure 3-3) is also relatively low in the vicinity of LF05-01. Both of these situations make the likelihood greater that contamination detected in monitor well LF05-01 is continuous with that in wells LF05-5A and LF05-5E.

The center of the TCE plume appears to be bimodal and is located hydraulically downgradient from Landfill 4, with TCE concentrations above 3000 μ g/L covering an area of approximately 6.5 acres. The apex of the TCE plume does appear to have shifted since the last ground-water sampling effort, which took place in April 1988. Figure 4-4 represents an isoconcentration contour map of the results of the April, 1988 ground-water sampling. By comparing the plume shape and concentration distribution shown on the April, 1988 isoconcentration map with that on the Spring, 1990 map, the plume appears to have migrated in an easterly, hydraulically downgradient direction. In addition, the maximum concentration observed between the two sampling efforts has decreased, from 6400 μ g/L in April 1988 to 4400 μ g/L in the most recent analysis. The potential significance of this decrease with respect to the fate and transport of the contaminants in the ground water will be discussed in Section 5 of this report. While the migration and degradation of the plume is consistent with the physiologic and hydrogeologic setting of the Flightline Area and the nature of the contaminant, some degree of analytical variability is inherent between any two laboratory analyses occurring over time. Continued monitoring of the wells in the Flightline Area will be necessary to confirm apparent trends in contaminant migration.

Multiple sources have been postulated for the organic contamination found in the subsurface in the Flightline Area. The disposal methods and



Contour Map of TCE Concentrations (> 1,000 $\mu g/L$) in Upper Zone Ground Water (April 1988), Flightline Sites, Carswell AFB, Texas Figure 4-4.

types of waste material believed to be present at Landfills 4 and 5 (LF04 and LF05) and the Waste Burial Area (WP07) are consistent with the types and amounts of contamination observed in downgradient wells. In addition, it is reasonable to assume that infiltration of some residual flammable solvents associated with the fire training activities at Site FT09 has occurred. Repeated evidence of TCE contamination in monitor wells located hydraulically upgradient of these sites indicates the existence of additional upgradient source(s). In the 1990 sampling, TCE concentrations of 1300 μ g/L and 1200 μ g/L were detected in monitor wells LF05-5E and LF05-5A, respectively, located upgradient to Landfill 5.

Air Force Plant 4 has been identified in past reports (Radian, 1986; Radian, 1989) as the probable upgradient source, but limited well control and lack of contemporaneous analytical data from the western and northwestern Flightline Area preclude this interpretation. A TCE concentration of 2700 μ g/L in monitor well LF05-01, in the extreme northwestern portion of the Flightline Area (Figure 4-2) supports the existence of a significant source to the northwest. Further evidence is provided by the contamination detected around Site FT08. Monitor well FT08-11B was found to contain 35 μ g/L TCE. While this well is downgradient to the site, no contamination was detected in previous sampling efforts, and the site is not considered a contributor to the main TCE plume.

Contamination in the subsurface associated with Site FT09 was not considered associated with the primary TCE plume in the RI/FS Stage 2 report. Evidence cited included the absence of ground water in boreholes beneath the site and ground-water contamination being limited to monitor wells which potentially receive runoff from the site. During the most recent investigation, TCE contamination was detected in each of the three wells at the site, suggest that, whatever the actual source, the contamination can be logically addressed along with the principal TCE plume for the purpose of this report. As with the other Flightline Area sites, the contamination may have resulted from activities conducted at the site, or may be from an upgradient source.

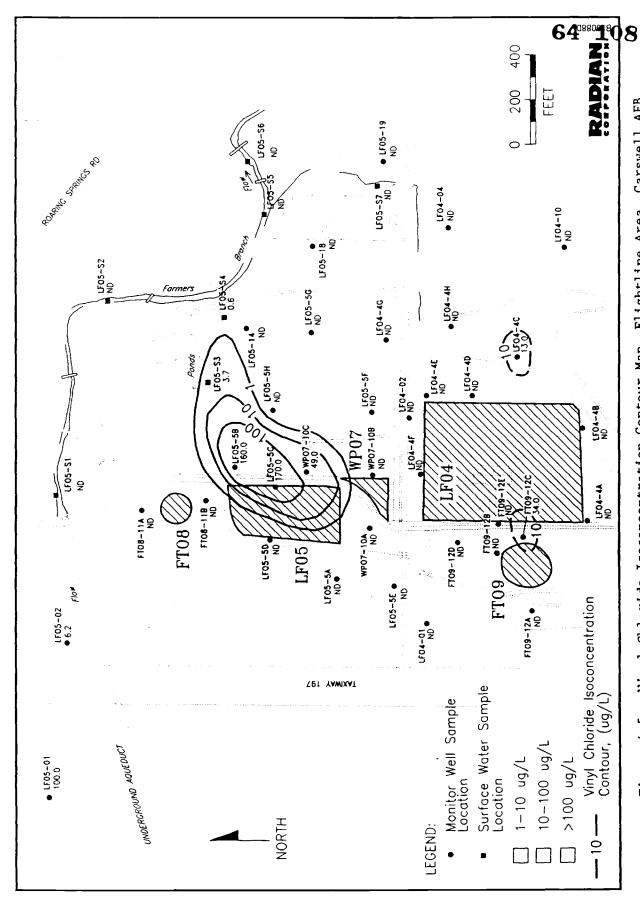
Although there is significant evidence for one or more upgradient, non-Flightline Area source of TCE contaminations in the shallow ground water, the increased TCE concentrations detected in the ground water as it moves through the Flightline Area suggest wastes previously disposed of in the landfills and waste burial area are point sources contributing to the overall contaminant plume.

Vinyl Chloride

Vinyl chloride was the second most dominant contaminant in the Flightline Area, exceeding the MCLs in seven wells. Figure 4-5 illustrates an isoconcentration map of the vinyl chloride concentrations in the Flightline Area. Unlike the TCE plume, the vinyl chloride plume appears to be composed of several smaller zones of contamination, with the principal area being associated with Landfill 5.

Each of the wells in the main plume in which the vinyl chloride was detected is immediately hydraulically downgradient of Site LF05. The maximum concentration of vinyl chloride detected in the Flightline Area was 170 μ g/L in monitor well LF05-5C. This well constitutes the apex of the main plume. Lesser amounts were detected in LF05-5B and WP07-10C, with 160 μ g/L and 49 μ g/L, respectively. Vinyl chloride was also detected in this area in the April, 1988 ground-water sampling effort. None of the sampled monitor wells located hydraulically upgradient of Site LF05 contained vinyl chloride, suggesting Site LF05 is the source of the main Flightline Area vinyl chloride plume.

Four additional wells contained vinyl chloride above the EPA MCL. Well LF04-4C contained vinyl chloride at 13 $\mu g/L$, which is a higher concentration than was detected in the April 1988 sampling, in which 3.8 $\mu g/L$ was detected. This is the only well downgradient from Site LF04 in which vinyl chloride has been detected. Vinyl chloride was also detected in LF05-01 (100 $\mu g/L$), again suggesting a contaminant source upgradient from the Flightline Area. Since vinyl chloride may be a primary contaminant or one of the



Vinyl Chloride Isoconcentration Contour Map, Flightline Area, Carswell AFB, Note: Figure will be colored in Final Report Texas (Based on Spring, 1990 Water Sampling) Figure 4-5.

daughter products of TCE and multiple sources have been postulated for the contaminants present in the Flightline Area, it is difficult to pinpoint the exact source(s) of the vinyl chloride present in any individual well. The chemical inter-relationship between vinyl chloride, TCE and the other organic contaminants detected in the Flightline Area is discussed in Section 5.

<u>Tetrachloroethene</u>

The presence of tetrachloroethene (PCE) was confirmed in six monitor wells in the Flightline Area. The EPA PMCL of 5.0 μ g/L was exceeded in three of these six wells. Due to the limited number of PCE detections in the Flightline Area ground water, an isoconcentration map was not prepared. Table 4-3 provides the laboratory results showing levels of PCE detected in each of the six monitor wells.

Two of the three wells found to exceed the PMCL for PCE were at Site FT09 (FT09-12B and FT09-12C). Monitor well FT09-12B had the highest confirmed level of PCE at 30 μ g/L. PCE was not detected at this site during the April, 1988 sampling event. However, because PCE can be a precursor of TCE, the PCE contamination detected in the Flightline Area is probably related to the TCE and will be discussed in conjunction with the TCE plume in this report.

Total-1,2-Dichloroethene

The presence of cis-1,2-dichloroethene (cis-1,2-DCE) was confirmed in thirty monitor wells in the Flightline Area, with concentrations ranging from 0.37 μ g/L to 730 μ g/L. Trans-1,2-dichloroethene (trans-1,2-DCE) was confirmed in six wells, with concentrations ranging from 0.72 to 44.0 μ g/L. Trans-1,2-DCE was detected only in wells in which cis-1,2-DCE was also detected. Because trans-1,2-DCE and cis-1,2-DCE are isomers, they will be considered together as part of the total-1,2-DCE plume.

TABLE 4-3. SUMMARY OF GROUND-WATER SAMPLES WITH CONFIRMED CONCENTRATIONS OF TETRACHLOROETHENE, SPRING 1990, CARSWELL AFB, TEXAS

Well Number	Tetrachloroethene Concentration (μ g/L)
LF04-4C	3.1
LF05-02	0.55
LF05-19	17.0
FT09-12B	30.0
FT09-12C	8.1
FT09-12E	0.82

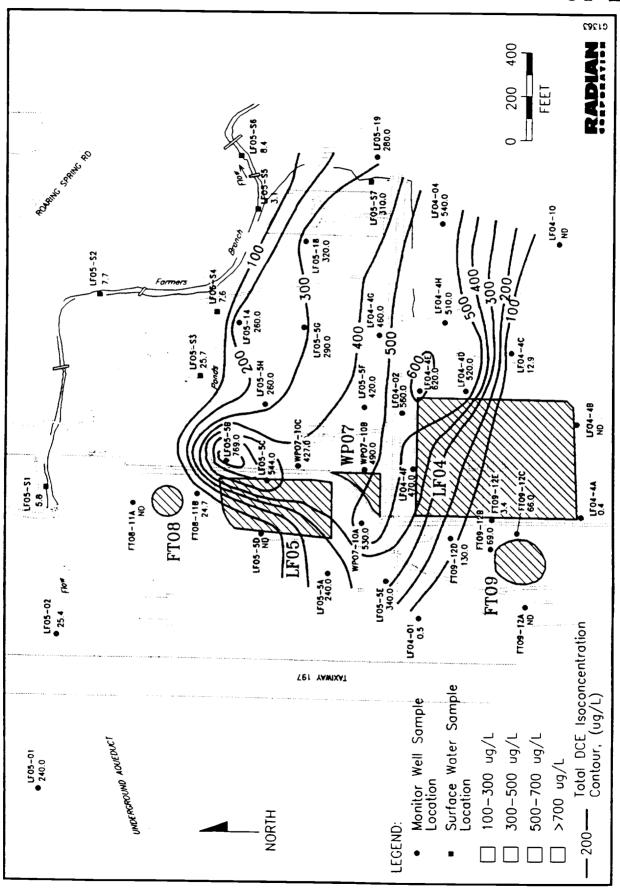
Figure 4-6 illustrates an isoconcentration contour map for 1,2-DCE in the Flightline Area. As in the case of the TCE isoconcentration contour map, the apex of the plume is bimodal. The two 1,2-DCE nodes are located hydraulically downgradient of LF04 and LF05, respectively, and each is of the same relative magnitude of concentration. Further similarity to the TCE plume includes a lack of definition in the eastern and western margins of the plume. Monitor well LF05-01, in the extreme northwest portion of the Flightline Area, had a detected level of 1,2-DCE of 240 μ g/L. This level of contamination, coupled with multiple confirmed detections of 1,2-DCE in wells immediately upgradient from sites LF04 and LF05, strongly support the presence of an upgradient contamination source. A confirmed detection of 540 μ g/L of 1,2-DCE in monitor well LF04-04, in the southeastern portion of the Flightline Area, again makes it impossible to enclose contaminant contours in that area with confidence.

Other Organic Contaminants

Several other purgeable halocarbons were detected in the ground water in the Flightline Area (Table 4-2). These include the detection of 1,1,1-trichloroethane, 1,1-dichloroethane, 1,1-dichloroethane, 1,4 dichlorobenzene, chlorobenzene, and methylene chloride. None of these compounds were detected in levels exceeding current EPA standards.

4.2.1.2 Inorganic Ground-Water Constituents

Four inorganic constituents, arsenic, mercury, chromium and lead, identified in the shallow Flightline Area ground water exceeded MCLs in unfiltered samples. However, based on the nature of the metal occurrences, they are not considered indicative of a ground-water contaminant problem at the site. Following is a discussion of inorganic contaminants detected in the shallow ground water of the Flightline Area.



Total-1,2-Dichloroethene Isoconcentration Contour Map, Flightline Area, Carswell AFB, Texas (Based on Spring, 1990 Water Sampling) Note: Figure will be colored in Final Report Figure 4-6.

4.2.1.3 Metals

Total arsenic and mercury were each detected above MCL values in unfiltered samples from single monitor wells in the Flightline Area. Table 4-4 shows the metals detected above MCLs. Total arsenic (MCL = 0.05 mg/L) narrowly exceeded the limit (by 0.003 mg/L) in the well in which it was detected (LF05-02). Total mercury exceeded the MCL by 0.0042 mg/L in FT09-12D. Total Arsenic was detected in concentrations above the MCL in eight monitor wells in the Flightline Area during the April 1988 sampling, but mercury was not detected.

Total lead was found to exceed the MCL of 0.05 mg/L in two monitor wells in the Spring 1990 sampling effort, as compared with total concentrations above the MCL in eight wells in the April 1988 sampling. Total chromium exceeded the MCL of 0.05 mg/L in three wells in the Spring 1990 sampling, as compared with twelve in 1988. No two total metals concentrations were found above established MCLs in the same well. The total lead contamination detected in monitor wells LF05-01 and LF05-14 exceeded federal standards by a maximum of 0.021 mg/L. Total chromium was detected at a maximum of 0.15 mg/L above federal standards in monitor well FT08-11A.

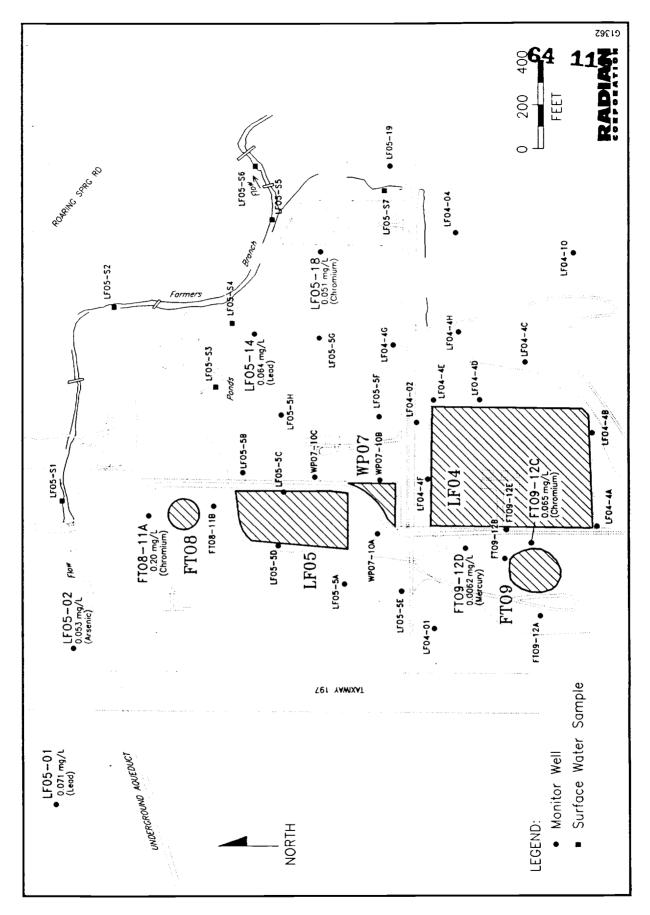
Figure 4-7 depicts the locations of the seven wells in which MCLs for total metals were exceeded. The random distribution of the contaminants makes delineation of a specific source difficult. Multiple man-made, as well as natural sources are possible for the detected metal concentrations. In general, the metal concentrations detected in Flightline Area wells were less than those reported from previous sampling events. Metals such as cadmium and barium, detected in several wells at total concentrations exceeding MCLs in the April 1988 sampling event, were not detected at levels above MCLs in any wells in the Spring 1990 sampling effort.

As stated above, no two metals were detected in excess of MCLs in the same well. In addition, in each case where a MCL was exceeded, the reported concentration was for total rather than dissolved metal. Total metal

SUMMARY OF INORGANIC GROUND-WATER SAMPLING RESULTS, SPRING 1990, CARSWELL AFB, TEXAS TABLE 4-4.

				Ic	Total Number of Samples	
	EPA Standard		Range of Concentrations	Analyses for Constituent	With Constituent	Exceeding EPA MCL
Analytical Parameter	(MCL).	of Detection Limits	of Constituents Detected	(No. of Wells)	Detected (No. of Wells)	(No. of Wells)
Metals						
Aluminum		0.20-0.40	0.23-52	74 (35)	39 (35)	0
Antimony		0.10-0.11	ND	74 (35)		0
Arsenic	0.05 (M)	0.004-0.33	0.0041-0.053		32 (24)	1 (1)
Bartum	1.0 (M)	0.01-0.011	0.07-0.47			0
Beryllium		0.002-0.0022	0.003-0.004			0
Boron		0.60-0.66	0.061-0.92	_	(7) 7	0
Cadmium	0.01 (M)	0.005-0.0055	QN	_	_	0
Calctum		1.00-2.00	99-740			
Chromium	0.05 (M)	0.01-0.011	0.015-0.20		_	3 (3)
Cobalt		0.01-0.011	0.012-0.039			0
Copper	;	0.02-0.022	0.024-0.047			0
Iron	;	0.04-0.044	0.041-61	_	_	0
Lead	0.05 (M)	0.003-0.055	0.003-0.09		_	2 (2)
Magnes 1 um		1.00-1.10	3.4-20		_	0
Manganese	1	0.01-0.11	0.012-5.00			0
Mercury	0.002 (M)	0.0002-0.0018	0.0025-0.0062		2 (2)	1 (1)
Molybdenum		0.05-0.055	QN			0
Nickel		0.02-0.022	0.022-0.12			0
Potassium		3.00-3.30	0.031-10	_	20 (13)	0
Selenium	0.010 (M)	0.005-0.33	QN			0
Silicon		1.00-1.10	4.2-110		_	0
Silver	0.05 (M)	0.01-0.11	0.011-0.027			0
Sodium		1.00-1.10	10-102	_		0
Strontlum		0.003-0.0033	0.029-1.1		74 (35)	0 (
Thalltum		0.10-0.11	Q	_		0
Vanadium		0.02-0.022	0.025-0.013	_		0
Zinc	:	0.02-0.22	0.024-0.012	74 (35)	59 (31)	0
Non-Metals						
Chloride	;	1.00-1.00	5.1-71	74 (35)	37 (35)	0
Fluoride	4.0 (M)	0.10-0.10	0.2-1.0	74 (35)	37 (35)	0
Nitrate as N	•	0.02-0.20	0.024-6.4	74 (35)	37 (35)	0
Orthophosphate		0.01-0.01	0.011-0.057	74 (35)	10 (9)	0
Sulface		0.20-20.0	2.2-140		_	0
Total Dissolved Solids	lids	9.00-9.00	9.0-760	74 (35)	37 (34)	0
10 01-40cc10 18301	27.103	>> >>	>> > > > > > > > > > > > > > > > > > > >			,

*EPA standard is designated: M - Maximum Contaminant Level (MCL).



Location of Monitor Wells (BOLD Well Numbers) in Which EPA MCLs for Metals Were Exceeded, Flightline Area, Carswell AFB, Texas Bas n S 1g, '.'0 W Sa 'ng) Figure 4-7.

analyses are performed on unfiltered samples and as such may yield artificially elevated metal results, because fine suspended material in the unfiltered sample can break down during sample acidification releasing additional metals ions into the fluid medium. The dissolved metals analyses, performed on field-filtered samples, are considered more representative of the actual ground-water chemistry. In light of this, there is little evidence to support the existence of metal contamination in the Flightline Area at this time. In addition, the fact that a dissolved metal analysis was not performed during earlier sampling efforts, suggests that the previous data on metal contamination in the Flightline Area are inconclusive.

4.2.1.4 Ground-Water Quality Indicators

Analysis of numerous anions and cations was performed on samples from each monitor well in the Flightline Area to aid in the determination of ground-water quality. These included:

- Calcium;
- Magnesium;
- Potassium;
- Sodium;
- Chloride; and
- Sulfate.

In addition, total dissolved solids (TDS) were analyzed. Table 4-5 lists the averaged concentrations for each analyte by site (in the Flightline Area), as well as the overall average for the entire Flightline Area, weighted by site. Also, a range of concentrations for each analyte (except potassium) is provided which is considered 'typical' for Tarrant County. Concentrations for each analyte are in milligrams per liter.

At each site, calcium concentrations are elevated above the 'typical' range. In contrast, sodium concentrations fall uniformly below the

SUMMARY OF GROUND-WATER QUALITY INDICATORS BY SITE, SPRING 1990, CARSWELL AFB, TEXAS, WITH TYPICAL RANGE FOR TARRANT COUNTY TABLE 4-5.

			Averag	ged Concer	Averaged Concentrations, mg/L	ng/L	
Site/Locality	Calcium	Magnesium	Potassium		Sodium Chloride	Sulfate	Total Dissolved Solids
FT08	150	7.8	3.3	70	22	87	089
FT09	140	5.4	3.1	23.8	13	64.2	787
LF04	136.6	9.9	3.3	29	25.5	61.3	565
LF05	167.7	11.3	5.3	28.9	33.9	65.2	782
WPO7	140	5.4	3.1	23.8	13	64.2	570
Flightline Area*	149.7	8.1	7.0	30.2	25.4	6.49	641.3
Tarrant County	1-114	0-11	1	141-670	14-650	21-579	381-1735

*Flightline Area averages were computed by the weighted probability method based upon the number of samples taken at each site.

given range. This is considered normal in ground water moving through limerich soils, such as those in the Flightline Area. All other ground-water quality indicator concentrations fall within the given range except the average chloride concentration in site FT09, which falls slightly below normal. Of significance is that a pronounced uniformity is evident between each of the sites in the Flightline Area, strongly suggesting an overall aquifer continuity, and further implying that the contaminants in the subsurface beneath each site are likely a part of the same contiguous plume.

4.2.2 Surface Water

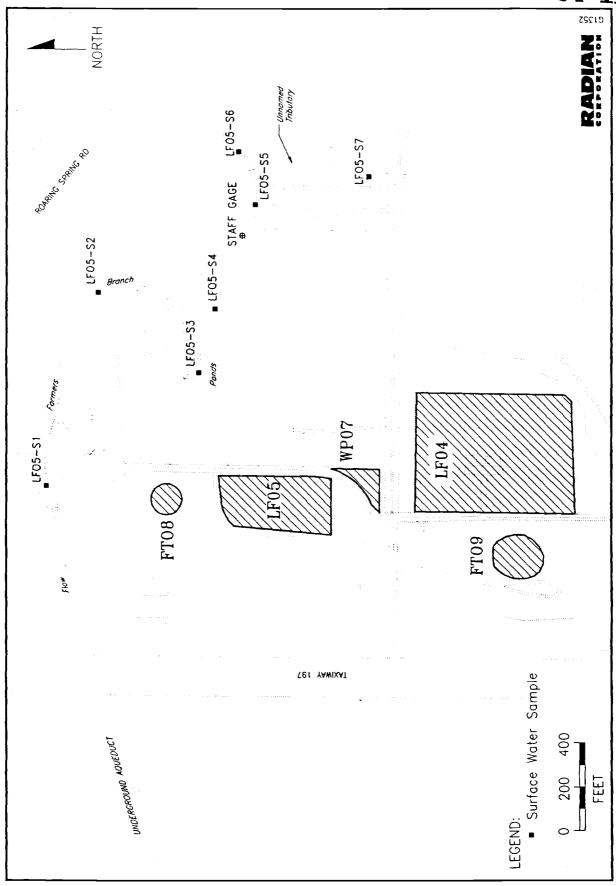
Seven surface water samples were collected from the locations shown in Figure 4-8. Samples were collected from four locations along Farmers Branch, one from the unnamed tributary to Farmers Branch, and one each from the two small ponds near the golf course maintenance headquarters. Surface water sampling sites were selected both to characterize the nature and extent of surface water contamination and to determine the relationship, if any, between surface water and ground water contamination. Surface water samples were also collected during the Phase II Stage 1 investigation (Radian, 1986).

4.2.2.1 Organic Contaminants

Table 4-6 summarizes the Spring, 1990 analytical results of organic constituents in surface water samples, with comparison to federal drinking water standards. Trichloroethene (TCE) was confirmed in all surface water samples, with federal MCLs being exceeded at five locations. Confirmed concentrations ranged from 1.8 μ g/L at LF05-S3 to 1400 μ g/L at LF05-S7. The elevated concentration at site LF05-S7 strongly suggests communication between the ground water and surface water at that location, as the concentration detected falls within the TCE isoconcentration contours generated for the ground-water analysis (Figure 4-2). Lower concentrations of TCE in samples collected from the upstream portion of Farmers Branch appear to be the result of an upgradient contaminant source. This is particularly evident at surface water sample location LF05-S1, which is located where the underground aqueduct emerges following transporting Farmers Branch water under the runway area of

Location of Surface Water Sampling Points, Flightline Area, Carswell AFB, Texas (Spring, 1990)

Figure 4-8.



4-26

SUMMARY OF ORGANIC SURFACE WATER SAMPLING RESULTS, SPRING 1990, CARSWELL AFB, TEXAS TABLE 4-6.

	EPA Standards	Range of Detection	Range of Concentrations of Constituents	Analyses for Constituent (No. of	With Constituent Detected and Second Column Confirmation	Exceeding EPA Standard (No. of
Analytical Parameter	(ng/L)	Limits	Detected	Locations)	(No. of Locations)	Locations)
Purgeable Halocarbons (601) µg/L						
1.1.1-Trichloroethane	200 (M)	0.20-10.0	Q.	8 (7)	0	0
1,1,2,2-Tetrachloroethane		0.15-7.5	ND	_	0	0
1,1,2-Trichloroethane		0.20-10.0	QN	8 (7)	0	0
1,1-Dichloroethane		0.50-25.0	ND	8 (7)	0	0
1,1-Dichlorethene	(X)	0.20-10.0	ě	_	0	0
1,2-Dichlorobenzene	600 (P)	0.50-25.0	S S	_	0	0
1,2-Dichloroethane	S (H	0.10-5.0	æ		0	0
1,2-Dichloropropane	S (P)	0.10-5.0	QN		0	0
1,3-Dichlorobenzene		0.32-16.0	£		0	0
1,4-Dichlorobenzene	75 (M)	0.24-12.0	æ		0	0
2-Chloroethylvinyl ether		0.50-25.0	æ		0	0
Bromodichloromethane		0.10-5.0	Z	8 (7)	0	0
Bromoform		0.50-25.0	Š		0	0
Bromomethane		1.2-59.0	Ð		0	0
Carbon tetrachloride	S (H)	0.12-6.0	S		0	0
Chlorobenzene		0.25-13.0	Ş		0	0
Chloroethane		0.52-26.0	Š		0	0
Chloroform		0.10-5.0	S S		0	0
Chloromethane		0.30-15.0	Š		0	0
Dibromochloromethane		0.20-10.0	£		0	0
Methylene chloride		0.40-20.0	QN	8 (7)	0	0
Tetrachloroethene	5 (P)	0.10-5.0	£			0
Trichloroethene	S (H)	0.20-10.0	1.8-1400		8 (7)	6 (5)
Trichlorofluoromethane		0.20-10.0	Ð	8 (7)	0	0
Vinyl chloride	2 (M)	0.20-10.0	0.56-3.7	_	2 (2)	1 (1)
cls-1,2-Dichloroethene	70 (P)	0.20-10.0	3.1-310.0	~		1 (1)
cis-1,3-Dichloropropene		0.20-10.0	QX QX	_	0	0
trans-1,2-Dichloroethene	100 (P)	0.20-10.0	0.46-0.66	8 (7)	2 (2)	0
trans-1,3-Dichloropropene		0.34-17.0	QN QN		0	0

'EPA standards are designated: M - Maximum Contaminant Level (MCL) and P - Proposed Maximum Contaminant Level (PMCL).

Carswell AFB. Surface water at this location has yet to be influenced by any Carswell AFB waste sites, as it is transported through a concrete conduit from the vicinity of Air Force Plant 4. Any contamination in a sample from this location is due to upgradient sources in the direction of Air Force Plant 4 further upstream. Surface water sampled at this location contained a TCE concentration of 39 μ g/L, which is above the MCL of 5 μ g/L.

TCE was also confirmed in the Phase II Stage 1 investigation. Two rounds of samples were collected, with TCE being detected upgradient of Site LF04 in both rounds and immediately downgradient from Site LF05 in the second round. No detected levels of TCE exceeded the MCL. No relationship was established between surface water and ground-water TCE concentrations during the Stage 1 study.

Vinyl chloride was the only other volatile organic compound detected in the surface water samples in excess of current MCLs during this investigation. Vinyl chloride was detected in two samples from the golf course ponds (LF05-S3 and LF05-S4). The MCL for vinyl chloride was exceeded in LF05-S3 where a concentration of 3.7 μ g/L was detected. Vinyl chloride was detected at the two locations where the lowest levels of TCE was detected, possibly suggesting a parent/daughter relationship. Vinyl chloride was also detected in Stage 1 surface water samples.

The other volatile organic constituents confirmed at the surface water locations during the Spring 1990 sampling event were cis- and trans-1,2-dichloroethene (-DCE), which have proposed MCLs. As in the case of the ground-water samples, the cis-1,2-DCE isomer was more prevalent than the trans-1,2-DCE isomer in surface water samples, with the cis- isomer occurring at each of the seven sample locations. Concentrations of cis-1,2-DCE ranged from 3.1 μ g/L to 310 μ g/L. Trans-1,2-DCE was confirmed in samples from two surface water locations, LF05-S2 and LF05-S3, with concentrations of 0.46 μ g/L and 0.66 μ g/L, respectively. As in the case of ground water, a relationship appears to exist between TCE and cis-1,2-DCE concentrations and the occurrence of each. Surface water sample LF05-S7 had the highest confirmed concentrations of both TCE and cis-1,2-DCE. The total-1,2-DCE concentration detected

at this sample location also falls within the total-1,2-DCE isoconcentration contours generated for the ground-water analysis (Figure 4-6).

4.2.2.2 <u>Inorganic Constituents</u>

No metals were detected in any surface water samples in excess of MCLs. Barium was detected at each location, and lead was being detected at all locations except LF05-S4 and LF05-S7. Arsenic was detected at LF05-S3. These concentrations are not considered significant, since the metals were commonly detected in levels below MCLs in the ground-water samples, and metals are naturally occurring constituents.

Water quality indicators were analyzed in the surface water samples. This was done both to assess the surface water quality and to attempt to clarify surface water/ground-water relationships. Indicators analyzed included:

- Total Dissolved Solids;
- Calcium;
- Magnesium;
- Potassium;
- Sodium;
- Chloride; and
- Sulfate.

Table 4-7 provides the averaged results for each of the water quality indicators for the surface water samples, as well as a range of concentrations for each analyte (except potassium) which are considered 'typical' for Tarrant County. In addition, the weighted averaged results for the same indicators are provided for the ground-water samples collected in the Flightline Area.

Only sodium occurs outside the range provided for the indicators analyzed, being considerably below what would be considered a 'normal' concentration. This was also the case in the ground-water samples. The

SUMMARY OF SURFACE WATER AND GROUND-WATER QUALITY INDICATORS, SPRING 1990, CARSWELL AFB, TEXAS, WITH TYPICAL RANGE FOR TARRANT COUNTY TABLE 4-7.

			Avera	zed Concer	Averaged Concentrations, mg/L	mg/L	
Locality	Calcium	Magnesium	Potassium	Sodium	Chloride Sulfate	Sulfate	Total Dissolved Solids
Surface Water Samples	105.7	6.2	က	26.5	28.7	69.3	447
Flightline Area	149.7	8.1	4.0	30.2	25.4	6.49	641.3
Tarrant County	1-114	0-11	;	141-670	14-650	21-579	381-1735

*Flightline Area averages were computed by the weighted probability method based upon the number of samples taken at each site.

similarity between the averaged surface water results and the averaged ground-water results strongly supports the interrelationship of the two water systems. This interrelationship has previously been discussed, and data generated at the site shows the unnamed tributary to Farmers Branch to be an influent stream in the Flightline Area. Only calcium differs slightly, with an averaged concentration in the ground water of approximately 45 mg/L greater than that of the surface water. This phenomenon is probably due to minor differences in the alkalinity of the two systems.

4.3 <u>Summary of Findings</u>

The main findings of the Flightline Area investigation with respect to the nature and extent of ground-water contamination are:

- Concentrations of TCE and vinyl chloride exceed MCLs in Upper Zone monitor wells in the Flightline Area.
- Multiple sources, including Sites LF04, LF05, WP07, FT09, and Air Force Plant 4, have been postulated for the various organic contaminant plumes which occur in the Flightline Area.
- Some downgradient migration of the plume apex and a decrease in total TCE concentration may have occurred since the monitor well network was previously sampled in 1988. However, continued monitoring is necessary to verify this possible trend, which could also be related by variability inherent in field and laboratory procedures or seasonal conditions.
- The extreme western limit of the Flightline Area TCE plume is as yet still undefined, but high levels of TCE and other contaminants detected in wells far upgradient of any known source areas or Carswell AFB strongly support the existence of additional upgradient source(s), potentially associated with documented TCE contamination in Upper Zone ground water beneath Air Force Plant 4.

- The extreme eastern (downgradient) limit of the TCE plume in the Upper Zone is also undefined.
- The vertical extent of contamination in the Flightline Area appears to correspond to the upper surface of the underlying Goodland/Walnut aquitard based on limited analytical results. Previous sampling of the two Paluxy Aquifer monitor wells did not detect any contamination.
- It is unlikely that any significant metals contamination exists in the Upper Zone Aquifer of the Flightline Area, as no dissolved metals concentrations exceeded MCLs.
- Both TCE and vinyl chloride were detected in excess of MCLs in surface water samples.
- Based upon the similarity between ground-water and surface water TCE concentrations, the unnamed tributary to Farmers Branch appears to be a zone of ground-water discharge.
- A pronounced similarity between surface water and ground-water quality indicators (and other analytes) supports the existence of zones of communication between the two water systems.
- In addition to contaminant contributions from unidentified upgradient source(s), the Flightline Area sites appear to be releasing some additional volatile organic compounds (mainly TCE, vinyl chloride, and 1,2-DCE) to the larger contaminant plume.
- Further investigation is required in the area between the
 Flightline Area sites and the upgradient source(s) to determine the relative contributions of each to Upper Zone ground-water contamination in the Flightline Area.

5.0 CONTAMINANT FATE AND TRANSPORT

The purpose of this section is to define the interrelationships between the various contaminant plumes which exist in shallow (Upper Zone) ground water in the Flightline Area, and to discuss their migration and persistence. The transport and fate of contaminants in the Flightline Area and the potential for off-site or off-base migration is a function of the physical hydrogeologic conditions and the plume interrelationship.

Volatile organic contaminants found in both the ground water and the surface water in the Flightline Area are the only hazardous waste constituents having a potential for off-site or off-base migration at levels of concern. No dissolved concentrations of inorganic constituents, specifically metals, were identified in the ground water at levels exceeding federal primary drinking water standards. Risk assessments were performed earlier during the Phase II Stage 2 investigation, however these focused principally on airborne hazards.

The ground-water contaminant plume in the Flightline Area is best described in terms of trichloroethene (TCE). As stated in Section 4, TCE is the principal contaminant at the site, with detected concentrations of up to 4400 μ g/L and exceeding EPA's MCL (5 μ g/L) in 27 wells. Other contaminants which are less widely distributed or occur in lower concentrations within the main Flightline Area plume include vinyl chloride, cis- and trans-1,2-dichloroethene, tetrachloroethene, and several other volatile organic halocarbon compounds.

5.1 Contaminant Persistence and Transformation

5.1.1 Background and Theory

The fate and persistence of the volatile organic contaminant plume in the Flightline Area is controlled by processes such as convection, contaminant adsorption and desorption on soil matrices, diffusion and dispersion, chemical and biological degradation, and volatilization and subsequent

resorption. Additionally, the nature of the contributing source(s), with regard to initial concentration and availability of contaminants, affects both fate and transport.

Diffusion and dispersion are chemical and mechanical processes whereby a contaminant tends to spread from the expected direction of transport governed by ground-water flow patterns. Diffusion depends on concentration gradients, and causes compounds to spread in the direction of lower concentrations. Dispersion is a function of mechanical transport, where physical mixing of the fluid media due to drag effects and pore channel tortuosity tend to cause some lateral solute spreading. Both of these phenomena contribute to dilution of specific contaminants within the body of the plume, but also result in the enlargement of the plume. Thus, these phenomena are factors in contaminant persistence and apparent retardation during transport.

Adsorption and desorption of a solute can be significant factors affecting the fate and transport of many types of contaminants. Compounds that are readily adsorbed onto grains of the aquifer material, and not readily desorbed are removed from the ground-water system and are not available for transport. Chemical partitioning by sorption can reduce effective transport by up to 100 percent. However, TCE is classified as a 'mobile' solute based upon its relatively low affinity to adhere to particles in the solid matrix. This classification is based on mobility, the value $K_{\rm d}$, from the equation:

$$K_d = \frac{a_s}{a_w}$$

where: K

 K_d - the soil-water distribution coefficient;

 a_s - the activity of the solute in the soil matrix; and

 a_w - the activity of the solute in the aqueous phase.

Mobility classes range from 'immobile' to 'very mobile', with TCE being in the second most mobile class out of five possible classes. In terms of solute transport, TCE has a higher activity in the aqueous phase, and hence will tend to both adsorb and desorb from soil grains with relative uniformity. Consequently TCE (and related daughter products) have a capacity for transport

which is only slightly retarded with respect to that due to the flow of ground water.

Mobility (K_d) is also a function of the concentrations of available solute, as the chemical activity of a solute will fluctuate based upon the chemical saturation of the parent media. One method of estimating K_d is based on site specific knowledge of TCE concentrations in the solid and aqueous phases. For the purpose of this report, TCE will be simply treated as a mobile solute, with adsorption and desorption being a factor in transport retardation.

As in the case of adsorption and desorption, TCE and other organic compounds may volatilize during transport and then be resorbed back into the aqueous phase. Chlorinated solvents are volatile compounds. Resorption of compounds following volatilization is based upon their ability to be adsorbed onto soil grains in the unsaturated zone and then be resorbed back into the ground water during periods of ground-water level fluctuation. Some compounds, such as 1,2-DCE and vinyl chloride, have low sorption coefficients, and consequently might be permanently removed from the ground-water system following volatilization. Because TCE is considered volatile and sorptive, some portion of the volatilized compound could re-enter the ground-water system during potentiometric (water level) rises. However, since the Upper Zone water table in the Flightline Area has not fluctuated significantly since 1985 when potentiometric surveys began, volatilization may possibly cause permanent removal of organic compounds from the ground water and therefore be a contributing factor in transport retardation. The degree of significance of this phenomenon is not known at the present time.

Chemical and biological degradation of the organic compounds in the Upper Zone ground water are potentially important factors in transport retardation in the Flightline Area. Tetrachloroethene (PCE), trichloroethene (TCE), cis- and trans-1,2-dichloroethene and vinyl chloride are all related by the chemical process of hydrogenolysis. From this reaction, PCE is broken down into a series of daughter products, ultimately yielding carbon dioxide

and water. This process is very common in nature, and may be biologically driven, as a form of biodegradation.

Figure 5-1 provides a summary of the three chemical and biological transformation pathways for the four principal organic contaminants in the Flightline Area. It is noteworthy that the half-lives for these pathways vary from tens of days to two to three years, and the pathway to cis-1,2-DCE is generally favored. Since TCE and PCE formerly were both widely used industrial solvents, some amount of TCE is probably from a primary source. It is doubtful that the sole source of TCE detected in the Flightline Area is from the breakdown of PCE. However, with the limited amount of PCE detected, either a significant portion of the original concentration of this solvent has broken down into TCE or related daughter products, or the original volume of PCE was much lower than TCE.

5.1.2 <u>Flightline Area (Golf Course)</u> Data

Figures 5-2, 5-3 and 5-4 present the isoconcentration maps generated for TCE, 1,2-DCE and vinyl chloride, respectively. This discussion of fate and transport of the ground-water contaminant plume does not consider the data north of the Farmers Branch underground aqueduct. There is insufficient lithologic and hydrogeologic data from the area between monitor well LF05-01 (to the north) and monitor wells LF05-5A and LF05-5E (to the south) to make a plausible interpretation of contaminant relationship between the areas.

Based on the previous discussion and the knowledge that 1,2-DCE and vinyl chloride are not known to be used at the base, it is reasoned that the presence of 1,2-DCE and vinyl chloride are the result of the chemical and biological breakdown of TCE. By comparing the zones of highest concentrations in these three plumes, some scenarios can be suggested regarding the timing and continuity of the contaminant sources. Reviewing the figures:

• During the Spring 1990 ground-water sampling, the apex of the TCE plume was centered along White Settlement Road, roughly hydraulically downgradient from Landfill 4 (LF04);

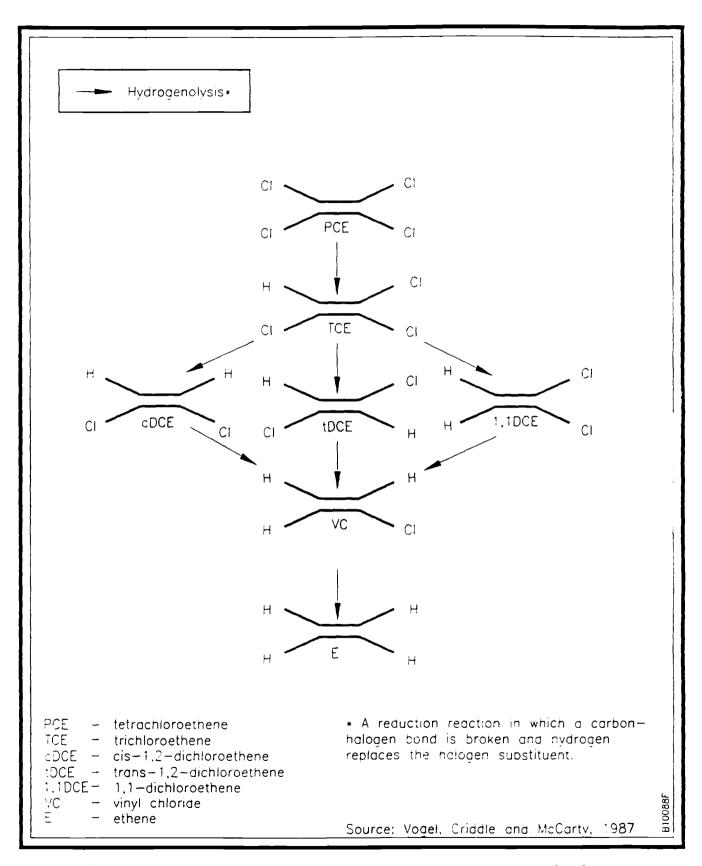
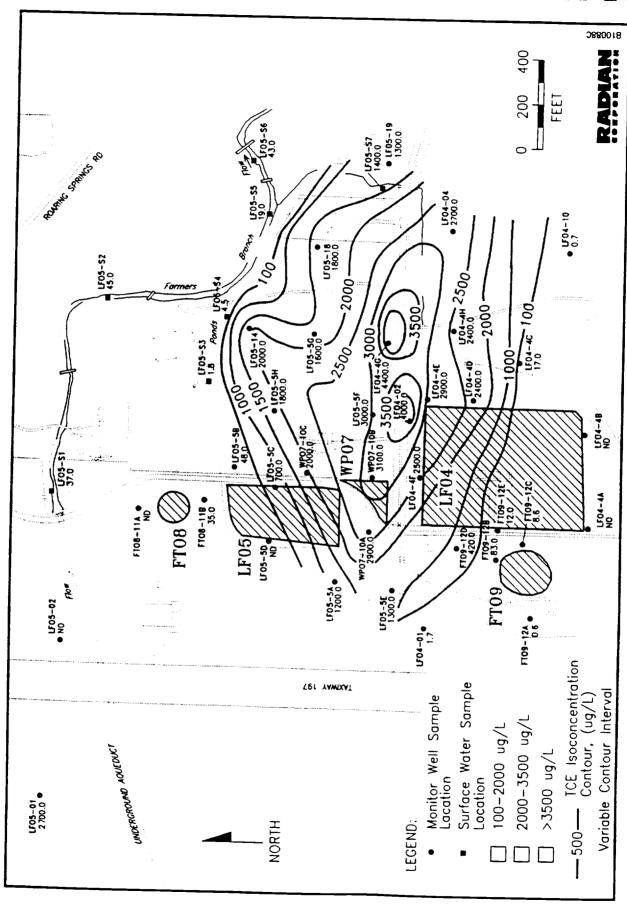
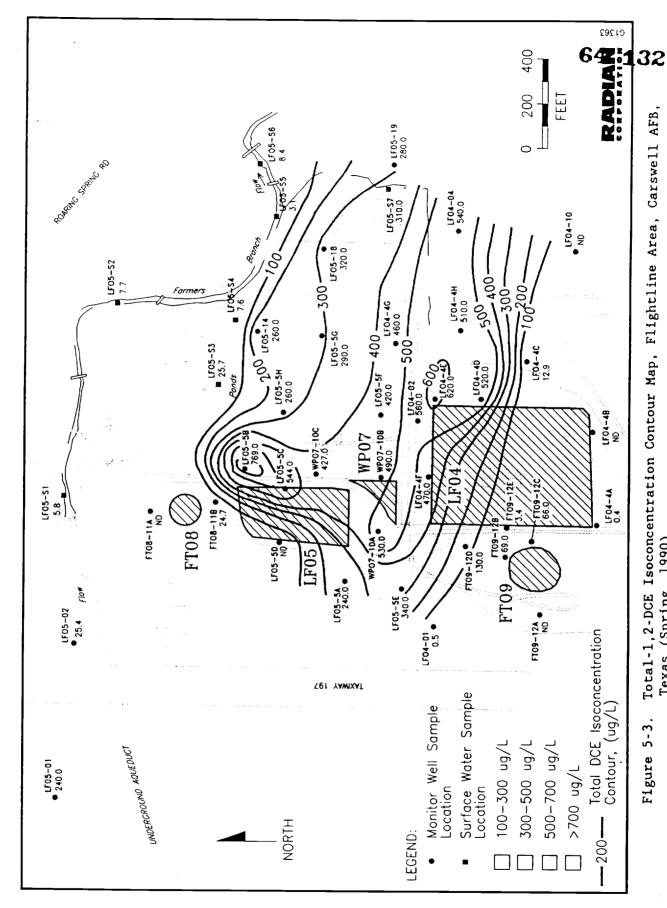


Figure 5-1. Potential Degradation Products and Reaction Mechanisms for Reduction of Chlorinated Ethanes and Ethylenes

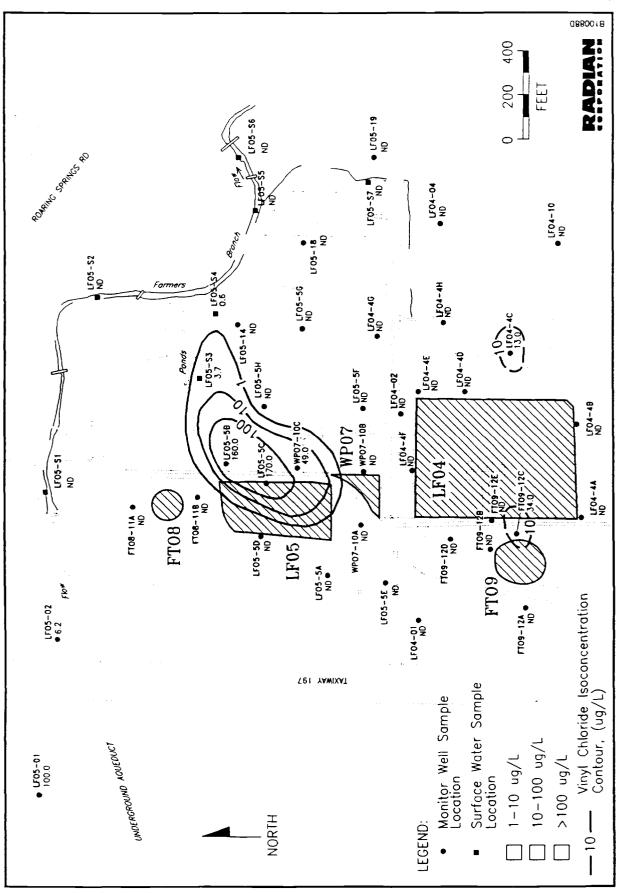


TCE Isoconcentration Contour Map, Flightline Area, Carswell AFB Texas (Spring, 1990) Note: Figure will be colored in Final Report Figure 5-2.



Total-1,2-DCE Isoconcentration Contour Map, Flightline Area, Carswell AFB, Texas (Spring, 1990) Note: Figure will be colored in Final Report

5-7



Vinyl Chloride Isoconcentration Contour Map, Flightline Area, Carswell AFB, Texas (Spring, 1990) Figure will be colored in Final Report Note: Figure 5-4.

- A small irregular area of elevated TCE concentrations is present around monitor well LF05-14, downgradient from Landfill 5 (Site LF05);
- The 1,2-DCE (Figure 5-3) plume has highest concentrations immediately downgradient from Sites LF05 and LF04, with gradually decreasing concentrations downgradient of both landfills; and
- Finally, vinyl chloride is present almost exclusively hydraulically downgradient of Site LF05.

If 1,2-DCE and vinyl chloride concentrations detected in the ground water are directly the result of TCE degradation, then a comparison of the locations and concentration distributions within the plumes suggests an earlier introduction of TCE from Site LF05 into shallow ground water, with significant degradation to 1,2-DCE and vinyl chloride having occurred, and a later release from Site LF04, where time has allowed only degradation to 1,2-DCE to occur. Furthermore, the overall release of contaminants from Site LF04 may have decreased somewhat with time, as concentrations of TCE immediately downgradient from Site LF04 were lower than in the previous sampling in April 1988.

The fact that cis-1,2-DCE is favored in the chemical breakdown of TCE supports the hypothesis that all of the 1,2-DCE present in the Flightline Area results from TCE degradation. As stated earlier, cis-1,2-DCE is present in concentrations far exceeding trans-1,2-DCE, and the compound was detected in five times as many wells. This would be expected if the two compounds were daughter products of TCE, as the breakdown pathways of TCE to trans-1,2-DCE or 1,1-DCE are considered minor. However, all of the interpretations in this section are speculative. Review of the historical ground-water chemical data from the Flightline Area indicates considerable variability in concentrations of volatile organic compounds over short periods (i.e., between monthly sampling rounds). These fluctuations are unlikely to be related to longer-term degradation patterns.

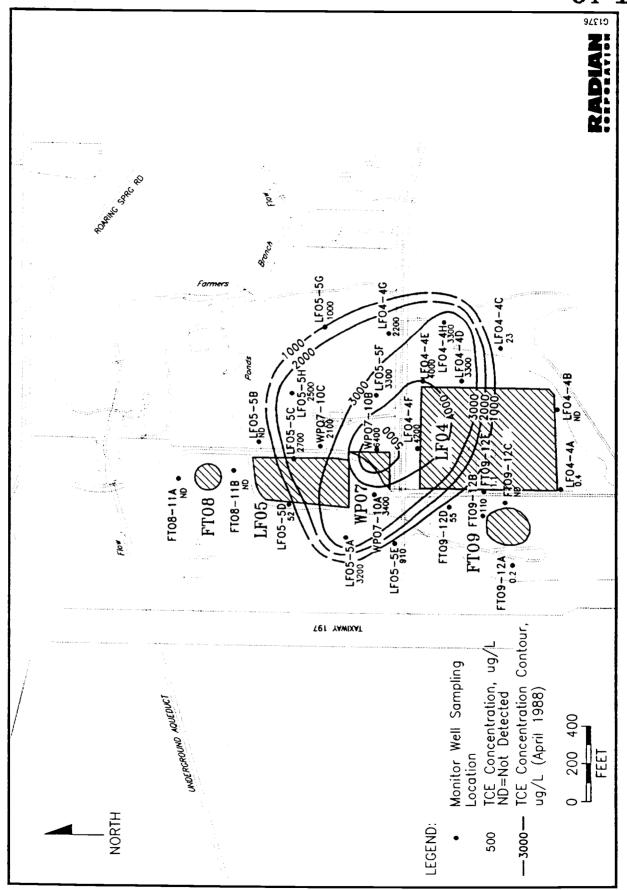
5.2 <u>Contaminant Migration Pathways</u>

Ground water and surface water at the Flightline Area appear to be in hydraulic communication, based on results of synoptic water level measurements, and supported by chemical analyses from surface-water and ground-water samples. The water quality indicator compounds in each system were similar, and the detected contaminants occurred in similar proportions. Ground-water contaminants TCE and 1,2-DCE were also detected in each surface-water sample. In addition, as discussed in Section 4, the concentrations of TCE and 1,2-DCE detected at surface-water sampling points were consistent with contaminant concentrations at nearby ground water sampling locations. These correlations support hydraulic connection between ground water and surface-water systems. Furthermore it is apparent that the tributary to Farmers Branch is a point of ground-water discharge which ultimately contributes contaminated water to Farmers Branch. To simplify the discussion of contaminant transport, the migration of the contaminant plume will be described individually in terms of the ground-water and surface-water systems.

5.2.1 Transport in Ground Water

Comparison of Figures 5-2 (Spring 1990) and 5-5 (April 1988) showing TCE concentrations in ground water suggests that some migration of the TCE plume has occurred. Recognizing that the interpreted isoconcentration contours can partially reflect sampling and analytical variabilities, the apex of the plume, once centered on monitor well WPO7-10B, is now centered between monitor wells LF04-4G and LF04-02. If this change is attributed to advection, it represents a migration distance of dissolved TCE of several hundred feet.

Data generated from Upper Zone Aquifer pump testing, performed in June 1990, and water-level data suggest the average ground-water flow rate in the Upper Zone is approximately 9 feet per day. This is based on a hydraulic conductivity of 785 feet/day and an hydraulic gradient of 0.0035. Since the hydraulic conductivity derived from aquifer testing falls in the suggested



Isoconcentration Contour Map of TCE Concentrations from April 1988 Upper Zone Ground-Water Sampling, Flightline Area, Carswell AFB, Texas (Radian, 1989) Figure 5-5.

range for clean sands to gravels (Freeze and Cherry, 1979), a porosity of 30% was assumed. The estimate for the average ground-water flow velocity is derived from a simplification of Darcy's Law:

$$\bar{v} = \frac{Ki}{\phi}$$

where:

v = average ground-water flow velocity

K - hydraulic conductivity of Upper Zone Aquifer (average 2.8×10^{-1} cm/sec or 785 feet/day),

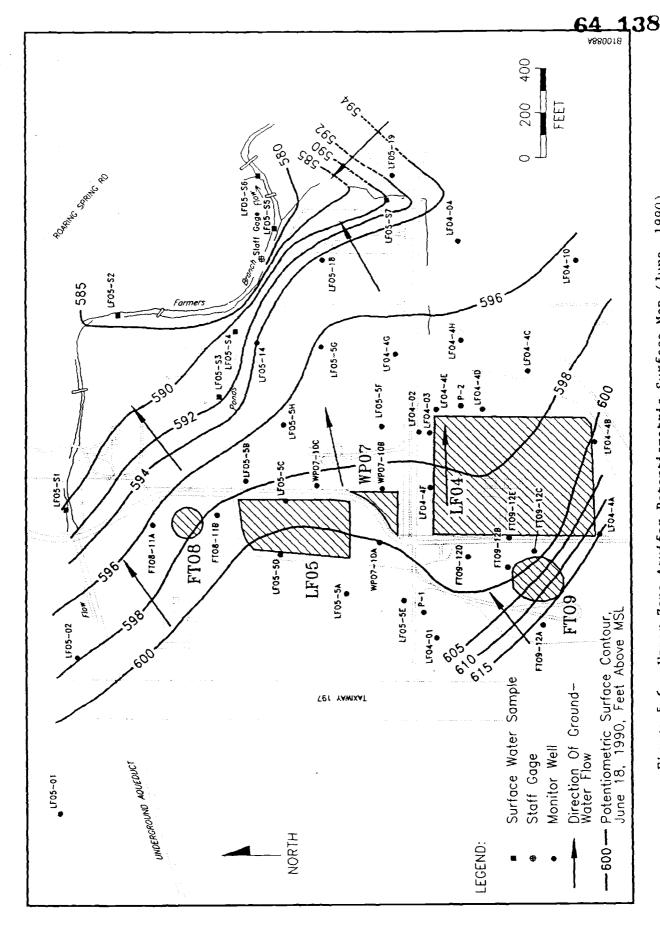
i - hydraulic gradient (0.0035) in the Upper Zone; and

 ϕ = estimated porosity of the Upper Zone deposits (0.30).

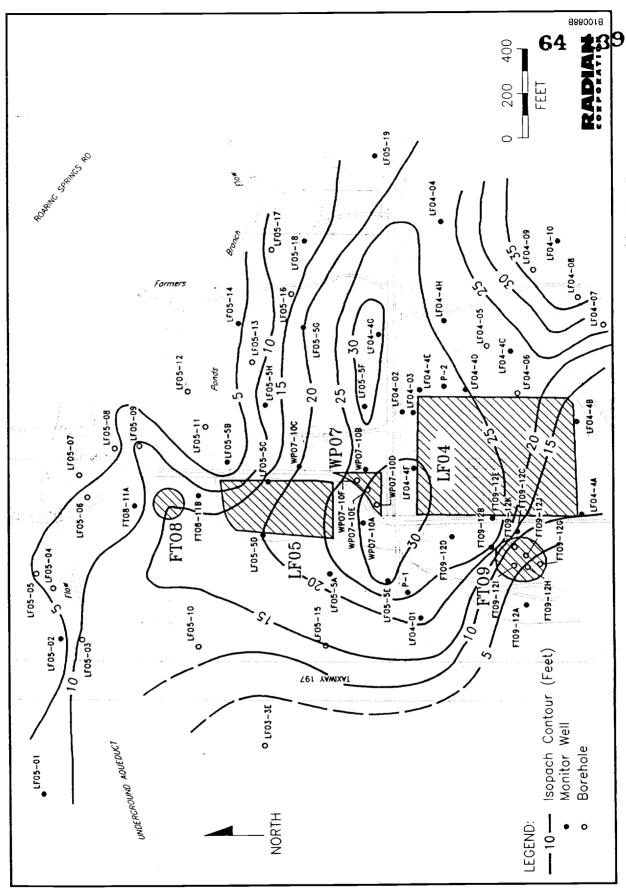
Based on this calculation, the position of the TCE plume is migrating approximately an order of magnitude slower than ground water flow. This is not unusual based upon the physical, chemical and biological factors which affect the solute mobility with respect to ground water, as previously discussed in Section 5.1.

The main contaminant plume appears to be migrating in a direction which is generally consistent with the direction of ground-water flow. Figure 5-6 shows a potentiometric surface map generated from the June 1990 water level survey, with the corresponding ground-water flow directions indicated. The dominant direction of migration closely follows the orientation of the thickest accumulation of sand and gravel in the Flightline Area (Figure 5-7). A comparison of the sand and gravel isopach map with the recent TCE plume map (Figure 5-2) clearly indicates that plume migration may be preferentially influenced by the increased porosity and hydraulic conductivity of the sand and gravel interval.

The direction of plume migration appears to be roughly parallel to White Settlement Road. The maximum extent of the plume in that direction is unknown, as samples from the two most easterly monitoring wells, LF04-04 and LF05-19 had detected levels of 2700 and 1300 μ g/L TCE, respectively, in the Spring 1990 sampling event. However, given historical observations and at the



Upper Zone Aquifer Potentiometric Surface Map (June, 1990), Flightline Area, Carswell AFB, Texas Figure 5-6.



Sand and Gravel Isopach Map, Flightline Area, Carswell AFB, Texas Figure 5-7.

estimated rate of contaminant transport, the apex of the contaminant plume would not be expected to migrate beyond the general locations of LF04-04 and LF05-19 within the next several years.

It is along this vector of migration that the plume most directly intersects the unnamed tributary to Farmers Branch. Both TCE and 1,2-DCE were found in high concentrations in surface-water sample LF05-S7 (collected from the small tributary (Figure 5-2)). At this locality, contaminated ground water appears to discharge directly into the surface water, which in turn flows into Farmers Branch. Because upstream flow in this small tributary intermittently disappears into the subsurface (from the southeast corner of LF04 to just upstream of LF05-S7), it is likely that the water at the sampled location is almost entirely the result of ground-water discharge. However, as evident from Figure 5-2, the tributary is not a ground-water flow boundary and thus all ground-water contamination in the vicinity of the small tributary is not 'captured' or diverted as surface-water flow. This conclusion is also supported by the finding of elevated concentrations of TCE and 1,2-DCE in wells hydraulically downgradient of the tributary. This is most evident on the south side of White Settlement Road, where TCE was detected at 2700 $\mu g/L$ in monitor well LF04-04, south (downgradient) of the small tributary. Also, test well LF05-19 is located east of the unnamed tributary and has a TCE concentration of 1300 μ g/L. Migration of a portion of the contaminants continues in an east-southeasterly direction past the location of LF04-04.

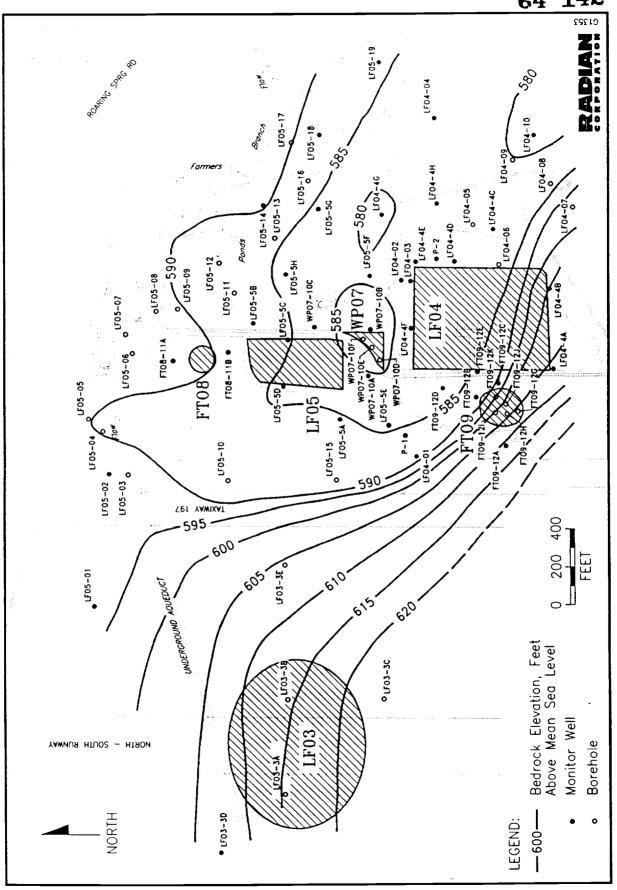
The more northerly component of the TCE plume migration, which parallels the direction of ground-water flow, is toward Farmers Branch. Farmers Branch was sampled at four locations in the Spring 1990 sampling event. While the dominant ground-water flow is in the direction of Farmers Branch, the main contaminant plume has not indicated a strong preferential migration in that direction. TCE concentrations of 1.8 and 4.5 μ g/L, found in surface-water samples collected in two small ponds located immediately north of monitor well LF05-14, appear to approximate the northerly extent of the TCE plume. Any potential contaminant migration to the east of these ponds would be intercepted by Farmers Branch. Since no samples have been collected on the opposite side (northern) of Farmers Branch, it is uncertain whether the ground

water on that side of the stream is contaminated. Contamination in Farmers Branch and the unnamed tributary to Farmers Branch is discussed in Section 5.2.2, below.

TCE has not been encountered as a dense non-aqueous phase liquid (DNAPL) in monitor wells installed in the Flightline Area, however, if DNAPL does exist, it would tend to sink due to the difference in specific gravity between TCE and water. Figure 5-8 depicts a structural contour map drawn on the top of the Goodland/Walnut Formation, which is the aquitard beneath the Upper Zone and considered to be the limit of vertical contamination. It is probable that migration of any DNAPL would be influenced by the configuration of the top of the aquitard. The solubility of TCE in water is 1100 mg/L, and based on the analyses received from the various sampling efforts, concentrations sufficient to warrant the presence of TCE as a DNAPL are not expected in the Flightline Area. While TCE may have been released in a pure phase from one of the source sites, immediate and extensive dilution occurs as the leachate enters the ground water, as reflected in the TCE concentrations detected in downgradient wells. Based on the concentrations of contaminants detected in the Flightline Area contaminant plume, the density of the water would not be expected to be much greater than that of fresh water. However, preferential migration of the contaminant plume through the thickest Upper Zone sand and gravel deposits and above the most eroded surfaces of the underlying aquitard is occurring in the Flightline Area.

5.2.2 <u>Transport in Surface Water</u>

Surface-water contamination in the Flightline Area is affected by both the extent and migration of the ground-water plume, and by the variations in the discharge and velocity of the two principal surface-water bodies occurring in the area. Farmers Branch, which ultimately flows off-site, had variable concentrations of TCE and 1,2-DCE based on the sample location. In addition, the Farmers Branch is fed by the small unnamed tributary draining the southern portion of the study area, from which the most highly contaminated surface-water samples were collected. As a consequence, surface-water contaminant transport will be considered exclusively in terms of Farmers

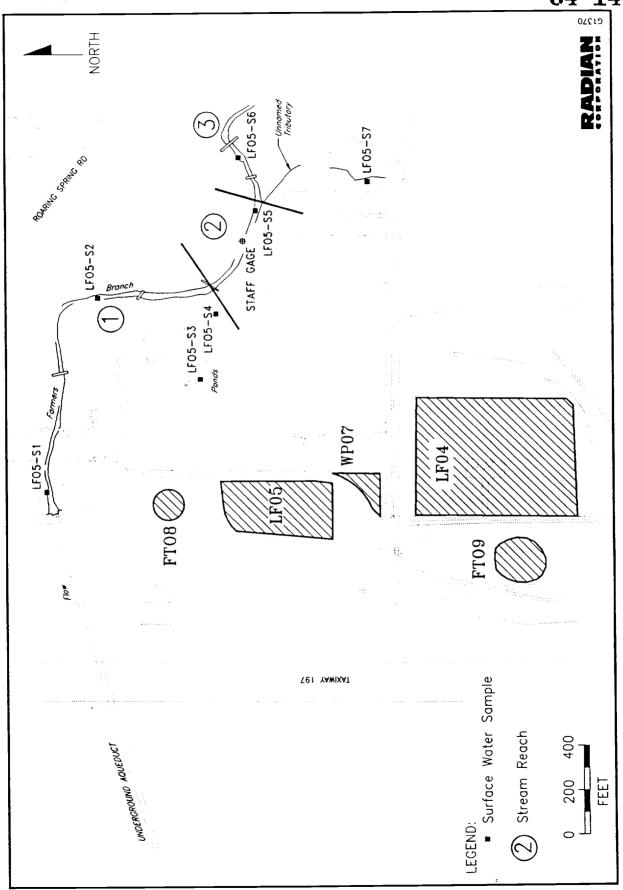


Elevation (MSL) of the Top of the Goodland/Walnut Formation, Flightline Area, Carswell AFB, Texas Figure 5-8.

Branch. For the purpose of this discussion, Farmers Branch will be divided into three reaches, each with a different contaminant input and potential for contaminant migration.

Figure 5-9 shows the location of the surface-water sampling sites and identifies the three divided reaches of Farmers Branch. The first reach of Farmers Branch includes the upstream portion from the end of the concrete underground aqueduct to the waterfall adjacent to the golf course ponds. This section of Farmers Branch is not influenced by the main TCE plume, as the golf course ponds are located approximately at the northern edge of the plume. TCE was detected, however, in the two samples collected in this reach. The TCE in these samples is believed to be the result of the upgradient source previously mentioned in this report. While the TCE detected in this portion of Farmers Branch is significantly above federal primary drinking water standards, it is probable that contamination observed in this reach does not contribute greatly to the overall observed downstream concentration of TCE. It is probable that a large percentage of all volatile organic contaminants (including TCE and 1,2-DCE) are stripped from the stream by volatilization as the stream crosses the waterfall which separates the first reach from the second reach.

The second designated reach of Farmers Branch includes that portion which is downstream of the waterfall and upstream of the intersection of Farmers Branch and the small tributary. In this reach, the main TCE plume appears to intersect the stream, and both TCE and 1,2-DCE contamination was detected in sample LF05-S5. However, even with continued migration of the main TCE plume in the direction of Farmers Branch, the concentration detected in this segment of the stream is not expected to increase significantly, and hence is not expected to be a major contributor to downstream contamination. The reason for this is the Upper Zone Aquifer outcrops in a broad cutbank of Farmers Branch across the entirety of this reach, and the ground water is therefore not in direct communication with the stream. Instead, water from the Upper Zone emanates from a series of seeps along the cutbank, and percolates down the face of the cutbank into a series of pools which are located



Surface Water Sampling Points and Three Divided Reaches of Farmers Branch, Flightline Area, Carswell AFB, Texas Figure 5-9.

on limestone bedrock of the Goodland/Walnut Formation. As in the case of the upper reach, this allows for significant volatilization and evapotranspiration to occur, and would consequently strip most of the contaminants from the water prior to any possible mixing with surface water from Farmers Branch. It is likely that minor amounts of contaminants from both reaches may migrate downstream to the third reach.

Significant concentrations of TCE and 1,2-DCE in the ground water (on the order of 1300 μ g/L and 280 μ g/L, respectively) are discharging as surface water in the vicinity of surface-water sample location LF05-S7. This water, in turn, discharges directly into Farmers Branch in the third reach, and constitutes the principal pathway for off-site and off-base migration. Since the unnamed tributary to Farmers Branch is considered equivalent to a direct discharge of the main TCE plume, the discharge of the tributary and also Farmers Branch were calculated to determine the effects of dilution as the two bodies intersect. This was done using the simple relationship:

Q - vA

where: Q = discharge

v - velocity

A = cross-sectional area

Applying this equation to values obtained in the field, the slow moving tributary had a calculated discharge of approximately 0.2 cubic feet per second (cfs) or about 129,000 gallons per day (gpd). In contrast, at the time of field measurement, the discharge of Farmers Branch was approximately 6.0 cfs, or about 3,900,000 gpd. This translates into a dilution factor of about 30, suggesting that contaminant concentrations in Farmers Branch would be thirty times lower than those occurring in the unnamed tributary. Surfacewater sampling results confirmed this, as the TCE concentrations between samples LF05-S7 and LF05-S6 (1400 μ g/L and 43 μ g/L) appear diluted by a factor of 33 and 1,2-DCE concentrations between the same two locations (310 μ g/L at LF05-S7 and 8.4 μ g/L at LF05-S6) appear diluted by a factor of 37.

It may be concluded that as the most highly contaminated portion of ground-water plume continues migrating to the east, the concentrations of organic contaminants detected in the unnamed tributary, and hence in Farmers Branch, may increase proportionately. However, plume degradation by physical, chemical and biological factors may result in transport of contaminants offsite remaining fairly constant over the next few years. Currently, TCE migration off-site in Farmers Branch is estimated at 45 μ g/L and 1,2-DCE migration off-site is estimated at 8.4 μ g/L. There are insufficient data available to estimate the concentration of these contaminants in reaches of Farmers Branch outside the Flightline Area. However, volatilization will reduce the organic contaminant content of Farmers Branch before its ultimate discharge into the Trinity River.

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6.0 BASELINE RISK ASSESSMENT

6.1 <u>Summary of Indicator Chemicals</u>

Sampling and analysis of soil and water in the Flightline Area has resulted in a large number of chemical substances being detected. Conducting a baseline risk assessment that included every detected chemical would be unnecessarily time consuming. The baseline risk assessment of the Flightline Area is therefore based on selected <u>indicator chemicals</u> that pose the greatest potential risks at the site, a methodology endorsed by the U.S. EPA for evaluation of the health impacts of waste sites (U.S. EPA, 1986a).

Indicator chemicals were selected from approximately 80 chemicals known to be present at the site according to <u>Health Evaluation Manual</u> (U.S. EPA, 1986a). The selection process, based in both 1988 and 1990 sampling and analyses performed on the soil, ground water, and surface water in the Flightline Area, resulted in the following list of indicator chemicals:

<u>Metals</u>	Semivolatile Organic Compounds	Volatile Organic Compounds (VOCs)
Antimony	Bis(2-ethylhexyl)- phthalate	Benzene
Arsenic	•	Chloroform
Barium		1,2-Dichloroethane
Beryllium		Methylene chloride
Cadmium		Tetrachloroethene
Chromium		Toluene
Lead		Trichloroethene
Nickel		Vinyl chloride
Selenium	•	
Silver		

Some of the indicator chemicals, particularly those detected at very low concentrations, may be the result of matrix interferences or sample cross-contamination. No analysis for semivolatile compounds was performed in 1990 and the low levels of phthalate detected previously are suspected as

being artifacts of sampling or laboratory contamination. As already discussed, dissolved metals concentrations in ground water and surface water samples, determined only in the 1990 effort, were all below MCLs and do not suggest a metals contamination problem. Nevertheless, all of the identified indicator chemicals were included in the risk assessment process to ensure a conservative (stringent-case) evaluation of possible health risks.

6.2 <u>Source and Release Characterization</u>

Possible mechanisms of contaminant release from Landfill 4 (LFO4), Landfill 5 (LFO5) and the Waste Burial Area (WPO7) include: 1) volatilization to the air, 2) fugitive dust generation, 3) leachate to ground water, 4) surface runoff, 5) direct release to surface water, and 6) contaminated ground-water discharge to surface water.

6.2.1 <u>Volatilization to the Air</u>

VOCs present in the soil are subject to volatilization to the air by virtue of high vapor pressures. Semivolatile organic compounds generally have very low vapor pressures and are not subject to volatilization. Most metals are nonvolatile as well. Indicator chemicals detected in the Flightline Area which can volatilize include benzene, chloroform, 1,2-dichloroethane, methylene chloride, tetrachloroethene, toluene, trichloroethene, and vinyl chloride.

Estimated emission rates based conservatively on maximum concentrations detected in the soil or water samples from the Flightline Area are:

Indicator Chemical	Emission Rate (grams/second)
Benzene	2.25×10^{-5}
Chloroform	1.58×10^{-6}
1,2-Dichloroethane	1.07×10^{-7}
Methylene chloride	2.85×10^{-5}
Tetrachloroethene	1.25×10^{-7}

Toluene 6.79×10^{-7} Trichloroethene 3.22×10^{-4} Vinyl chloride 7.51×10^{-5}

The methodology used to estimate emission rates is described in the IRP Stage 2 RI/FS Final Draft Report (Radian, 1989).

6.2.2 Fugitive Dust Generation

Contaminants must be present in exposed soil to be subject to fugitive dust generation. Because wastes in these IRP sites are buried and the surface is vegetated, contaminants present in the soil are not subject to significant fugitive dust generation.

6.2.3 Leachate to Ground Water

Indicator chemicals detected in ground-water samples from downgradient monitor wells in the Flightline Area include: antimony, arsenic, barium, beryllium, cadmium, chromium, lead, nickel, selenium, silver, bis(2-ethylhexyl)phthalate, benzene, chloroform, methylene chloride, tetrachloroethene, toluene, trichloroethene, and vinyl chloride.

6.2.4 <u>Surface Runoff</u>

Contaminants must be exposed at the land surface to be subject to significant surface runoff during precipitation. Because Landfill 4 and the Waste Burial Area were covered and vegetated after disposal operations ceased, and because both are relatively flat, contaminants present in the soil are not subject to significant surface runoff. Landfill 5 was also covered and vegetated after disposal activities ceased. However, because Landfill 5 was constructed above ground level and is adjacent to the small tributary to Farmers Branch, there is a greater potential for surface runoff of contaminants than for the other two sites.

6.2.5 <u>Discharge to Surface Water</u>

There is no direct discharge of contaminants to surface water. However, there is indirect discharge in the form of contaminated ground water discharging to Farmers Branch, the small tributary, and the two golf course ponds in the Flightline Area.

6.3 Transport and Fate of Contaminants

The Flightline Area sites potentially release VOCs to the air via volatilization and all identified indicator chemicals to the ground water via waste leaching. The main mechanism for contaminant release to surface water is by Upper Zone ground-water discharge. Potentially significant contaminant transport and fate mechanisms in the air and ground-water media include: 1) air dispersion, 2) ground-water migration, 3) discharge to the surface, 4) transport in surface water, and 5) subsequent uptake by plants and animals.

6.3.1 Air Dispersion

Emission of VOCs from the Flightline Area IRP sites occurs at ground level in the gaseous phase. The gases disperse in the ambient atmosphere according to local meteorological conditions. Annual ambient air concentrations of the volatile organic indicator chemical emissions were estimated using the ISCLT model. The dispersion modeling methodology is discussed in the IRP Stage 2 RI/FS Final Draft Report (Radian, 1989).

6.3.2 Ground-Water Migration

In the Flightline Area, ground water in the Upper Zone occurs in sand and gravel deposits that are underlain by relatively impermeable and dry limestone/shale bedrock. Hydraulic head in the Upper Zone Aquifer decreases toward Farmers Branch, indicating that ground-water flow is also toward Farmers Branch. The bed of Farmers Branch is cut into the same bedrock that forms the base of the Upper Zone; therefore ground water is expected to discharge directly to Farmers Branch or to be consumed by evapotranspiration

as it exits the Upper Zone materials near the creek. This in fact is the case as ground water is continually seeping from the cut-bank face of the creek and ponding on the limestone bedrock that forms the creek bed. Ground-water flow is generally not toward the base perimeter in this area. Therefore, migration of contaminants from the Flightline Area to any domestic or agricultural use wells in the area is unlikely.

6.3.3 <u>Transport in Surface Water</u>

Since VOCs remain in a gaseous state and do not deposit on the ground, surface water in the area is not subject to contamination via emissions to the air from the Flightline Area. Contaminants which reach Farmers Branch via ground-water migration (or surface runoff from Landfill 5) are subject to dilution and movement with the surface flow downstream to the West Fork of the Trinity River located east of the base. The West Fork of the Trinity River is downstream of Lake Worth, which is the source of drinking water for Fort Worth and Carswell AFB. Thus the path of surface water drainage precludes the transport of contaminants from the Flightline Area to the sole surface water source of drinking water in the area. Any VOCs present in surface water would probably volatilize to the air, thus leading to decreasing VOC concentrations with increasing distance downstream.

6.3.4 Uptake by Plants and Animals

Food crops, including commercial agricultural crops and backyard gardens, are subject to accumulation of contaminants migrating from the Flightline Area IRP sites via root uptake of any contaminants present in the water used for watering or irrigation. Migration of ground water to a surface water source used for watering or irrigation is the only significant pathway for contaminants to move from the Flightline Area to plants. However, farming operations in the area generally rely on natural precipitation or irrigation of crops with ground water (South, J., 1988), which eliminates this potential pathway for human exposure. Since emissions to the air from the Flightline Area would be limited to VOCs which remain in a gaseous state in ambient air,

they will not deposit on above-ground plant surfaces or on the soil or surface water so as to be available for root uptake.

Terrestrial organisms, including farm animals and wildlife, are potentially subject to accumulation of contaminants originating in the Flightline Area sites by: 1) inhalation of ambient air, and 2) ingestion of surface water contaminated via ground-water migration. As discussed above, farm operations in the area do not use surface water to irrigate crops. Therefore, farm animals are not subject to ingestion of plants irrigated or watered with surface water contaminated via ground-water discharge.

Aquatic organisms, including fish, are subject to accumulation of contaminants by uptake from surface water contaminated via ground-water discharge/surface transport. Contaminants can bioaccumulate in the food chain of both terrestrial and aquatic organisms.

6.4 Exposure Pathways

Figure 6-1 depicts potential pathways for contaminants to move from the Flightline Area to human exposure points. Pathways which are not complete were eliminated. Remaining pathways include:

- 1. Volatilization to the air/air dispersion/inhalation of ambient air:
- Volatilization to the air/air dispersion/inhalation by animals/ingestion of meat and dairy products;
- 3. Leaching to ground water/ground-water migration to surface water (fishable source)/uptake by fish and other aquatic organisms/ingestion of aquatic organisms;
- 4. Leaching to ground water/ground-water migration to surface water (agricultural use source)/ingestion by animals/ingestion of meat and dairy products;

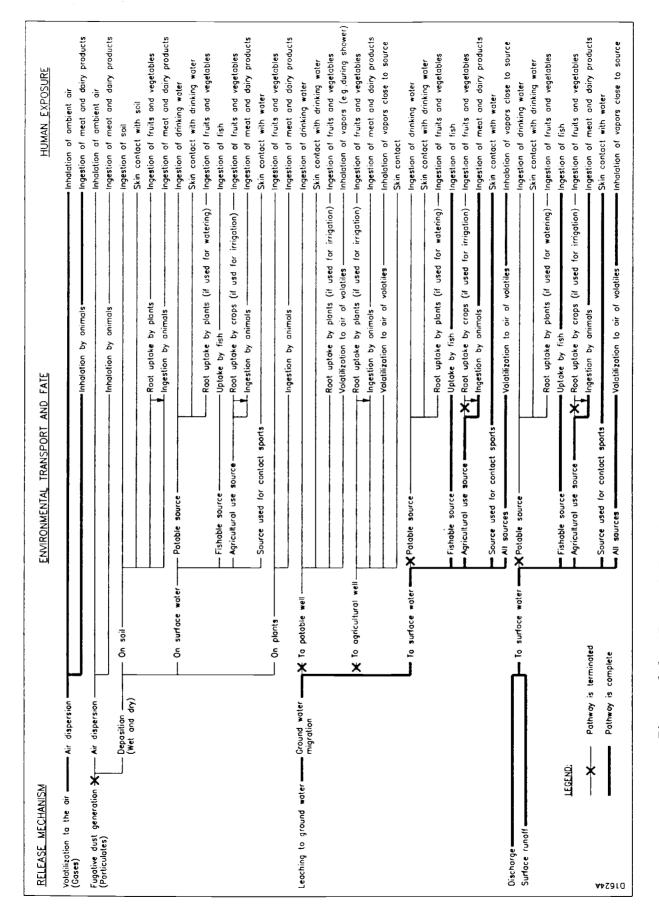


Figure 6-1. Potential Pathways to Human Exposure from the Flightline Area

- 5. Leaching to ground water/ground-water migration to surface water (source used for contact sports)/skin contact with water; and
- 6. Leaching to ground water/ground-water migration to surface water/volatilization of volatiles/inhalation of vapors close to source.

Contaminant contributions to surface water used for fishing, for agriculture, for contact water sports, or from which VOCs can volatilize, can also potentially result from surface runoff from Landfill 5 to a Farmers Branch tributary.

6.5 Identification of Receptors

Based on available exposure pathways, potential human receptors for exposure to contaminants migrating from the Flightline Area include: 1) persons residing and/or working in nearby areas, particularly downwind of the site; 2) persons ingesting meat and dairy products from animals exposed to contaminants in the ambient air or contaminated surface water; 3) persons ingesting fish or other aquatic organisms exposed to contaminated surface water; and 4) persons swimming or participating in other contact sports in contaminated water.

Potential wildlife receptors include: 1) terrestrial organisms with habitats close to the Flightline Area that inhale ambient air and ingest surface water, particularly from Farmers Branch, its unnamed tributary and/or the golf course ponds, and 2) aquatic organisms in the on-base surface water bodies and the West Fork of the Trinity River.

6.6 Quantification of Exposures

6.6.1 <u>Inhalation Exposure</u>

Inhalation of ambient air is the most direct exposure pathway for contaminants to move from the Flightline Area to human receptors. Table 6-1 presents the on-site maximum and off-site maximum predicted annual ambient air concentrations resulting from estimated Flightline Area emissions, and predicted concentrations at several discrete locations: site of the proposed base day care center, which is central to the largest on-base residential area, the Fort Worth National Fish Hatchery, and the closest dairy and beef operations. The table also lists Texas Air Control Board (TACB) Health Effects Screening Levels (ESLs) which the agency uses to evaluate the impacts of air contaminants. TACB screening levels are based on occupational exposure limits [American Conference of Governmental Industrial Hygienists (ACGIH) Threshold Limit Values (TLVs), Occupational Health and Safety Administration (OSHA) standards, or National Institute for Occupational Safety and Health (NIOSH) recommendations], odor nuisance potential, vegetation effects, or corrosion effects. Generally the annual ESL corresponds to 0.1% of the lowest occupational exposure limit.

The maximum predicted annual average concentrations resulting from estimated Flightline Area emissions for benzene, chloroform, 1,2-dichloroethane, methylene chloride, tetrachloroethene, toluene, trichloroethene, and vinyl chloride are lower than the conservative TACB Effects Screening Levels by orders of magnitude ranging from 4 to 8.

6.6.2 Ingestion Exposure

Potential ingestion exposures include ingestion of meat and dairy products from animals exposed to contaminants in the ambient air or contaminated surface water, and fish exposed to contaminated surface water. The Flightline Area contributes very low concentrations of VOCs to the ambient

PREDICTED ANNUAL AVERAGE AMBIENT AIR CONCENTRATIONS RESULTING FROM ESTIMATED FLIGHTLINE AREA EMISSIONS® TABLE 6-1.

	Predicted		Average Amb	ient Air Cor	Annual Average Ambient Air Concentration (ug/m³)	(ug/m³)	
Contaminant	On-Site Maximum	Off-Site Maximum	Day Care	Fish Hatchery	Dairy Operation	Beef Operation	TACB Annual Effects Screening Level ^b (ug/m^3)
Benzene	2.3×10 ⁻⁴	3.2×10 ⁻⁵	7.2x10-5	9.7×10 ⁻⁷	2.0x10 ⁻⁷	7.3x10 ⁻⁸	3
Chloroform	8.7x10 ⁻⁶	8.8×10^{-7}	2.4x10 ⁻⁶	5.5×10 ⁻⁸	1.1x10 ⁻⁸	4.0x10 ⁻⁹	10
1,2-Dichloroethane	1.1x10 ⁻⁶	1.5×10^{-7}	3.4×10^{-7}	4.6x10 ⁻⁹	<10.	<10.9	7
Methylene chloride	1.6x10 ⁻⁴	1.6x10 ⁻⁵	4.4×10-5	9.9×10 ⁻⁷	2.8×10 ⁻⁷	7.5x10 ⁻⁸	26
Tetrachloroethene	$6.9x10^{-7}$	6.9x10 ⁻⁸	1.9×10^{-7}	4.0x10-9	1.0x10°9	<10-9	33.5
Toluene	9.1x10.6	4.8×10 ⁻⁷	1.3×10.6	3.3×10 ⁻⁸	7.0x10°9	3.0x10 ⁻⁹	375
Trichloroethene	3.6×10^{-3}	2.3×10 ⁻⁴	5.9×10 ⁻⁴	1.5×10-5	3.1×10 ⁻⁶	1.1x10 ⁻⁶	135
Vinyl chloride	1.6×10 ⁻³	3.1×10 ⁻⁵	6.5×10 ⁻⁵	3.0×10 ⁻⁶	6.0x10 ⁻⁷	2.1x10 ⁻⁷	10

*Individual contributions from Landfill 4, Landfill 5, and the Waste Burial Area, as reported in Radian, 1988 have been added to derive estimated annual average ambient on concentrations associated with the Flightline Area.

^bNovember 15, 1990.

air. At the sites of the nearest dairy and beef operations, concentrations are predicted on the order of $10^{-7}~\mu g/m^3$ and lower (see Table 6-1). Although cows will absorb inhaled VOCs, these compounds do not tend to accumulate in milk or edible tissues which humans might consume. Likewise, livestock consumption of surface water containing contaminants originating from the Flightline Area is theoretically possible, if livestock consumes water from the West Fork of the Trinity River; however, any exposure can be expected to be minimal due to the distance from Carswell AFB to the nearest dairy and beef operations. Consumption of locally produced beef and dairy products therefore does not represent a significant pathway of human exposure to contaminants originating from the Flightline Area.

The most significant fishable resource in the vicinity of Carswell AFB is Lake Worth. The Fort Worth National Fish Hatchery is located at the western end of the lake. Since there is no available pathway for contaminants to move from the Flightline Area to Lake Worth, there is no potential for human exposure to contaminants originating at the Flightline Area via ingestion of fish caught in the lake. There is some theoretical potential for fish in the West Fork of the Trinity River to accumulate contaminants from the Flightline Area in the area downstream of the intersection of Farmers Branch with the river. However, contaminant contributions to the river from the Flightline Area via contaminated ground-water discharge to Farmers Branch are likely to be very minimal due to the distance between the site and the river (approximately one mile), dilution, volatilization, and the low concentrations of contaminants in ground water. Therefore, concentrations of contaminants in the river which originate from the Flightline Area were not established.

6.6.3 <u>Dermal Exposure</u>

The potential for skin contact with contaminants originating from the Flightline Area is limited to exposure while swimming in (or otherwise in contact with) contaminated surface water. Lake Worth is the most highly utilized surface water body for swimming and other water contact sports in the area. Again, since there is no available pathway for contaminants to move from the Flightline Area to Lake Worth, there is no potential for human

exposure to contaminants originating from the Flightline Area via skin contact with lake water. As discussed above, contaminant contributions to the West Fork of the Trinity River from the Flightline Area are theoretically possible but likely to be very minimal; therefore, skin contact with river water is not considered a significant exposure pathway for this site. Skin contact with water in Farmers Branch, which is not amenable to swimming or other contact activities other than possibly wading, could contribute to dermal exposure. The exposure potential from this pathway was not quantified.

6.7 Threat to Human Health

6.7.1 Noncarcinogenic Risks

Table 6-2 shows estimates of average daily inhalation exposure (in mg/kg body weight/day) at the location of the on-site and off-site maximum predicted annual average concentration, and at the proposed on-site day care facility, and compares these values with inhalation Reference Doses (RFDs) for chronic (long-term) exposure. An inhalation RFD is an estimate of the dose of a chemical that can be inhaled daily for a lifetime without producing adverse noncarcinogenic health effects. The derivation of RFDs (Formerly Acceptable Daily Intakes--ADIs) used in this assessment is discussed in the IRP Stage 2 RI/FS Final Draft Report (Radian, 1989).

Average daily inhalation exposures for benzene, chloroform, 1,2-dichloroethene, methylene chloride, tetrachloroethene, toluene, trichloroethene, and vinyl chloride are lower than pollutant-specific RFDs in all cases by more than three orders of magnitude. The total hazard index is significantly less than one at all sites, indicating that the threat of noncarcinogenic health effects of inhalation exposure to contaminants originating from the Flightline Area is not significant.

ESTIMATED ANNUAL AVERAGE DAILY INHALATION EXPOSURES FOR CONTAMINANTS FROM THE FLIGHTLINE AREA TABLE 6-2.

		On-Site Maximum	x i mum	Off-Site Maximum	(ax i mun	Day Care	are
Contaminant	Inhalation Reference Dose ^a (mg/kg/day)	Inhalation Exposure ^c (mg/kg/day)	Hazard Index ⁴	Inhalation Exposure ^c (mg/kg/day)	Hazard Index	Inhalation Exposure ^b (mg/kg/day)	Hazard Index ^c
Benzene	3.2×10-16	6.57×10-	2.01×10 ⁻⁷	9.14×10 ⁻⁹	2.86×10-	2.01×10-	6.43×10-
Chloroform	1.0x10 ⁻²	2.48×10-*	2.43×10 ⁻⁷	2.53×10 ⁻¹⁰	2.53×10 ⁻⁹	6.95×10 ⁻¹⁰	6.95x10-
1,2-Dichloroethane	2.7×10-30	3.14×10 ⁻¹⁰	1.16×10-7	4.29×10-11	3.30×10-	9.7×10 ⁻¹¹	7.47×10-
Methylene chloride	8.6×10-1	4.48×10-	5.21×10-	4.56×10-*	5.30×10-9	1.25×10-	1.45×10-
Tetrachloroethene	1.0×10 ⁻²	1.96×10 ⁻¹⁹	1.96×10-	2.00×10 ⁻¹¹	2.00×10.*	5.50×10 ⁻¹¹	5.50×10-9
Toluene	5.7×10-1	2.60×10-*	4.56×10 ⁻⁹	1.37×10 ⁻¹⁰	2.41×10 ⁻¹⁹	3.71×10 ⁻¹⁰	6.52×10 ⁻¹⁰
Trichloroethene	2.46×10-25	1.02×10-*	4.18×10 ⁻⁵	6.57×10*	2.67×10-*	1.68×10-7	6.85×10-
Vinyl chloride	1.3×10 ⁻³⁰	4.51×10 ⁻⁷	3.47×10-4	8.86×10.	6.81×10.	1.86×10-	1.43×10-5
TOTAL HAZARD INDEX			3.89×10-4		9.55×10-		2.14×10 ⁻⁵

Estimate of the dose of a chemical that can be inhaled dally for a lifetime without producing adverse noncarcinogenic health effects.

Derived for this assessment (see Radian, 1989).

'Inhalation exposure assumes inhalation for 24 hours/day of predicted annual average ambient concentrations by an individual with an average body weight of 70 kg and with an average inhalation rate of 20 m²/day.

'Inhalation Exposure/Inhalation Reference Dose.

6.7.2 <u>Carcinogenic Risks</u>

Inhalation Risk--Of the eight indicator chemicals that might be released to the air from the Flightline Area, seven are potential carcinogens. These are: benzene, chloroform, 1,2-dichloroethane, methylene chloride, tetrachloroethene, trichloroethene, and vinyl chloride. Cancer potency estimates developed by EPA were used in conjunction with total daily contaminant doses to develop estimates of incremental individual cancer risk:

Individual Cancer Risk - Total Daily Dose x Cancer Potency
(mg/kg/day) (mg/kg/day)⁻¹

Incremental individual cancer risk is the increased probability of developing cancer in one's lifetime.

Table 6-3 shows estimates of incremental individual cancer risk for the maximum on-site and maximum off-site exposed individual and for an individual inhaling ambient concentrations in the immediate vicinity of the proposed day care facility continuously for a lifetime. These risks, the highest of which is one in 10 million, can be dismissed as inconsequential.

<u>Ingestion Risk</u>--The potential for ingestion exposure to contaminants originating from the Flightline Area is remote and likely to be minimal. The risk of ingestion exposure was therefore not quantified.

<u>Dermal Risk</u>--The potential for dermal exposure to contaminants originating from the Flightline Area is also minimal. Unless an individual immersed frequently in the waters of Farmers Branch for a long period of time, skin contact exposure can be considered insignificant. The risk of dermal exposure was therefore not quantified.

6.8 Threat to Wildlife

Contaminants migrating from the Flightline Area, as discussed previously, pose some risk to terrestrial wildlife that use Farmers Branch,

ESTIMATED INDIVIDUAL CANCER RISK ASSOCIATED WITH INHALATION OF POTENTIAL CARCINOGENS FROM THE FLIGHTLINE AREA TABLE 6-3.

	Inhalation		Individual Cancer Risk ^b	
Contaminant	Slope Factor* (mg/kg/day) ⁻¹	On-Site Maximum Exposed Individual	Off-Site Maximum Exposed Individual	Individual Exposed at Day Care Facility
Benzene	2.9x10 ⁻²	1.9x10-*	2.7x10-10	01-01-88 P
Chloroform	8.1×10 ⁻²	2.0x10 ⁻¹⁶	2.0x10-11	5.6×10-11
1,2-Dichlorethane	9.1×10-2	2.9x10-11	3.9×10-12	0.0000
Methylene chloride	1.4x6-2	6.3×10'10	6. 4×10-11	01-01-0
Tetrachloroethene	1.8×10 ⁻³	3.5x10-13	41-01-7 E	: 01x0:T
Trichloroethene	1.7x10-2	1.7x10-0	0.0XL0	9.9 x1 0-x
Vinyl chloride	2.9×10 ⁻¹	1.3×10.7	2.6x10-	2.0X10 5.4×10°
TOTAL 70 Year Risk		1.5x10-7	4.1x10-*	e-01×6

"See the IRP Stage 2 RI/FS Report (Radian, 1989) for discussion and documentation. Some values have been revised by EPA and revised values have been used.

'Risk calculation assumes inhalation for 24 hours/day for a 70 year lifetime of predicted annual average ambient concentrations by an individual with an average body weight of 70 kg and with an average inhalation rate of 20 m³/day.

its small tributary, and the golf course ponds as a source of drinking water, as well as aquatic organisms in these surface water bodies. In the past, there have been some instances of fish kills in Farmers Branch and in the small ponds near Building 233. Table 6-4 compares the maximum values of indicator chemicals detected in the Flightline Area surface water samples with EPA water quality criteria (where available) for aquatic life in fresh water.

The only organic indicator chemical that has an established criterion (LOEL - lowest observed effect level) is TCE. The maximum detected concentration of TCE in surface water samples is 15 times less than the chronic LOEL for fresh water aquatic species.

Two metals, lead and silver, were detected in concentrations greater than the ambient fresh water chronic criteria. Silver was detected three times (twice in golf course ponds and once in Farmers Branch). However, all three detectable concentrations occurred in unfiltered samples and all were less than five times the method detection limit. All dissolved silver concentrations were below the method detection limit (10 μ g/L). Because the detection limit is higher than the chronic criterion for aquatic life in fresh water, it is not possible to determine whether any dissolved silver concentrations actually exceeded the chronic criterion.

Lead was detected in all four water samples from Farmers Branch and from one of the golf course ponds. The only detected concentration exceeding the chronic criterion, however, was in the golf course pond sample. The accuracy of the reported lead concentration is questionable as the corresponding dissolved lead concentration was roughly three times greater than the total concentration which did not exceed the chronic criterion. All four samples collected from Farmers Branch contained lead in concentrations approaching the chronic criterion for fresh water aquatic life. One of these samples was collected from a reach of Farmers Branch upstream of any of the Flightline Area sites, so it appears that either natural background concentrations of lead in surface water are relatively high and/or Farmers Branch is receiving lead from an upstream source.

TABLE 6-4. COMPARISON OF MAXIMUM DETECTED SURFACE WATER INDICATOR CHEMICAL CONCENTRATIONS WITH EPA WATER QUALITY CRITERIA

Indicator Chemical	Maximum Detected Concentration (µg/L)	Fresh Acute (µg/L)	Fresh Chronic (µg/L)
TCE	1,400.0	46,000*	21,000*
Vinyl chloride	3.7		
Arsenic (metal)	4.8		
- Pentavalent		850*	48*
- Trivalent		360	190
Barium	210.0		
Lead	29.0	330**	12.9**
Silver	23.0	26.9**	0.12

^{*}Insufficient data to develop criteria. Value presented is the LOEL - Lowest Observed Effect Level.

Source: U.S. EPA, Quality Criteria for Water 1986b. EPA 440/5-86-001. May 1, 1986.

^{**}Hardness Dependent Criteria (300 mg/L used).

⁻⁻ No criteria or LOEL available.

6.9 <u>Defense Priority Model Evaluation</u>

Radian used the Defense Priority Model (DPM) (Oak Ridge National Laboratory, 1987) to evaluate the Flightline Area (Sites LF04, LF05, WP07, and FT09) and four East Area IRP sites at Carswell AFB. DPM uses site-specific data to prioritize sites according to the severity of contamination. For the DPM, geologic and hydrologic data are used to indicate ground-water travel times and chemical analyses are analyzed using toxicological benchmarks to indicate risk to the local human population and natural environment.

Using information obtained during Stage Two of the Installation Restoration Program (IRP) at Carswell AFB, the DPM indicated the following ranking for the sites investigated (numbers in parentheses are the results of the DPM scoring and indicate relative rankings):

- 1. Unnamed Stream (20,760);
- Flightline Area (19,381);
- 3. Landfill 1 (7,036);
- 4. Base Service Station (5,929); and
- 5. POL Tank Farm (4,584).

Radian has conducted extensive, detailed investigations of these sites and has produced a ranking of these sites which differs somewhat from the DPM ranking. The alternate ranking, which is based on the results of the Radian investigations is as follows:

- 1. Flightline Area;
- Unnamed Stream;
- 3. POL Tank Farm;
- 4. Base Service Station; and
- Landfill 1.

This discrepancy is probably because the DPM is designed as an unbiased tool for comparison and, therefore, has a simple, rigid format that does not take into account all factors which might be relevant to the ranking

of a particular site. Indeed, the Introduction to the User's Manual for the DPM indicates the possibility of false high scores using the DPM. Radian's justification for giving the Flightline Area higher priority for remedial action relative to the Unnamed Stream is explained below. The DPM evaluation worksheets for the Flightline Area are provided as Appendix G.

Flightline Area Versus Unnamed Stream

Two factors strongly influenced the DPM ranking of the Flightline Area below that of the Unnamed Stream. The more important of these is the relatively low levels of metals (especially lead) detected in the Flightline Area, compared to the Unnamed Stream site. Also important was the difference in contaminant transport times because of the proximity of the Unnamed Stream to the plant boundary and the Trinity River.

Radian assigns a higher ranking to the Flightline Area for several reasons, the most important of these being the relative concentrations of contaminants detected at these two sites. At the Unnamed Stream, no contaminants were detected at levels in excess of Maximum Contaminant Levels (MCLs). At the Flightline Area, however, TCE, vinyl chloride, tetrachloroethane and cis-1,2-dichloroethane were detected above current (or proposed) MCLs. Metals were detected in higher concentrations in the surface water samples from the Unnamed Stream, but none exceeded any regulatory concentration limit.

Another reason for assigning the Flightline Area a higher ranking is its size relative to the Unnamed Stream. The Flightline Area is much larger and contains a larger volume of contaminants than the Unnamed Stream site. It therefore presents a more complicated problem for remediation and a greater potential for future environment degradation.

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7.0 SUMMARY AND CONCLUSIONS

This section summarizes the environmental contaminants detected in the Flightline Area, with special emphasis on the extent of contaminant migration, the mechanisms/pathways by which the contaminants are transported, and the level of risk the contaminants pose to the human health and environment. Also identified are existing data gaps, possible ways to address additional data requirements, and the objectives of any remedial actions conducted in the Flightline Area.

7.1 Summary of Contamination and Associated Risks

The following subsections present an overview of the main contaminants in the Flightline Area and the quantified risks associated with exposure to those contaminants.

7.1.1 Nature and Extent of Contamination

Ground Water

Environmental sampling conducted in the Flightline Area thus far has shown ground-water contamination by volatile organic compounds, particularly trichloroethene and vinyl chloride, to be the most widespread and significant problem. During the most recent ground-water investigation (April/May,1990), TCE was detected in concentrations exceeding the federal MCL in 27 of the 35 monitor wells sampled. Vinyl chloride exceeded its MCL in seven wells. Figures 5-2 and 5-4 show isoconcentration contour maps of TCE and vinyl chloride in the Upper Zone Aquifer at the Flightline Area.

As seen in Figure 5-2, ground-water sampling of the existing monitor well network has adequately defined of the northern and southern limits of the TCE plume; however, the extent of the plume to the east and west is currently unknown. The evidence generated to date suggests the TCE contamination is preferentially migrating along paleochannels that were identified during drilling and were mapped in the Flightline Area (Figure 5-7).

The maximum vertical extent of the TCE contamination, as well as all other contamination detected in the area, apparently corresponds to the upper surface of the Goodland/Walnut Formation, which underlies the Upper Zone sediments. The limestone and shale of the Goodland/Walnut Formations appear to be an effective barrier to downward migration of ground-water contaminants to deeper aquifers, because no contaminants were detected in the two Paluxy Aquifers (the sand aquifer directly under the Goodland/Walnut aquitard) monitor wells, one of which (P-2) is located near the center of the plume during the sampling performed in 1988.

Figure 5-4 shows the lateral extent of vinyl chloride detected in the Flightline Area Upper Zone ground water. The vinyl chloride contamination is less areally extensive and better defined than the TCE plume. Isoconcentration contour mapping of vinyl chloride detected in the Upper Zone ground water suggests Landfill 5 (LF05) is the principal source of the contamination.

Several other organic compounds were detected in the ground water from the Flightline Area monitor wells, most notably tetrachloroethene and cis-1,2-dichloroethene, but the concentrations of the compounds detected were either below MCLs or they have no established MCLs.

Multiple sources are apparently contributing the organic contaminants detected in the shallow ground water of the Flightline Area. Landfills 4 and 5, the Waste Burial Area, and to a lesser extent, Fire Training Area 2 appear to be contributing to the contamination, based on the concentration distribution of the volatile organic contaminants and the consistent nature of the detected contaminants and disposed wastes. However, repeated evidence of organic contamination in monitor wells located hydraulically upgradient of these sites suggests one or more additional off-base sources. Based on similar concentrations of TCE and related transformation products detected in upgradient wells on adjoining AF Plant 4 property, AF Plant 4 is considered the principal upgradient candidate source of the balance of the Flightline Area contamination.

Although several metals species were detected in concentrations greater than respective MCLs in unfiltered ground-water samples, it is probable that no metals contamination exists in the Upper Zone Aquifer at the site as no concentrations exceeding MCLs were reported in the dissolved metals analyses which most directly reflect ground-water chemistry.

Surface Water

Trichloroethene is the principal contaminant in the surface water of the Flightline Area. It was detected in all seven of the water samples taken in 1990, and exceeded the MCL in five of the samples. The highest detected concentration was in a sample from a small tributary to Farmers Branch (sample location LF05-S7 on Figure 5-9). There is strong evidence that the shallow ground water is providing the base-flow and the resulting contamination in this small stream. As with ground water, contamination observed in a reach of Farmers Branch upstream of the Flightline Area sites suggests an additional upstream contaminant source. The farthest downstream sample from Farmers Branch contained TCE in excess of the MCL. At this location, it appears that Farmers Branch is receiving a significant contaminant contribution from the previously mentioned tributary.

Vinyl chloride was the only other volatile organic compound detected in the surface water samples in excess of any MCLs and it was detected above the MCL in only one sample collected from the golf course ponds located adjacent to the golf course maintenance facilities.

The remaining volatile organic compounds detected in the surface water samples were the cis- and trans-isomers of 1,2-DCE. These compounds were commonly detected in the Flightline Area Upper Zone ground water.

No metals were detected above MCLs in any of the surface water samples collected in 1990. Water quality indicator results from the surface water samples were compared to the ground-water results. The strong similarity in the concentrations of cations and anions suggests that discharge of Upper Zone ground water is supplying a large portion of the surface water flow.

7.1.2 <u>Fate and Transport</u>

Fate of Contaminants

No dissolved metals concentrations in Upper Zone ground-water samples exceeded MCLs. Therefore only the persistence and transformation of organic contaminants were addressed. The ground-water contamination in the Flightline Area consists mainly of volatile chlorinated organic solvents, principally TCE with lesser amounts of chemically-related transformation compounds (Figure 5-1). The fate and persistence of these volatile organic compounds is controlled largely by the processes of diffusion and dispersion, adsorption and desorption, volatilization and subsequent resorption, and chemical and biological degradation.

Diffusion and dispersion are chemical and mechanical processes which contribute to dilution of specific contaminants within the body of the plume, but also result in enlargement of the plume. Because TCE and its related daughter products are generally classified as mobile solutes in water and therefore have a higher activity in the aqueous phase, their capacity for transport is only slightly retarded with respect to that due to the flow of ground water.

The organic compounds observed in the Upper Zone Aquifer in the Flightline Area are volatile by nature, and any volatilization of these compounds from the ground-water system could result in their permanent removal. Although some of the compounds might be adsorbed onto overlying sediments, historically the Upper Zone Aquifer water table has not changed significantly, and therefore there is little chance of the compounds being resorbed back into the ground-water system.

Tetrachloroethene, trichloroethene, cis- and trans-1,2-dichloroethene and vinyl chloride are all chlorinated solvents and related by the chemical process of hydrogenolysis (Figure 5-1). This process is very common in nature and may be biologically driven, as a form of biodegradation. Based on available records and water sampling results, it appears TCE was the principal solvent disposed of in the Flightline Area, and the cis- and trans-1,2-DCE and vinyl chloride detected in lesser quantities are mainly daughter products of the TCE (and possibly the PCE).

Transport in Ground Water

Using data obtained from the June 1990 Upper Zone Aquifer pumping test and the potentiometric surface map of the aquifer, the average groundwater flow rate in the Upper Zone is calculated to be approximately 9 feet per day. By comparing the TCE contaminant plume position as determined in both 1988 and 1990, it appears the plume is migrating approximately an order of magnitude slower than the ground water. The contaminant plume migration does not conform wholly to the ground-water flow direction, which is generally toward Farmers Branch. A portion of the plume appears to be preferentially moving through the thickest accumulations of sand and gravel in the Upper Zone, in a more easterly direction than the shallow ground-water flow. While Farmers Branch and one of its tributaries are capturing a portion of the contaminant plume, there is continued plume migration in a generally east-south-easterly direction from the Flightline Area.

Transport in Surface Water

The two main surface water bodies in the study area, Farmers Branch and the small tributary to Farmers Branch, were found to contain varying concentrations of volatile organic compounds. The small tributary exhibited the greatest degree of contamination, the indirect source of which is believed to be discharge of Upper Zone ground water. A portion of Farmers Branch that is upstream of, and therefore unaffected by the Flightline Area sites, contained volatile organic compounds from an upstream source. Currently, the estimated concentration of TCE migrating off-site in Farmers Branch is 45 μ g/L, and 1,2-DCE is estimated at 8 μ g/L. Volatilization will reduce the volatile organic contaminant content of Farmers Branch before its ultimate discharge into the Trinity River.

7.1.3 Risk Assessment

Using both the 1988 and 1990 analytical results from soil, ground water, and surface water samples collected in the Flightline Area, 19 indicator chemicals were selected from the approximately 80 chemicals known to be present at the site. The indicator chemicals consisted of 10 metals, eight volatile organic compounds and one semivolatile organic compound. These chemicals were selected according to the methods in the U.S. EPA Health Evaluation Manual (1986a). Although several of the indicator chemicals selected, particularly the metals and the semivolatile compound, are not believed to represent an actual contaminant problem at the site, they were included in the risk assessment process to ensure a conservative evaluation of possible health risks.

Possible mechanisms of contaminant release from the Flightline Area sites include: 1) volatilization to the air, 2) fugitive dust generation, 3) leachate to ground water, 4) surface runoff, 5) direct release to surface water, and 6) contaminated ground-water discharge to surface water. Of these six possible mechanisms, volatilization to the air, leachate to ground water, and contaminated ground water discharging to surface water appear to be the most important release mechanisms in the Flightline Area.

Potentially significant contaminant transport and fate mechanisms were identified and include: 1) air dispersion, 2) ground-water migration, 3) discharge to the surface, 4) transport in surface water, and 5) subsequent uptake by plants and animals.

Results of an evaluation to determine possible human exposure routes from the six previously mentioned waste release mechanisms (Figure 6-1) show six potential pathways exist. All six of the pathways initially involve contaminants volatilizing to the air or leaching to the ground water. Based on the potential pathways identified, potential human and wildlife receptors for exposure to contaminants migrating from the Flightline Area were identified.

Three types of exposures - inhalation, ingestion, and dermal contact were quantified in the risk assessment. The maximum predicted annual average concentrations resulting from estimated Flightline Area VOC indicator chemical emissions are lower than the conservative TACB Effects Screening Levels by orders of magnitude ranging from 4 to 8. Potential ingestion exposures included consuming meat and dairy products or fish exposed to contaminants, however, neither of these potential pathways were found to represent a significant threat of human exposure. Dermal exposure to contaminants in Lake Worth and the Trinity River was found to be insignificant, at most. Skin contact with water in Farmers Branch, which is not amenable to swimming or contact activities other than wading, could result in dermal exposure, but the insignificance of such potential exposure did not merit quantification.

The threat to human health posed by the site was evaluated in terms of noncarcinogenic and carcinogenic risks. The noncarcinogenic evaluation involved comparing maximum predicted annual average volatile organic contaminant concentrations at various locations, both on-site and off-site, with inhalation Reference Doses (RFDs) for chronic (long-term) exposure. The results of this comparison indicate the threat of noncarcinogenic health effects of inhalation exposure to contaminants released from the Flightline Area is not significant. Concerning carcinogenic risks, seven of the eight VOC indicator chemicals are potential carcinogens. Incremental individual cancer risks were estimated for maximum exposed individuals at locations both on- and off-site. The highest risk of one in 10 million was dismissed as inconsequential. Ingestion and dermal risks were considered minimal and were not quantified.

When considering the threat to wildlife and aquatic organisms from the contaminants migrating from the Flightline Area, the level of contaminants found in the site surface water bodies were compared to the EPA Quality Criteria for Water (1986b). Some risk exists for terrestrial wildlife that use Farmers Branch, the small tributary, or the golf course ponds as a source of drinking water, as well as for aquatic organisms in these surface water bodies. Lead was detected in a concentration exceeding the chronic criterion

for fresh water aquatic life in the westernmost golf course pond (Figure 5-9), however the reported result is questionable because it was from the dissolved lead analysis, and the total lead concentration in the unfiltered sample was less than the chronic criterion. Silver was detected at three locations in concentrations above the chronic criterion, but all three results were for total silver. Silver was not detected in the dissolved phase, however, the detection limit for the analytical method (10 μ g/L) was greater than the chronic criterion. Therefore it is not possible to determine whether any dissolved silver concentrations exceeded the criterion.

7.2 <u>Conclusions</u>

The following subsections focus on additional data requirements, recommended ways to obtain the additional data, and the remedial action objectives for the Flightline Area.

7.2.1 <u>Data Limitations and Recommendations for Future Work</u>

The remaining information needed from the Flightline Area is primarily for more complete definition of the extent of the volatile organic contaminant plume, and better understanding of the mechanics of ground-water flow in the Upper Zone. Specifically:

- The lateral and downgradient limits of the VOC plume in the Upper Zone Aquifer;
- Identification and characterization of the upgradient, offbase source(s) of Upper Zone contamination in the Flightline Area;
- The VOC content of the water in Farmers Branch at a location immediately upstream of its discharge point to the Trinity River;

- Computer modelling of ground-water flow and contaminant transport;
- Upper Zone Aquifer properties, such as transmissivity and storage coefficient, near Farmers Branch and the small tributary.

Although estimates of aquifer properties were obtained as a result of the June 1990 pumping test, this test was conducted in an area where the thickest sequence of sands and gravels observed in the Flightline Area occurs. If, as anticipated, the selected remedial alternative involves the use of ground-water extraction wells in areas with thinner, less permeable Upper Zone sediments, the aquifer properties in these areas will require re-evaluation. Also, various scenarios of the aquifer response to pumping can be generated with computer programs.

Specific recommendations for additional work in the Flightline Area follow. All of these activities could be incorporated into the detailed design phase for the selected remedial alternative.

- Installing up to five additional Upper Zone monitor wells to determine the lateral and downgradient extent of the VOC contaminant plume. The location of the wells will be selected to determine the downgradient (easternmost) extent of the plume, and to determine whether the contaminant plume extends beneath Farmers Branch to the north. These wells could also be included in any long-term monitoring scheme to evaluate the effectiveness of the selected remedial alternative in preventing further plume migration.
- Performing one round of ground-water sampling and analyses for volatile halocarbon compounds that includes all Carswell AFB Flightline monitor wells, and monitor wells previously installed by Hargis and Associates for AF Plant 4 in the Carswell Flightline Area and on adjoining AF Plant 4 property.

Analytical results from this effort would help to determine the location, nature, and magnitude of upgradient contaminant sources; define the upgradient limits of Upper Zone groundwater contamination; and evaluate the degree of continuity of ground-water contamination beneath AF Plant 4 and the Carswell AFB Flightline Area.

- 3) Surface water sampling of Farmers Branch at a point just above its confluence with the Trinity River. Information gained through this activity will help in determining the extent of surface water contamination, will provide information regarding contaminant fate and transport, and will validate assumptions made in the risk assessment.
- 4) One to two aquifer tests along Farmers Branch and the small tributary are recommended to provide additional information to support remedial actions.
- 5) Computer modelling to obtain a better understanding of groundwater flow and contaminant migration patterns.

7.2.2 <u>Recommended Remedial Action Objectives</u>

The Flightline Area Upper Zone ground water, surface water, and soils are contaminated with volatile organic compounds. Based on the existing environmental conditions, the recommended objectives of any remedial actions are to:

- 1) Reduce or eliminate potential impacts to human health and the environment;
- 2) Reduce or eliminate the potential for future contaminant migration in the ground water or surface water; and

3) Reduce, eliminate, or immobilize contaminants in near-surface soil (Upper Zone deposits).

To identify and evaluate remedial alternatives, potentially contaminated environmental media were identified based on previous Flightline Area investigative results. These media include waste material and contaminated soil, Upper Zone ground water, and surface water. Specific remedial action objectives identified for each of the media are presented in Table 7-1. Remedial action objectives were developed for each media based upon the following standards or criteria:

- 70-year cancer risk potential;
- National interim primary drinking water standards maximum contaminant levels (MCLs) for organics (40 CFR 141.12 and 141.61) and inorganics (40 CFR 141.11 and 141.62); and
- · Proposed MCLs for organics and inorganics.

Table 7-1 does not list all contaminants that have regulatory criteria or standards. Instead the table lists those contaminants that were identified as indicator chemicals in the baseline risk assessment for the Flightline Area. As previously explained, metals are included as indicator chemicals on the basis of total concentrations detected. However, the dissolved metals concentrations detected in the 1990 sampling event do not suggest a metals contamination problem.

Remedial Action Objectives	FOR HUMAN HEALTH: Prevent ingestion or direct contact with soil or waste at sites which contributes to greater than or equal to 10 ⁻⁸ excess cancer risk (or a potential risk characterized as greater than negligible) from the following carcinogens: TCE, benzene, bis(2-ethylhexyl)phthalate, arsenic, cadmium, and methylene chloride.	Reduce inhalation of potential carcinogens (TCE, 1,2-DCE, tetrachloroethylene, vinyl chloride, methylene chloride, benzene, chloroform, and bis(2-ethylhexyl)phthalate] at locations which contribute to excess inhalation cancer risk levels of greater than or equal to 10.8 so that risk levels are lower than 10.8.	FOR ENVIRONMENTAL PROTECTION: Prevent migration of contaminants from soil that would result in ground-water contamination in excess of the following concentrations for each specific contaminant:	<u>Inorganics</u>	Arsenic 0.05 mg/L TCE TCE 5 Mg/L Barium 1.0 mg/L Vinyl Chloride 2 Mg/L Cadmium 0.01 mg/L Benzene 5 Mg/L Chromium 0.05 mg/L 1,2-DCE 70 Mg/L Lead 0.05 mg/L Tetrachloroethene 8 Mg/L Selenium 0.01 mg/L Toluene 2,000 Mg/L Silver 0.05 mg/L Toluene 2,000 Mg/L
Environmental Media	WASTE AND CONTAMINATĘD SOIL				

la Remedial Action Objectives	FOR HUMAN HEALTH: Prevent ingestion of ground water that contributes to an excess cancer risk of greater than or equal to 10 ⁻⁸ . FOR ENVIRONMENTAL PROTECTION: Remove contaminants from the ground water to levels below the following concentrations:	<u>Inorganics</u> <u>Organics</u>	Arsenic 0.05 mg/L Vinyl Chloride 2 Mg/L Barium 1.0 mg/L Benzene 5 Mg/L Cadmium 0.01 mg/L 1,2-DCE 70 Mg/L Chromium 0.05 mg/L TCE 5 Mg/L Lead 0.05 mg/L Tetrachloroethene 8 Mg/L Selenium 0.01 mg/L Toluene 2,000 Mg/L Silver 0.05 mg/L 10.05 mg/L 10.00 mg/L	FOR HUMAN HEALTH: Prevent ingestion of or skin contact with surface water that contributes to an excess cancer risk of greater than or equal to 10°8. Prevent ingestion of fish from surface water that contributes to an excess cancer risk of greater than or equal to 10°8.	FOR ENVIRONMENTAL PROTECTION: Prevent future discharge of contaminated ground water to surface water. If treated ground-water effluent is discharged to Farmers Branch, it must meet the environmental protection criteria for ground water (above).
Environmental Media	GROUND WATER			SURFACE WATER	

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GLOSSARY OF DEFINITIONS, NOMENCLATURE, AND UNITS

AA atomic absorption

AFB Air Force Base

Alluvium stream-deposited sediment; predominantly clay,

silt, sand, and gravel

Aquifer geologic unit capable of storing and

transmitting significant quantities of ground

water

Aquitard geologic unit impervious to ground water which

acts to contain ground water within an adjacent

unit

ARAR Applicable or Relevant and Appropriate

Requirement

Artesian term applied to ground ater confined under

hydrostatic pressure

BLS below land surface

DOD U.S. Department of Defense

ECD electron capture detector

EICP Extracted Ion Current Profile

EPA U.S. Environmental Protection Agency

Evapotranspiration loss of water from the soil both by evaporation

and by transpiration to growing plants

Extraction method for mobilizing contaminant species from a

solid matrix prior to analysis

FDTA Fire Department Training Area

FS feasibility study

GC gas chromatography

GC/HSD gas chromatography/halide specific detector

GC/MS gas chromatography/mass spectroscopy

GFAA graphite furnace atomic absorption spectroscopy

GLOSSARY OF DEFINITIONS, NOMENCLATURE, AND UNITS (Cont.)

gpd gallons per day

gpm gallons per minute

Hydraulic Conductivity a coefficient of proportionality describing the

rate at which water can move through a permeable

medium

IRP Installation Restoration Program

MCL Maximum Contaminant Level

MS mass spectroscopy

MSL mean sea level

MS/MSD Matrix Spike/Matrix Spike Duplicate

NCP National Contingency Plan

OEHL Occupational and Environmental Health Laboratory

OVA organic vapor analyzer

0&G oil and grease

PCB polychlorinated biphenyl

PID photoionization detector

piezometric/potentio-

metric surface

an imaginary surface representing the static head of ground water defined by the level to

which water will rise in a well

PMCL proposed maximum contaminant level

ppb parts per billion

ppm parts per million

QAPP Quality Assurance Program Plan

QA/QC Quality Assurance/Quality Control

RI/FS Remedial Investigation/Feasibility Study

SOW State of Work

GLOSSARY OF DEFINITIONS, NOMENCLATURE, AND UNITS (Cont.)

spike a known amount of a compound added to a sample

and analyzed to determine the accuracy of

analysis

SW-846 EPA test methods for evaluating solid wastes,

physical and chemical methods

TCE trichloroethene

TDS Total Dissolved Solids

TOC Total organic carbon

TOX Total organic halides

TPM Technical Program Manager

Transmissivity the rate at which water is transmitted through a

unit width of an aquifer or confining bed under

a unit hydraulic gradient.

USAF United States Air Force

USAFOEHL United States Air Force Occupational and

Environmental Health Laboratory

USDA United States Department of Agriculture

USGS United States Geological Survey

VOC volatile organic compound

water table the elevation of the ground water surface in an

unconfined aquifer

GLOSSARY OF DEFINITIONS, NOMENCLATURE, AND UNITS (Cont.)

Multiplication Factor	<u>Prefix</u>	<u>Symbol</u>
1,000,000,000,000,000,000-1018	exa-	E
1,000,000,000,000,000-1015	peta-	P
1,000,000,000,000-10012	tera-	T
1,000,000,000-10	giga-	G
1,000,000-10	mega-	M
1,000-103	kilo-	k
100-10,	hecto-	h
10-101,	deka-	da
0.1-10-1	deci-	d
0.01-10-2	centi-	c
0.001-10-3	milli-	a
$0.000\ 001-10^{-6}$	micro-	u
0.000 000 001-10	nano-	n
0.000 000 000 001-10 15	pico-	p f
0.000 000 000 000 001=10-13	fento-	f
0.000 000 000 000 000 001=10	atto-	a

```
ppm(parts per million) - mg/kg, ug/g, ng/mg, pg/ug, mg/L, ug/mL, ng/uL
ppb (parts per billion) - ug/kg, ng/g, pg/mg, ug/L, ng/mL, pg/uL
ppt (parts per trillion) - ng/kg, pg/g, fg/mg, ng/L, pg/mL, fg/uL
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APPENDIX A

Lithologic Logs

(Previous Lithologic Logs may be found in CH2M Hill (1984), Radian (1986), and Radian (1989))

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DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
1. PI	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 40.1 ft BGL	
Ĺ_	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
] 2. L	OCATION: F	l <u>ig</u> htline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DI	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 17	
	OLE NO.: L				11. ELEVATION GROUND WATER: 600.26 ft MS	L (6/18/90)
	AME OF GEOL		E. Fain	-	12. DATE HOLE ESTABLISHED: 3/23/90	
	OORDINATES				13. SURFACE ELEVATION: 626.50 ft MSL	
•			397653.57		14. BACKGROUND:	
1					15. MEASURING POINT ELEVATION: 629.24 ft	MSL
Depth	Graphic	Blow	Soil	1		1
	Log		Class/Code	Visual Descr	iption	Remarks
10	7/7/		U/CLLR		rown, slightly silty, very stiff, damp	Full recoveries
i	$V//\lambda$		1	minor small		unless noted.
i	$V//\lambda$		<u> </u>	1	•	1
1	V//X		i	ì		i I
2			I II/CLLB	ICLOVE As abo	ve, 5 - 10% calcareous material (nodules,	
4			U/CLLR	•	ve, 5 - 10x catcaleous material (hoostes,	
1			1	mottling).		1
!	<i>\///</i>		I .	1		1
1	Y///		<u> </u>			
1 4	Y///) U/CLLR	•	/Brown, silty, minor fine sand, calcareous	:
1	V///		ነ	material ~ 1	0 - 20% of sample, very stiff.	knife.
1	V///			1		1
1			1	1		1
6			U/CLLR	Clay: As abo	eve, mottling of various colors is disturbed	1
i			i	llooking.		į
i	Y///		ì	i		i
i	Y///		1	i		
8	Y///		U/CLLR	IClav. As abo	ve, - 20% green silty clay.	Boring does not
0	Y///) O/CEER	i	ve, Low green sitty etay.	appear to encounter
ļ	V///		1	I I		fill material (Like
I .	V///		!			
1 40	V///	i	1	151 0	the state of the smaller of the	LF05-02).
10			U/CLLR		/brown with greenish mottling, silty,	
1			1	sandy, - 1%	calcareous material, firm.	
1	Y///		Ì	1		
ļ	Y///		1	1		
1	\mathbb{Z}/\mathbb{Z}		1	1		
12.3	1		U/SDSH	Sand: Orange	e/brown, very clayey and silty; very fine to	
1	1		1	fine grained	, bedding (horizontal) evident, damp: Clays	1
i			İ	occur mainly	/ in 2 - 4 in. seams - every foot.	İ
14	· · · · ·		U/SDSM	Sand: As abo	•	İ
i			i	i		İ
i			i	i		i
ì			i	i		
l l 16		}	I I U/SDSM		orange, fine grained, slightly clayey,	 1.2 ft. Recovery
1 10		!	U/SUSFI	•		It were
}	1	}	1	juanp, quartz	tose, Clay occurs as thin seams.	1
!	\	}	1	Į.		1
ļ.]	!	Į,	!		1
	1	[1	Ţ		Į.
1	1		1	1		1
19		1	U/SDFN	•	fine grained, loose, >95% quartz, damp;	4.2 ft Recovery.
i	1		1	oxidation st	tained laminae 21.5 - 22 ft.; 0.4 ft. clay	1
1	1		}	seam 21.1 -	21.5 ft.	1
i	1		i	i		İ
i	1	1	İ	i		i
	1	Ī				:
i	1	}		ł		i

1. PR		RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS
	OJECT: CAR	-			7. TOTAL DEPTH OF HOLE: 40.1 ft BGL	
		PHASE II			8. DATUM FOR ELEVATION SHOWN: see level	
2. LO	CATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mohile Deill D-61
`			ronmental Dri	illere inc	10. NO. OF SAMPLES TAKEN: 17	NODITE DITTE 5-01
			TOTAL DI	itters, file.		
	LE NO.: LI		r raim		11. ELEVATION GROUND WATER: 600.26 ft MS	E (6/18/90)
	ME OF GEOL	-	E. Fain		12. DATE HOLE ESTABLISHED: 3/23/90	
	ORDINATES (13. SURFACE ELEVATION: 626.50 ft MSL	
<u> </u>	2019579.	19 Y:	<u>397653.57</u>		14. BACKGROUND:	
					15. MEASURING POINT ELEVATION: 629.24 ft	: MSL
	Graphic	Blow	Soil	1		
<u> Ft.) </u>	Log	Count	Class/Code	Visual Descr	iption	Remarks
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j.			1	1		İ
1			i	1		i
ĺ			j	i		1
- 1	• • • • •		i	i		1
1	• • • •		;	i		1
24	`.'.'		U/SDFN		ve heavily avidical 2/ - 25 fe	1
			i O/SOFM	Janus va apo	ve, heavily oxidized 24 - 25 ft.	1
as I			1	1		!
25	////		U/CLLR	•	gray in 1 - 2 in. seams, oxidation	İ
1	///\		ļ.		ndy (fine grained), cohesive, moist;	1
ľ	///		1	getting sand	ier past 28 ft., wet at 28.5 ft.	1
r	///		1	1		1
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į	////		i	i		1
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29	///		ן ווערוים	Charter Bases	Name and Control of School of School	1
-			U/CLLR		· · · · · · · · · · · · · · · · · · ·	W. L. Measured
r			1		fine to fine grained, - 30 - 40%; 31 - 32	•
ľ			!	1	ttle sand; 32 - 34 ft. sand with minor	ft. BLS, W. L.
Y	////		l	ctay.		after completion =
ŀ	////		1	1	•	27.5 BLS, 3.6 ft.
Ļ			1	1		Recovery.
32			U/SDSM	Sand: Burnt	orange (heavily oxidized), fine to medium	İ
j.			ĺ		ghtly clayey, slightly cohesive. Increasing	ì
i i			i	•	nd 10 - 20% gravels (small) 33 - 34 ft.	i i
- 1	• • • • •		i		······································	1
34 F			1 11/5000	I cond and one	Mala Canada EO/EO	17.0
~ }	10.00		U/SDGR		vel: Orange, 50/50, wet; sands very fine to	:
	$\gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot \gamma \cdot$		Į.		grained, poorly sorted; gravels bimodal:	ft.
F	~~~\\		1	chert and qu	artz gravels, mostly granule and small	
l	.O.O.A			pebble size;	large gravel (20 - 50 mm) is very	†
F	0.0.01		1	fossiliferou	s limestone clasts.	1
•	.0.0.4		1	1		İ
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39	· · · · · · · · · · · ·	- ^		1		40.0 ft.
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39 40				1		5.5 ft. sampler; 50
(1		[•		
(<u> </u>	j		blows = 1 in.; T.D.
([1		blows = 1 in.; T.D. = 40.1.
([; 		•
([; 		•

DPTII	THE LOC	DANTAS			I INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SUFETS
			CORPORATION			OF & SHEETS
IRP PHASE II STAGE 2					7. TOTAL DEPTH OF HOLE: 37.7 ft BGL	
					8. DATUM FOR ELEVATION SHOWN: sea level	
		<u>lightline</u>			9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill 8-61
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
	LE NO .: L	_			11. ELEVATION GROUND WATER: 597.45 ft MS	L (6/18/90)
		OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/28/90	
	ORDINATES			,	13. SURFACE ELEVATION: 621.00 ft MSL	
<u> </u>	2020510.	50 Y:	397732.54	<u> </u>	14. BACKGROUND:	
					15. MEASURING POINT ELEVATION: 623.68 ft	MSL
epth	Graphic		Soil			(
(Ft.)	Log	Count	Class/Code	Visual Descr		Remarks
0			U/CLLR	Clay: Dark b	rown, silty, firm, roots, damp,	Full samplers
ľ			}	carbonaceous	staining.	unles noted.
ľ]		1
ł	////		1	Į.		Į.
2			U/CLLR	Clay: As abo	ve; at 3.0 ft. going to orange/brown, silty	ľ
ŀ			İ	clay with 5	- 10% calcareous material.	Ì
ĺ	///		į	İ		İ
l	///		í	i		i
4	///		U/CLLR	Clay: As abo	ve.	1 1.5 ft. Recovery
			1	1		1
ľ			1	1		1
ľ] 	1		<u> </u>
,			1 446415		there can although a same fine and	Ĭ,
6	////		U/CLLR	•	/brown, very silty, minor very fine grained	!
ŀ	///		ļ	sand, stiff,	calcareous nodules, carboaceous streaking.	1
l	////		ļ	ļ		
l	///		l	}		ļ
8	///		U/CLLR	Clay: As abo	ve, increasing calcareous material to 30%.	1
ſ			1			1
ľ			1			1
ľ						!
ł	////		1			1
Ì			Ì	1		İ
11		!	U/SDGR	Sand and Gra	vel: Orange, very poorly sorted, cohesive,	į
}	$ \cdot \circ \cdot \circ \cdot $		i	7	y, damp, abundant calcareous material.	i
)	0.0.0		i	1	,, ,, ,	i
	.0.0.4	· 	i	ί		1
13			U/SDLR		fine grained, minor larger sizes to	1
'			i O/SOCK		htly clayey and silty, damp.	1
12 2			1 11/00/2			1
13.5	0.0.0		U/SDLR	•	ve, increasing coarseness with depth, 5 -	
	0.000		}	10% small gr	avels.	
ļ	0.0.0		1	!		1
	0.0.0		I			<u>!</u>
1			}	1		1
16.5	0.0.0		U/SDLR	Sand: As abo	ve, gravelly; changing to tan, fine to	
- 1	0.0.9		1	medium grain	ed, loose, quartzose at 18.0 ft., damp.	!
	0.0.0		1	1		
	.0.0.0		i	Ì		İ
18.5	0.0.0		U/SDLR	Sand: As abo	eve, well sorted, medium grained, damp; 0.4	3.5 ft. Recovery
				•	zone at 21.5 - 21.9 ft.	1
			1	1 2.0,000	more we write will be	1
	h.o.o		1	1		I
ļ	0.0.0		1	I		1
	ام اما اما	1	i	1		Į.
	0.0.0	Į	1	i		1
	0.0.0		Ì]

			_		
DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS
1. PROJECT: CAR	RSWELL AFB,			7. TOTAL DEPTH OF HOLE: 37.7 ft BGL	
IRF	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
2. LOCATION: 1	<u>lightline</u>	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DRILLING AGE	NCY: Envi	ronmen <u>tal Dri</u>	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14	1
1 4. HOLE NO .: L	F04-02			11. ELEVATION GROUND WATER: 597.45 ft MS	L (6/18/90)
5. NAME OF GEOL	OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/28/90	
6. COORDINATES	OF HOLE:			13. SURFACE ELEVATION: 621.00 ft MSL	
X: 2020510.	.50 Y:	397732.54		14. BACKGROUND:	
				15. MEASURING POINT ELEVATION: 623.68 ft	MSL
Depth Graphic	Blow	Soil	1		1
[(Ft.) Log	Count	Class/Code	Visual Descr	iption	Remarks
23.5 - 23.5		 U/SDLR 	•	0% quartz; 0.3 ft. gravelly zone at 27 ft.,	
28.5 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0		U/SDLR	 Sand: As abo 	ove, 1-3% granule size gravel.	W. L. measured at
33.5 0.0.0.0 0.0.0.0 0.0.0.0 0.0.0.0	1	 	 Sand: Tan, m gravels to 2 	nedium grained, quartzose, loose, wet, 5% 25 mm.	
	· · · · · · · ·	- U/MARL 	 Limestone: M fissile. 	Marly, weathered sand and gravel intermixed,	 T.D. = 37.7 ft.

			CORPORATION			OF 2 SHEETS
1. PR	OJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 37.6 ft BGL	
		PHASE II			8. DATUM FOR ELEVATION SHOWN: see level	
2. LC	CATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DF	RILLING AGE	NCY: Envi	ronmental <u>Dri</u>	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
4. HC	DLE_NO.: L	F04-03			11. ELEVATION GROUND WATER: 597.58 ft MS	L (6/18/90)
5. N/	ME OF GEOL	OGIST: S.	B. Blount, S	. E. Fain	12. DATE HOLE ESTABLISHED: 3/20/90	
6. CC	ORDINATES	OF HOLE:			13. SURFACE ELEVATION: 620.50 ft MSL	
X:	2020506.	79 Y:	397683.46	•	14. BACKGROUND:	
				-	15. MEASURING POINT ELEVATION: 623.25 ft	MSL
Depth	Graphic	Blow	l Soit	1		1
(Ft.)			•	 Visual Descr	iption	Remarks
0	7777		U/CLAY		soft to firm, semi-plastic, with fine	Full recovery
-			1	:	minor carbonaceous streaking and	unless otherwise
	///		1	•		indicated.
1			1	particles, m	Dist to wet.	i micateu.
_			1	1-1		
2			U/CLAY	: '	ve, firm to stiff (stiffens to base), minor	1 100 Stiff to cut.
	Y///		!	:	ebris, more abundant carbonaceous staining,	!
	Y///			very stiff;	3.8 - 4.0 ft.	
	Y///		ļ			ļ.
4	$Y//\lambda$		U/CLLR	Clay: Orange	/brown at 4.1 ft; brittle, damp, abundant	Hard pushing.
			İ	calcareous d	ebris, slickensided, calichified with some	1
	////		1	authigenic m	ineralization (crystals of CaCO3 in shell	1
			1	frags.); ver	y hard, silty.	1
6			U/CLLR	Clay: As abo	we, very stiff, slightly sandy and silty.	1
			i	i		i
	Y///		i	i		,
	Y///		1	i		1
8	Y///		i I U/CLLR	Irlav: As abo	ve, few large CaCO3 pebbles (25 mm),	 1 ft. recovery,
	V//A		1 0/0222		lacareous material with depth, very fine	ST. Rig broken.
			l l	grained sand	• • •	
				gratned sand	•	Continue after
40			11/01/2	101	dh	repairs.
10			U/CLLR		/brown, silty, cohesive, damp, > 30%	Caliche layer at
			!	calcareous m	waterial, stiff.	12 ft., drilling
			1	ļ		through.
	Y ///		I	I		
	<u>/ / / /</u>					1
12.1	l		U/SDFN	Sand: Orange	, fine grained, loose, damp, quartzose,	1
	1	1	1	well sorted;	at 14.3 ft. sharp change to tan, very fine	1
	1	l	1	grained sand	, heavily oxidized in laminae.	1
]		i	Ì	•	İ
14.5]. `. `. `.		U/SAND	Sand: Orange	, fine to medium grained, quartzose, damp,	3 ft. Recovery.
			1	•	elly seam 15 - 15.5 ft.	1
					regreen to topo the	
		1	1	1		#
	<i> </i>	1	1	1		
		1	1	!		1
	1	}	1	1		1
		l	Į.	!		
	[Į.	I	İ		
		Į	1	1		
	• • • •		1	1		1
19.5	0.0.0	ì	U/SDLR	Sand: Orange	tan, fine to medium grained, damp, loose,	4 ft. Recovery.
		i		subround, >	90% quartz, 1 - 3% small gravel and shells.	
	[`^`^	}	i	i		Ì
	10.0.0	t	1	•		1
	[· ` ` ` ` ` ` ` ` ` ` ` ` ` ` ` ` ` ` `	ł	1			I .
	0.0.0	<u> </u>				1

DRILLING LOG		CORPORATION_		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS	
1. PROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 37.6 ft BGL		
-	PHASE II S	_		8. DATUM FOR ELEVATION SHOWN: see level		
2. LOCATION: F		_		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DRILLING AGE		ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14		
4. HOLE NO.: L	•			11. ELEVATION GROUND WATER: 597.58 ft MS	L (6/18/90)	
5. NAME OF GEOL		B. Blount, S	. E. Fain	12. DATE HOLE ESTABLISHED: 3/20/90		
6. COORDINATES				13. SURFACE ELEVATION: 620.50 ft MSL	 	
<u> X: 2020506.</u>	<u>79 Y:</u>	397683.46	· · · · ·	14. BACKGROUND:		
<u> </u>		1		15. MEASURING POINT ELEVATION: 623.25 ft	MSL	
Depth Graphic		Soil	l			
(Ft.) Log	Count	Class/Code	Visual Descr	iption	Remarks	
24.5 24.5		 	-	e/tan, fine to medium grained, wet, loose, relly zone at 27 ft., quartzose; at 30 ft.	 	
29.5 0.0.0 0.0.0 0.0.0		 	 Sand: As abo	eve, saturated.	 - 3.2 ft. Recovery. - -	
32 000		 U/GRVL 	Gravel: Vari <10% sand, s	colored, up to pebble size (30 mm), shells, saturated.	i ! !	
34.5 000 000 000 000		 	•	above, mainly small pebble size (5 - 10 mm), angular to subrounded, large percentage of		
37.5	50	U/MARL 		gray, indurated, oxidation stained	Sampler refusal at 37.5 ft., drove 1 1/2 in. S.S. 50 blows = 1 in.; T.D. = 37.6 ft.	
		{ 	 		{ 	

		_						
DRILL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	OF 2 SHEETS		
1. PF	ROJECT: CAR	SWELL AFB,	,		7. TOTAL DEPTH OF HOLE: 25.4 ft BGL			
1	<u>IRP</u>	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level			
2. LC	CATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61		
3. DF	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 10			
1 4. HC	DLE NO.: L	F04-04			11. ELEVATION GROUND WATER: 595.32 ft MS	SL (6/18/90)		
5. NA	ME OF GEOL	OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/20/90			
6. CC	ORDINATES	OF HOLE:			13. SURFACE ELEVATION: 609.40 ft MSL			
<u> x:</u>	<u>2</u> 021365.	82 Y:	397554.53		14. BACKGROUND:			
1			·		1 15. MEASURING POINT ELEVATION: 612.07 ft	: MSL		
Depth	Graphic	Blow	Soil	1				
(Ft.)	Log	Count	[Class/Code	Visual Descr	iption	Remarks		
0			U/CLLR	Clay: Red/br	own, sandy, silty, damp, cohesive, roots;	Full sample		
1			1	increasing s	and with depth.	recoveries unless		
1			İ	1		noted.		
1.5			U/SDSM	Sand: Red/br	own, clayey, cohesive, minor small gravel,	1.6 ft. Recovery.		
	• • • • }		1	damp, decrea	sing clay content with depth.	İ		
			1	1		i		
i i			İ	İ		į i		
j	••••		İ	İ		j		
4			U/SAND	Sand: Orange	, fine to medium grained, slightly	į i		
i			i	cohesive, qu	ertzose, damp, subangular to subrounded.	i i		
i	• • • •		i	i .		i		
i			i	İ		i		
i 6			U/SAND	Sand: As abo	eve, only tan and loose.	1.7 ft. Recovery.		
_i'	[1	1				
i			i	İ				
i		1	i	i I				
18			U/SAND	Sand: As abo	ive. damo.	1.5 ft. Recovery.		
i			1	1	,			
i .		1	i	! 				
i	(1	! !				
10	$rac{1}{2}$		U/SDLR	 Sand: Tan wi	th occassional iron stained thin beds,			
1 ,0	1.0.0.4		0,00 2K	•	fine to medium grained; 1 - 3% gravels			
<u> </u>	0.0.0			starting at				
1	6.0.0	<u>.</u>	1	Starting at	12.5 11.			
i			1	 				
-	0.001	i 		1] 		
-		 		1]]		
	Y,Y,Y]		1	1				
17 7	1.0.0.d		 II/ence	 Cand and Con	wal. Fine and so makhle airs			
13.7	0.0.0		U/SDGR	•	ivel: Fine sand to pebble size gravel,	3.5 ft. Recovery.		
ļ.	1.0.0.4		1	•	yey, shells, 50/50 sand to gravel, mainly			
I	b.o.ol			quartz/chert	, wet.			
I	1.0.0.1		1	1	•	!		
!			1	ļ		1		
- !	M_{M}			!		!		
!	[``A`A`}		ļ	!		<u> </u>		
ļ	h.a.al		!	ļ.		ļ		
ļ	·⊙· <u></u> ⊙∙∮		!	ļ.		!		
1	p.o.ol		ļ.	ļ.		1		
19	1.0.0.0		U/GRSM	•	Sand: As above, but gravel content	4.0 ft. Recovery.		
Į.	b.n.nl		I	•	to 70%, gravels mostly 5 - 10 mm; but some			
ļ	~ 0.00		ļ	•	and mainly coarse grained, limestone clasts;			
!			1	23 - 24 ft.	slightly indurated - increased limestone			
ļ	$\mathbb{M}^{\mathcal{M}}$		ļ	content.				
	1.0.0.		1	1				
	$\mathcal{O}(0)$							

DRILLING LOG	<u> </u>
1. PROJECT: CARSWELL AFB, 7. TOTAL DEPTH OF HOLE: 25.4 ft BGL IRP PHASE II STAGE 2 8. DATUM FOR ELEVATION SHOWN: see level	3
IRP PHASE II STAGE 2 8. DATUM FOR ELEVATION SHOWN: see level	
2. LOCATION: Flightline Area 9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Dril	l B-61
3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO. OF SAMPLES TAKEN: 10	
4. HOLE NO.: LF04-04 11. ELEVATION GROUND WATER: 595.32 ft MSL (6/18/90)	
5. NAME OF GEOLOGIST: S. E. Fain 12. DATE HOLE ESTABLISHED: 3/20/90	
6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 609.40 ft MSL	
X: 2021365.82 Y: 397554.53 14. BACKGROUND:	
15. MEASURING POINT ELEVATION: 612.07 ft MSL	
Depth Graphic Blow Soil	1
	i
25 U/MARL Limestone: (Marl) White/gray with iron staining in fractures, indurated, shaley parting. 1	well ft.; 50 0 in.;

DRILL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
1. PR	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 26.1 ft BGL	
		PHASE II	_		8. DATUM FOR ELEVATION SHOWN: sea level	
2. LC	CATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 12	
4. HC	DLE NO.: L	F04-05			11. ELEVATION GROUND WATER:	
			B. Blount		12. DATE HOLE ESTABLISHED: 3/28/90	
6. CC	ORDINATES	OF HOLE:			13. SURFACE ELEVATION: 608.80 ft MSL	
х:	2020805.	42 Y:	397347.91		14. BACKGROUND:	
	-			_	15. MEASURING POINT ELEVATION:	-
epth	Graphic	Blow	Soil			1
Ft.)	Log	Count	Class/Code	Visual Descr	iption	Remarks
0	///		U/CLLR	Clay: Dark b	rown grading to brown and orange mottled,	Full samplers
	Y///		i	fine roots,	soft to firm, damp, silty with minor (< 5%)	unles noted
i	Y///		i	calcareous d	lebris and carbonaceous streaking.	otherwise.
	Y///		i	İ		İ
2	Y//A		U/CLLR	Clay: As abo	ove, calcareous debris in small caliche	1 ft. Recovery.
	Y//A		ĺ	pockets (<5	mm).	İ
	$V//\lambda$		i	ï		İ
	$V//\lambda$		i	i		i
4	$V//\lambda$		U/CLLR	Clay: As abo	ove, calcareous debris zone 4.6 - 4.9 ft.,	1 ft. Recovery.
	///		1		ess than 5%; softer, moist.	1
			i	1	,	İ
			1	1		j I
6			I U/CLLR	 Clave As abo	ove, mottling decreased - uniform orange	
0			1 0/000	•	areous debris and rootlets < 2%; increased	I RECOVERY.
	Y///		i	•	-	j i
	Y///		!	I SILE TO BLING	ost clayey silt.	İ
	Y///		į	1		
	Y//A		ļ	I .		ļ
		1		10-4 7-4		14.5.44
8.8			U/SDSH		uff at 8.8 ft.; very fine to fine grained,	1.5 ft. Recovery,
			Į.	•	poor sorting, subangular, quartzose with >	Very sharp contac
			1		and heavy minerals, very loose, damp, minor	sample disturbed
			ļ	clay lenses	at top, few coarse shell fragments.	(in pile).
			1			ļ
11.1	1.0.0.0		U/SDGR	Sand and Gra	evel: at 11.1 ft. sand is as above, oxidized	1 ft. Recovery.
	0.0.0		1	orange, wet,	, very poorly sorted; gravel is - 30%,	
			1	average 10 m	nm, CaCO3, minor clay makes entire sample	
	0.0.0		1	fairly cohes	sive; Clay increases to 13 ft.	1
12	h.n.n		U/GRSM	Gravel, Sand	d, and Clay: As above, gravel up 40%.	Water in hole at
	0.000		1	1		12 ft.; W. L. =
	0.0.0		1	1		12.72 ft., 13 to
	1.0.0.0	1	1	1		ft. no recovery.
14	0.0.0	Ì	U/GRSM	Gravel and S	Sand: As above, with minor clay.	1
16	0.000	}	U/GRSM	Gravel and S	Sand: Orange, 60% + gravel, average 20 mm up	Poor recovery;
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		İ	to 80 mm; ve	ery poor sorting, subrounded; coarse	gravet stipped ou
	0.0.0		ĺ		edominantly CaCO3 frags; finer fraction	1
	1.0.0.0	1	i	•	ly variclored subrounded quartz grains; some	Ī
	0.00	}	i	•	frags (sand sized), very loose; wet.	i
	10.0.0	1	i	1	,	i
19	0.0.0	1	U/GRSM	 Gravet and 9	Sand: As above, gravel is 'coarse' as above	 Possibly gravel
	.0.0.0	ł	1 3,0,0,		0 mm; sand is fine to coarse grained,	only; sample poor
	0.0.0	}	i	•	loose, wet, very porly sorted, subangular.	sand recovered ma
		1			totoly set; tery porty our tedy amonguture	be sluff.
	.O.O.	1	1	1		1
	0.0.0	}	l I	j I		1
	1.0.0.0	1	I	I		I

between lamina, harder to base (clay-like at top), blows went < 0.1							
1. PROJECT: CARSWELL AFB, 7. TOTAL DEPTH OF HOLE: 26.1 ft BGL	DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS	
2. LOCATION: Flightline Area 9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61							
2. LOCATION: Flightline Area 9. MANUFACTURER'S DESIGNATION OF DRILL; Mobile Drill B-61 3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO, OF SAMPLES TAKEN: 12 4. NOLE NO. : LFOA-05 11. ELEVATION GROUND WATER: 5. MAME OF GEOLOGIST: S. B. BLOUNT 12. DATE HOLE ESTABLISHED: 3/28/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 608.80 ft MSL X: 2020805.42 Y: 397347.91 14. BACKGROUND: Depth Graphic Blow Soil (Ft.) Log Count Class/Code Visual Description Remarks 15. MEASURING POINT ELEVATION: 16. COUNT Class/Code Visual Description 17. MEASURING POINT SAMPLES AND AND AND AND AND AND AND AND AND AND	IRP PHASE II STAGE 2						
11. ELEVATION GROUND MATER: 5. NAME OF GEOLOGIST: S. B. Blount 12. DATE MOLE ESTABLISHED: 3/28/90 6. COORDINATES OF HOLE:			-		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
11. ELEVATION GROUND MATER: 5. NAME OF GEOLOGIST: S. B. Blount 12. DATE MOLE ESTABLISHED: 3/28/90 6. COORDINATES OF HOLE:	3. DRILLING AGE	NCY: Envir	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 12		
12. DATE HOLE ESTABLISHED: 3/28/90	-				11. ELEVATION GROUND WATER:		
X: 2020805.42 Y: 397347.91 14. BACKGROUND: 15. MEASURING POINT ELEVATION:	5. NAME OF GEOL	OGIST: S.	B. Blount				
15. MEASURING POINT ELEVATION:	6. COORDINATES	OF HOLE:			13. SURFACE ELEVATION: 608.80 ft MSL		
Depth Graphic Blow Soil	x: 2020805.	42 Y:	397347.91		14. BACKGROUND:		
Count Class/Code Visual Description Remarks					1 15. MEASURING POINT ELEVATION:	1	
U/GRSM Gravel and Sand: As above, good coarsening downward seq., fine to medium grained sand to sand and gravel to clean fine gravel to coarse gravel; sand is same as 11 to 12 ft. 25.8	Depth Graphic	Blow	Soil	1		1	
U/GRSM Gravel and Sand: As above, good coarsening downward seq., fine to medium grained sand to sand and gravel to clean fine gravel to coarse gravel; sand is same as 11 to 12 ft. 25.8	(Ft.) Log	Count	Class/Code	Visual Descr	iption	Remarks	
	24	50	 	seq., fine t clean fine g to 12 ft. Marl: Highly shaley clay; between lami	o medium grained sand to sand and gravel to ravel to coarse gravel; sand is same as 11 calcareous, fissile, semi-indurated, light to medium grey, heavily oxidized na, harder to base (clay-like at top),	Refused at 26 ft. Went in with SS; 50 blows went < 0.1 ft. Abundant coarse gravel on augers when removed. T.D. at 26.1 ft. Hole caved to 14.5 ft. after auger	

DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS	
1. P	ROJECT: CAR	RSWELL AFB,			7. TOTAL DEPTH OF HOLE: 31.5 ft BGL		
IRP PHASE 11 STAGE 2					8. DATUM FOR ELEVATION SHOWN: sea level		
2. L	OCATION:	Flightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. D	RILLING AGE	NCY: Envi	ronmental Dri	tlers, Inc.	10. NO. OF SAMPLES TAKEN: 13		
1 4. H	OLE NO.:	F04-06	-		11. ELEVATION GROUND WATER:		
_5. N	AME OF GEOL	.ogist: s.	B. Blount		12. DATE HOLE ESTABLISHED: 3/28/90		
6. C	DORDINATES	OF HOLE:			13. SURFACE ELEVATION: 613.30 ft MSL		
x:	2020593.	.25 Y:	397210.60	·	14. BACKGROUND:		
<u></u>					15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1	-	1	
(Ft.)	Log	Count	Class/Code	 Visual Descr	iption	Remarks	
0	7//	_	U/CLLR	Clay: Brown,	soft to firm, semi-plastic, sandy in	Full recovery	
Ì	Y///	Ì	i	intervals (1	- 1.5 ft.), roots, moist, minor calcareous	unless noted	
i	Y///		i	flecks.		otherwise. 1 ft.	
Í	Y///		j	i		Recovery.	
) 2	Y///		U/CLLR	Clay: As abo	ve.	i	
i			ĺ	i		i	
i			i	i		i	
3.3	V///		U/CLLR	Clay: Brown.	firm semi-brittle, abundant calcareous	i	
i			i	•	to damp, minor roots, caliche zone to 5.4	i	
i			i		is dry, white/brown mottled, brittle,	i	
i			1	•	alcareous and carbonareous debris.	,	
5.4			U/SAND	•	, very fine grained, subrounded, moderately	 Sharp_contact.	
1			1		tzose w/ < 95% quartz, dry, loose w/ minor	1	
;			i		w shell fragments < 3 mm.	1	
i		}	1	1	a officer if agriculta - 5 april	1	
1			!	1		j 	
1 8		፡ ነ	U/SDLR		ve, clayey soil horizion at top with	Musky odor.	
;	0.0.0) 0/30EK		careous), roots.	Indaky oddi.	
İ	000	}	1	pesotes (car	corecto, rocto.	1	
i	0.0.0	1	1	1		1	
1 10	0.0.0		U/SDLR	 Sand: As abo	ve, thin pebble layer at 10.2 - 10.5 ft.	I ST refusal at 12	
.0		3	1 U/SULK		· · · · · · · · · · · · · · · · · · ·		
1	1.0.0.0		1		careous and up to 15 mm); sand below very	ft.; drive SS.	
1	0.0.0	}	1		with some coarser fraction, poorly sorted,		
1	1.0.0.0	1	1		ous pebbles < 10 mm, minor shell frags,		
	0.00		1	Isingle grave	i clast - 25 mm.	1	
1	1.0.0.0	1	1	ļ			
!	6.0.0	1	1	1		I	
1		4				1	
14		1	U/SDLR	Sand: As abo	ve.	1	
!	\mathcal{V}	1	1	1		Į.	
1	1.0.0.0	1	I	1		!	
	b.0.0		1	1	,,	1	
16	1.0.0.0	1	U/SDLR	•	r-orange, very fine grained, subangular,	!	
1	0.0.0	[1		ell sorted, quartzose > 95% quartz, loose,	I .	
!	1.0.0.1	1	!	:	5 ft., moist to wet to 19 ft., wet below;	!	
Į	hinin	1	ļ.	•	< 1% throughout; color	<u> </u>	
[ł	İ	laminations/	mottling, coarsening downward.	1	
1		1	1	I		ļ	
1	h.n.o	ļ	1	1			
1	1.0.0.0	1	1	1			
20	p.0.0	1	U/SDLR	Sand: Light	brown/tan, very fine to medium grained,	Water in hole at	
1	1.0.0.0	1	1	very poorly	sorted, angular, quartzose with 5 - 10%	20 ft. Sand and	
1	b.0.0)	1	heavy minera	ils, loose, saturated, rock fragments (very	gravel.	
1	1.0.0.	4	1	coarse sand/	fine pebbles) increase to base ~ 25% from		
		1				•	

			1	OF 3 000000	
DRILLING LOG RADIAN CORPORATION 1. PROJECT: CARSWELL AFB, IRP PHASE II STAGE 2 2. LOCATION: Flightline Area			INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 2 SHEETS 7. TOTAL DEPTH OF HOLE: 31.5 ft BGL		
			9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
			3. DRILLING AGENCY: Envir	<u>ronmental Dri</u>	tters, Inc.
4. HOLE NO.: LF04-06			11. ELEVATION GROUND WATER:		
5. NAME OF GEOLOGIST: S.	8. Blount		12. DATE HOLE ESTABLISHED: 3/28/90	_	
6. COORDINATES OF HOLE:		•	13. SURFACE ELEVATION: 613.30 ft MSL		
X: 2020593.25 Y:	397210.60		14. BACKGROUND:		
		•	15. MEASURING POINT ELEVATION:	<u> </u>	
epth Graphic Blow	Soil	i i		1	
Ft.) Log Count	Class/Code			Remarks	
25.21.00.00.00.00.00.00.00.00.00.00.00.00.00	U/SDLR U/GRSM	 Sand: As abo Gravel and S 30 mm, compo	eve. Sand: Gravel is very poorly sorted from 2 to used of quartz, calcareous lithoclasts and ents. Sand is as above.		
29.6	 U/GRSM 	 Gravel, Sand soft.	d, and Clay: Highly calcareous, chalky,		
31	U/MARL	•	e, indurated, light grey, calcareous,	Refused at 31 ft.	
1	1	•	sley. (Minor marly frags at bottom of sample	•	
1 1) 	= basis for		with SS. Cave in.	
	! }	1- 50313 101	ocaci ipi ioni,	Will enter with bit	
1]	1		,	
1 1	ļ	<u> </u>		and obtain solid	
	!	ļ.		bit refusal. Entire	
i i	!	ļ		recovery fell;	
	1	1		Driller says bit	
	ł	1		refusal at 31.5 ft.	
	1	ı		T.D. at 31.5 ft.	
1 1	l			4	
		1		}	
	 	1		-	
	; ;	1			
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	 			1 	

DRILLING LOG RADI			INSTALLATION: CARSWELL AFB, TX SHEET	1 OF 2 SHEETS	
1. PROJECT: CARSWELL A	FB,		7. TOTAL DEPTH OF HOLE: 39.1 ft BGL		
IRP PHASE	II STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: Flightli	ne Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DRILLING AGENCY: E	nvironmental Dr	illers, Inc.	10. NO. OF SAMPLES TAKEN: 15		
4. HOLE NO .: LF04-07			11. ELEVATION GROUND WATER:		
5. NAME OF GEOLOGIST:	S. E. Fain		12. DATE HOLE ESTABLISHED: 3/19/90		
6. COORDINATES OF HOLE	•		13. SURFACE ELEVATION: 630.40 ft MSL		
X: 2020897.22 Y	: 396819.74		14. BACKGROUND:		
	_		15. MEASURING POINT ELEVATION:		
epth Graphic Blo	₩ Soil	1			
Ft.) Log Coun	t Class/Code	Visual Descr	iption	Remarks	
0	U/CLLR 	•	crown, silty, firm to stiff, damp, roots; modules abundant 3 - 4 ft., carbonaceous	Full sample recoveries unless noted. 1 ft. Recovery.	
•	 U/CLLR 	 Clay: As abo	ove, Orange/Brown, getting siltier, stiff.		
6.5	 U/SILT 	abundant cal	e/Brown with very fine sand, dry, cohesive, careous nodules and infilled fissures, s staining in laminae.		
9.8	 U/SDVF 	 Sand: Tan, v	very fine grained, loose, dry, well sorted.	 Pushed 1.5 ft. SS. sampler.	
10	l U/SDVF	Sand: As abo	ve. drv.	1.5 ft. Recovery.	
15	U/SDVF	Send: As abo	ove, slightly indurated in places.	2.5 ft. Recovery.	
18	 U/SAND 	slightly inc	e/Tan, very fine grained to fine grained durated in places, trough cross-laminated, taining in laminae.		
20	 U/SAND 	 Sand: As abo	ove, dry.	 3.0 ft. Recovery 	
	1	1			

		1		-	1	2.05.0 000000
			CORPORATION	_	· · · · · · · · · · · · · · · · · · ·	2 OF 2 SHEETS
1. P	ROJECT: CARS	-			7. TOTAL DEPTH OF HOLE: 39.1 ft BGL	
IRP PHASE II STAGE 2 2. LOCATION: Flightline Area					8. DATUM FOR ELEVATION SHOWN: sea level	
				<u> </u>	9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 15	
	DLE NO.: LF				11. ELEVATION GROUND WATER:	
	ME OF GEOLG		E. Fain		12. DATE HOLE ESTABLISHED: 3/19/90	
	CORDINATES (13. SURFACE ELEVATION: 630.40 ft MSL	
X:_	2020897.2	<u>22 Y:</u>	396819.74		14. BACKGROUND:	
				 	15. MEASURING POINT ELEVATION:	
	Graphic Log	Blow	Soil Class/Code	 Visual Descr	intion	 Remarks
				1		l l
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			I I	1 1] [
22.2	\		l uzenen	 	Top 50/50 security and the second is second in the second	1
23.7	0.0.0		U/SDGR	•	evel: Tan, 50/50, gravel is mainly granule	1
	0.0.0		I .	:	and shell fragments), loose, dry,	1
	0 0 d			subrounded.		
25	0.0.0		U/SDGR	•	ivel: As above, dry, poorly sorted, very	2.7 Recovery.
	[•,.*•,.*•,		ļ.	fine sand to	pebble size gravel (10 mm).	ļ
	[0,0,0]		I	I		1
	D.O.O.1		1	1		1
			1	1		1
28	, , , , , ,		U/SDVF	Sand: Orange	e, slightly clayey (28 - 29 ft.), damp, ver	v İ
]		í	fine grained		i
			i			i
			1	;		
30			l livenen			
J U	[]		U/SDFN		e/Tan, fine grained, loose, slightly damp,	2.5 ft. Kecovery.
	· · · · .		Į.	well sorted,	quartzose.	
	• • • !		ļ	!		!
			1	ļ.		!
]		1	1		
	1 1		1	1		
33			U/SDFN	Sand: As abo	ove.	1
	1		1	1	·	
	[]		1	1		1
	J		İ	İ		i
35	10.00		U/SDLR	Sand: Orange	e/tan, damp, fine to medium grained, loose;	W. L. measured at
	0.0.0			-	gravel 37 - 38.2 ft., wet, medium to	37.0 ft., 2.5 ft.
	N.O.O.!		i	coarse grain		Recovery, Auger
	10.0.d			1	· -	refusal at 38.5 f
	Þ.Ö.Ö.₹		1 '	1		Treinsarar 2013 T
	0.0.0			1		ļ
	! ``````!		!	Į.		1
	h.O.O.		1	1		1
38.2	i 1 14;	50	U/MARL	•	sh - Gray with oxidation staining,	Drove 15 in. S.S.
	<u> </u>		I	catcareous,	indurated.	50 blows/ 3/4 in.
	1		Ţ	ļ		38.6 ft. T.D.
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DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	OF 3 SHEETS
1. PROJECT: CAR	-			7. TOTAL DEPTH OF HOLE: 47.4 ft BGL	
	PHASE II			8. DATUM FOR ELEVATION SHOWN: sea level	
2. LOCATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DRILLING AGE	NCY: Envi	<u>ironmental Dri</u>	illers, Inc.	10. NO. OF SAMPLES TAKEN: 17	
4. HOLE NO.: L	F04-08			11. ELEVATION GROUND WATER:	
5. NAME OF GEOL		. E. Fain		12. DATE HOLE ESTABLISHED: 3/19/90	
6. COORDINATES				13. SURFACE ELEVATION: 630.00 ft MSL	
x: 2020021.	91 Y:	396935.08		14. BACKGROUND:	
				15. MEASURING POINT ELEVATION:	
epth Graphic	Blow	Soil	!		!
Ft.) Log	Count		Visual Descr		Remarks
° [///		U/CLAY	Clay: Dark B nodules at 3	rown, stiff, damp, roots, calcareous .5 - 4.0 ft.	Full sample recoveries unless
$-Y//\lambda$		i	i		noted.
$-Y//\lambda$		i	i		i
2 ///		U/CLLR	Clay: As abo	we, silty.	İ
		İ	Ì		İ
- V//X		İ	Ī		İ
$-V//\lambda$		İ	1		İ
- 1///		Ì	1		İ
- V//X		1	1		İ
5		U/SILT	Silt: Orange	e, sandy (very fine grained), dry, cohesive,	No Recovery; could
		j	carbonaceous		not get sample out
		1	1		of shelby tube,
		j	Ì		Description based
		İ	j		on top and bottom
		İ	İ		of sample.
		i	Ì		İ
8.1		U/SDFN	Sand: Orange	e/tan, fine grained, loose, dry, well	i
		İ		ound, quartzose.	İ
		İ	İ		İ
10		U/SDFN	Sand: As abo	ove, horizontal bedding seen in/as minor	İ
		i	1	es, dry; going to tan at 12 ft.	i
		i	i		i
		i	i		i
• • • •		i	i		i
		i	i		İ
		i	i		1
		i	i		i
14		I U/SDFN	Sand: As abo	ove.	
					sampler at 14 ft.
		i	i		3 ft. Recovery.
		i	i		
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		i	i		
		i	i		i
17		I U/SAND		very fine to fine grained, dry to slightly	
		5,500,00	•	quartz, subangular to subround, frosted.	1
		i			1
			1		1
19		I U/SAND	 Sand: Ac sh	ove, still dry, mainly fine grained.	
· · · · · · · · · · · · · · · · · · ·		l O/SAND	juenu. As abt	ore, stitt dry, mainty fine grained.	J.J IL. RECOVERY.
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	1				•
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DRILL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 3 SHEETS
1. PR	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 47.4 ft BGL	
<u> </u>	IRP	PHASE II S	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
1 2. LC	CATION: F	lightline /	Агеа		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
1 3. DR	RILLING AGE	NCY: Envi	ronmental Dr <u>i</u>	llers, Inc.	10. NO. OF SAMPLES TAKEN: 17	
1 4. HC	DLE NO .: L	F04-08		<u>-</u>	11. ELEVATION GROUND WATER:	
1 5. NA	ME OF GEOL	OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/19/90	
6. CC	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 630.00 ft MSL	
1 X:	2020021.	91 Y:	396935.08		14. BACKGROUND:	
					15. MEASURING POINT ELEVATION:	
Depth	Graphic	Blow	Soil	1		1
(Ft.)	Log	Count	Class/Code	Visual Descr	<u>iption</u>	Remarks
! !			ļ	!		ļ
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!	[· · · · .]		1	ļ.		ļ
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			!	<u> </u>		!
_			1			
24			U/SAND	Sand: As abo	ve.	1
						1
	<u> :-:-:</u>					
25.2			U/SDLR	:	•	3.2 ft. Recovery
! !	$\dot{\alpha}$		ļ	•	to slightly damp, gravel mostly chert, 0.1	ļ
			1	•	ssilferous limestone bed at 28 ft. Tan fine	1
ļ ļ			l	sand 28.1 ft	. to 29 ft.; gravels - 5% - 10%.	1
ļ į	h.h.h		ļ	ļ		
!	0.0.0		!	!		1
!	0.0.0		!	!		!
29	0.0.0		U/SDLR	•	ine to medium grained, loose, dry,	4 ft. Recovery
ļ	0.0.0		!	quartzose, 1	- 3% chert gravel.	
. !	0.0.0		ļ	!		ļ
ļ	0.0.0		ļ.	!		ļ
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1		!		!		ļ
Ţ	M^{M}		!	ļ		İ.
	1.0.0.0		Ī	ļ.		İ
33	[0.0.0]		U/SDLR	•	ove, increasing gravel to 5 - 10% at 33 - 34	İ
	1.0.0.0		!	ft.		İ
34	[0.0.0]		U/SOLR	Sand: As abo	we, wet, fine to medium grained.	W. L. measured at
!	0.00		!	!		35.2 ft. BLS 1.5
ļ	0.0.0		ļ			ft. Recovery.
!	$\cdot 0 \cdot 0 \cdot 0$		ļ	!		!
ļ			!	!		!
	0.0.0		1	<u> </u>		1
37			U/MARL	•	fossiliferous, weathered; intermixed with	Not good limestone
ļ	\mathbf{r}		!	•	evel, wet, gravels are granule and pebble	or shale. Still
ļ.			!	size, mainly	chert.	significant sand
				I .		and gravel.
39	 		U/MARL	•	meds and gravel size pieces of limestone	3.6 ft. Recovery.
!		[ļ	intermixed w	ith sand, gravel, and shells, wet, shaley.	!
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ORILLING LOG RADIAN CO	ORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	3 OF 3 SHEETS
1. PROJECT: CARSWELL AFB,	JAI GRAITE		7. TOTAL DEPTH OF HOLE: 47.4 ft BGL	1
IRP PHASE II S	TAGE 2	•	8. DATUM FOR ELEVATION SHOWN: sea level	
2. LOCATION: Flightline A			9. MANUFACTURER'S DESIGNATION OF DRILL:	
3. DRILLING AGENCY: Enviro			10. NO. OF SAMPLES TAKEN: 17	1
4. HOLE NO.: LF04-08			11. ELEVATION GROUND WATER:	
5. NAME OF GEOLOGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/19/90	
6. COORDINATES OF HOLE:			13. SURFACE ELEVATION: 630.00 ft MSL	
X: 2020021.91 Y:	396935.08	· ·	14. BACKGROUND:	
1			15. MEASURING POINT ELEVATION:	
Depth Graphic Blow	Soil	<u> </u>		
		Visual <u>Descr</u>	ription	Remarks
				1
44	U/MARL U/SHLE	 Marl: As abo ft.) intermi	ove, indurated limestone beds (0.1 - 0.3 xed with gravelly sand. Gray, indurated, fissile, no fossils,	Drilling through mart, looking for auger refusal. Auger refusal at 47 ft.; 50 blows for 0.4 ft.; T.D. = 47.4 ft.
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DRILLING LOG	RADIAN CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 3 SHEETS
1. PROJECT: CARSWE	LL AFB,		7. TOTAL DEPTH OF HOLE: 47.0 ft BGL	_
IRP PH	ASE II STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
2. LOCATION: Fligh	htline Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DRILLING AGENCY	: Environmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 17	
4. HOLE NO.: LF04	-09	_	11. ELEVATION GROUND WATER:	
5. NAME OF GEOLOGIS	ST: S. E. Fain		12. DATE HOLE ESTABLISHED: 3/6/90	
6. COORDINATES OF	HOLE:		13. SURFACE ELEVATION: 627.40 ft MSL	
X: 2021145.70	Y: 397136.15	-	14. BACKGROUND:	
<u></u>			15. MEASURING POINT ELEVATION:	
Depth Graphic	Blow Soil	!		ļ
. 777		Visual Descr		Remarks
	U/CLLR 	•	going to red/brown at 2 ft., silty, moist; ry, crumbly, very stiff, roots, minor staining.	Top soil first 1 ft.; Using 5 ft. S.S. sampler; 4 in. O.D., 3 1/2 in. I.D.
4	 U/CLLR 	calcareous n	silty, minor very fine grained sand, codules 5 - 5.2 ft., carbonaceous staining s, increasing very fine grained sand at 7.5	;
8	 U/CLLR 	 Clay: As abo 	ve, Red and Brown mottled, dry.	
9.6	 U/SAND 	Sand: Orange damp, loose.	e, very fine to fine grained, quartzose,	 3.5 ft. Recovery (9 - 12.5 ft.).
11.5 0.0.0	U/SDGR 		evel: Orange/tan, poorly sorted, loose, was shells, gravels to 20 mm.	
14	 U/SAND 		tan, very fine to medium grained, loose, mineralogies.	 2.5 ft. Recovery.
16 .0.0.0	 U/SDGR 	•	evel: Tan, very fine sand - pebble size se, damp, numerous shells, various	
17	U/SDVF 	Sand: Tan, v	very fine grained, quartzose, loose, dry, subround, slightly indurated and laminated	}
19 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	U/SDGR 	Sand and Gra	ovel: Orange/tan, poorly sorted, 50% sand - numerous pelycepod? shells, loose, damp; an clay seam at 22 ft.; gravels to 30 mm,	3.5 Recovery.

1 68***		I penanti			I THOUTHING CONCERN APP TO I CHEET A	OF 7 CHEETE	
-	LING LOG		CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 3 SHEETS		
1. Pi	ROJECT: CARS	•	STACE 3		7. TOTAL DEPTH OF HOLE: 47.0 ft BGL		
12 14	DCATION: FI	PHASE II S			8. DATUM FOR ELEVATION SHOWN: see Level 9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61		
			ronmental Dri	liers inc	1 10. NO. OF SAMPLES TAKEN: 17	SOUTH DE DE LE DE DE LE	
	OLE NO.: LI		Ortherical Diri	ccers, iic.	11. ELEVATION GROUND WATER:		
-	AME OF GEOLG		F Fain		12. DATE HOLE ESTABLISHED: 3/6/90	· · · · · · · · · · · · · · · · · · ·	
-	OORDINATES (13. SURFACE ELEVATION: 627.40 ft MSL		
	2021145.7		397136.15		14. BACKGROUND:	 	
i					15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1	-	1	
<u> (Ft.)</u>		Count	Class/Code	Visual Descr	iption	Remarks	
 25 			 U/SDLR 	•	fine grained, > 90% quartz, dry, loose, well angular to subrounded, minor small gravel.	 3 ft. Recovery. 	
 29 	0.0.0 0.0.0		U/SDLR	 Sand: As abo 	ove, increasing gravel.	! 	
30.5			, U/MARL 	•	-	Still relatively easy drilling.	
32 			U/MARL	•	ove, damp, slightly consolidated, fissile in ious gravel size particles.	Weathered Limestone?	
 34 			 U/MARL 	•		 Wet at 34 ft. (measured W.L. = 33 ft. 10 in.). Still easy drilling. 	
 39 				 	ove.	 	

DRILLING LOG RADIAN CORPORATION				INSTALLATION: CARSWELL AFB, TX SHEET	3 OF 3 SHEETS	
1. PROJECT: CARSWELL AFB,				7. TOTAL DEPTH OF HOLE: 47.0 ft BGL		
IRP PHASE II STAGE 2				8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION:	Flightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DRILLING A	GENCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 17		
4. HOLE NO.:	LF04-09			11. ELEVATION GROUND WATER:		
5. NAME OF GE	OLOGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/6/90		
6. COORDINATE	S OF HOLE:			13. SURFACE ELEVATION: 627.40 ft MSL		
X: 202114	5.70 Y:	397136.15		14. BACKGROUND:		
<u> </u>				15. MEASURING POINT ELEVATION:		
Depth Graphic	Blow	Soil	1			
[(Ft.)] Log	Count	Class/Code	Visual Descr	ription	Remarks	
	Ä	1	}		1	
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i h	πi	İ	į		i	
44		U/MARL	Marl: As abo	ove.	Descriptions based	
	Li .	1	1		on returns and	
i h-1	⊤1	ì	, 		drilling speed.	
` }	<u> </u>	i	ì		Auger refusal at 47	
	Ľ	1	ì			
	T	1			detection (2/9) at	
╏╏	4	1	1		•	
1 47	τ¦	I II/MADI	 Manta An aba		top of auger.	
4/	!	U/MARL	Mart: As abo	ove.	!	
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DRIL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 3 SHEETS	
1. PI	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 49.1 ft BGL	1	
IRP PHASE II STAGE 2				_	8. DATUM FOR ELEVATION SHOWN: sea level		
] 2. L	OCATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DI	RILLING AGE	NCY: Envi	ronmental Dri	llers, inc.	10. NO. OF SAMPLES TAKEN: 18	1	
4. H	DLE NO .: L	.F04 <u>-1</u> 0			11. ELEVATION GROUND WATER: 596.05 ft MS	L (6/18/90)	
5. N/	ME OF GEOL	OGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 4/2/90		
6. C	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 626.90 ft MSL		
X:	2021275.	03 Y:	397025.34		14. BACKGROUND:		
<u></u>					15. MEASURING POINT ELEVATION: 626.54 ft	MSL	
Depth	Graphic	Blow	Soil	1		1	
(Ft.)	Log	Count	Class/Code	Visual Descr	iption	Remarks	
0			U/CLLR	Clay: Brown	With orange mottling, soft to firm, damp,	Full recovery	
	[///]			minor carbon	aceous streaking, semi-plastic, silty seam,	unless otherwise	
1	[///!			(parting) at	1 ft Coaly fragments. 0 to 0.05 ft.	noted. Windy.	
1	/ ///I		1	1			
2	Y///		U/CLLR	Clay: As above	ve, very silty to 3.2 ft., below 3.2 ft.	'Contact' (fill	
1	r///		1	has no silt,	Orange/brown, plastic, firm, minor	material on top?).	
1	Y///		1	carbonaceous	streaking.	1	
1	Y///		1	1		1	
4	Y//A		U/CLLR	Clay: Very s	ilty to 4.7 ft Same as 2 - 3.2 ft		
1	Y//A		1	1		İ	
4.7	$V//\lambda$		U/CLAY	Clay: Burnt o	orange, firm to stiff, semi-plastic, damp	Sharp 'contact'.	
1	$V//\lambda$		1	with carbona	ceous streaking, and minor calcareous		
1	V//X		1	debris; with	calcareous debris concentrated from 5.6 -		
1	///			5.8 ft.	j j		
6	V//)		U/CLAY	Clay: As above	Hard pushing.		
1			1	concentrated	in 'caliche' layer 7.5 - 7.8 ft.		
8			U/SAND	Sand: Very f	Sharp contact, 1.5		
1			1	sub-rounded,	Burnt Orange (oxidized), slightly silty in	Recovery (sand);	
1)			intervals (le	enses); clay pocket (dark grey/soft) at 8.5	sand is loose,	
1)		1	ft.; sand has	v very minor carbonaceous streaks, damp,	cohesive w/ clay in	
1))		1	moist, at bas	se; quartzose w/ < 95% quartz, < 5% iron	lenses.	
	• • • •			magnesium.		ĺ	
10)		U/SDSM	Sand: As above	ve, slightly silty to 11 ft., oxidation	1.5 ft. Recovery.	
1			1	decreasing to	o base with color laminations evident. Clay	j j	
1	• • • •		1	lenses at 10	- 10.1 ft. and 10.6 - 10.7 ft.; sand is	İ	
1			1	buff yellow	at 11 ft	i i	
12			U/SDSM	Sand: As above	ve, lighter color (buff tan), silty	Pushed SS to 14	
1			1	interval 13	- 13.3 ft., minor color taminae.	ft.; going to	
1)' . ' . ' . ' <u> </u>		1	l		augers.	
14			U/SDSM	Sand: As above	ve, minor clayey lenses, semi-indurated	2.5 ft. Recovery -	
1	• • • •		I	sandstone la	yer at 14.9 - 15 ft.; damp, loose; with	Moss.	
1			1	color lamina	e and < 5% heavy minerals.	j i	
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İ			İ	İ		į i	
19			U/SDSM	Sand: Very f	ine grained, buff w/ orange clay lenses,	4.5 ft. Recovery.	
ĺ	• • • •			•	t, brittle, sandy, dark orange/brown, sand		
i			i	1	y to poorly sorted, buff, grading to	. !	
i			i		y from 19 - 19.5 ft. and 20.5 - 22.5 ft.,	i i	
i] • • • •		i		No clay below 22.5 ft., very minor	'	
i			i	calcareous fi		, 	
•			1	,	·	. '	

1 00111					I INCTALLATION, CAROCTIL APP. TV. I CHEFT 2	OF 7 OUESTS		
-	LING LOG		CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 3 SHEETS			
1. PROJECT: CARSWELL AFB,					7. TOTAL DEPTH OF HOLE: 49.1 ft BGL 8. DATUM FOR ELEVATION SHOWN: sea level			
IRP PHASE II STAGE 2 2. LOCATION: Flightline Area					9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61			
-				liers inc.	10. NO. OF SAMPLES TAKEN: 18			
3. DRILLING AGENCY: Environmental Drillers, Inc. 4. HOLE NO.: LF04-10					11. ELEVATION GROUND WATER: 596.05 ft MSL (6/18/90)			
-	AME OF GEOLG		R. Rigunt		12. DATE HOLE ESTABLISHED: 4/2/90			
-	CORDINATES (D. Drogn		13. SURFACE ELEVATION: 626.90 ft MSL			
X:		03 Y:	397025.34	•	14. BACKGROUND:			
1		<u></u>				15. MEASURING POINT ELEVATION: 626.54 ft MSL		
Depth	Graphic	Blow	Soil			1		
(Ft.)	Log	Count	Class/Code	Visual Descr	Remarks			
Ī			1	1				
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1	1			1		ĺ		
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1	<u>[</u>]		1	1		1		
24	<u></u>		U/SDLR	Sand: As abo	ve, buff to orange laminated, no clay or	3 ft. Recovery		
	14.4.4		1	silt, very f	ine grained, moderately well sorted, dry to	İ		
				damp; layer of abundant ~ 5% shell frags and calcareous				
	[0:0:9		1	debris with	some gravel from 26 - 26.5 ft.; gravel up			
	b.0.0.1			to 40 mm, mi	nor gravel fragments to base.	ĺ		
	10.0.d		Ì	1		Ì		
	0.0.0.1		1	1		1		
	lo o d		1	1		1		
	5.0.0.			1				
1	0.0.0		Ì	1		Ì		
29	1		U/SDLR Sand: As a		ve.	4.5 ft. Recovery.		
}			i	1		İ		
	[0.0.d		1	1		1		
30.5	0.0.0		U/SDGR	Sand and Gravel: Sand is very poorly sorted, buff, very		Sample wet at 32		
1	0.0.d		1	fine to coar	se grained, subrounded, with minor	lft		
	D.O.O.		1	loxidation se	oxidation seams, gravel is 2 - 100 mm, approximatly			
	10.0.d		1	50%, compose	0%, composed of calcareous debris of shells etc. up to			
	5.0.0.1		1	5 mm; large	fragments are broken, well indurated	1		
	lood		1	micritic lim	estone.	1		
33	0.0.0		U/SDLR	Sand: Tan, m	medium grained with abundant carbonaceous	Cobbles lengthwise		
1	12,27,4		1	streaking an	d gravel, as above, at base.	in sampler.		
34	0.0.0		U/GRSM	Sand and Gra	vel: Sand as above up to 15% gravel is	1		
!	0.00		1	quartz and c	alcareous debris, averaging 5 mm and up to			
Į.	[0.0.0]		1	40 mm. Moder	ate to poor sorting, subrounded, wet. Large	Į.		
ļ.	D.O.O.		I	fragments ar	e CaCO3, as above. Grain size increases to	<u> </u>		
ļ	10.0.d		1	base.		,		
	0.0.0		1	1				
1	10.0.0		1	Ţ				
1	5.0.0.1		1					
1	0.0.0		I	1				
39	5.0.0.		U/SDGR	Sand and Gra	ivel: As above, wet, averaging 10 - 15 mm.	2.5 ft. Recovery.		
!	12 2 4		1	Continues co	parsening to base, minor clay pockets 40 -			
!	0.0.0		1	42 ft. makir	ng fine gravel/slightly cohesive. Gravel up	1		
1	5.0.0.		1	to 50 mm. Co	parse Sand.			
1	10.0.a		1	1		1		
1	p.0.0.1		1	1		1		
!	0.0.0		1	1		1		
1	5.0.0.1		1	1		1		
		_						

					64 814	
DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 3	OF 3 SHEETS	
1. PROJECT: CARS	WELL AFB,			7. TOTAL DEPTH OF HOLE: 49.1 ft BGL		
IRP_IRP	PHASE II	STAGE 2	<u></u>	8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: FL	ightline .	Area		9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61		
3. DRILLING AGEN	ICY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 18		
4. HOLE NO.: LF	04-10			11. ELEVATION GROUND WATER: 596.05 ft MSL (6/18/90)		
5. NAME OF GEOLO	GIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 4/2/90		
6. COORDINATES O	F HOLE:			13. SURFACE ELEVATION: 626.90 ft MSL		
X: 2021275.0	3 Y:	397025.34		14. BACKGROUND:		
1				15. MEASURING POINT ELEVATION: 626.54 ft	MSL	
Depth Graphic	Blow	Soil	1		1	
(Ft.) Log	Count	Class/Code	Visual Descr	<u>iption</u>	Remarks	
0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.] - - - - -	wet, grey tal (< 5 mm) arous carbonaceous layer 46.5 -		not 'sandy'; has few grains in each 'pocket'. 	
			•	coated micritic limestone w/ ed fossils, grey to buff, well indurated,	49 - 49.1 ft. augered into marl; 'core' sample. No SS. T.D. at 49.1 ft.	

RILLING LOG	RADIAN CORPORATION	INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
. PROJECT: CARS	WELL AFB,	7. TOTAL DEPTH OF HOLE: 25.2 ft BGL	
IRP	PHASE II STAGE 2	8. DATUM FOR ELEVATION SHOWN: sea level	
LOCATION: FL	ightline Area	9. MANUFACTURER'S DESIGNATION OF DRILL:	<u>Mobile Drill B-61</u>
. DRILLING AGEN	CY: Environmental Dr	illers, Inc. 10. NO. OF SAMPLES TAKEN: 11	
. HOLE NO .: LF	05-01	11. ELEVATION GROUND WATER: 603.82 ft MS	SL (6/18/90)
. NAME OF GEOLO	GIST: S. E. Fain	12. DATE HOLE ESTABLISHED: 3/22/90	
. COORDINATES C	F HOLE:	13. SURFACE ELEVATION: 619.30 ft MSL	
X: 2018791.3	8 Y: 399361.24	14. BACKGROUND:	
	<u> </u>	15. MEASURING POINT ELEVATION: 621.96 ft	MSL
pth Graphic	Blow Soil		1
t.) Log	Count Class/Code	Visual Description	Remarks
	U/CLLR	Clay: Dark brown, firm, silty, red mottling, roots,	Fill.
- (///	1	damp; minor sand and gravet.	1
	<u> </u>	I	1
	l l	1	
			I .
[U/SDLR		1
0.0.0	ļ	small gravel.	!
1.0.0.0	!	!	Ţ
<u> 0.0.0</u>	<u> </u>		1
	U/CLLR	Clay: As above, damp.	1.2 ft. Recovery.
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-Y//A			ĺ
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	i	i	i
	i	i	İ
	i		:
	¦		-
		Class Brown and aromas massland constitutions of	10.711.4711
' ///	U/CLLR	Clay: Brown and orange, mottled, very disturbed,	Still fill
Y//A	ļ.	gravelly, soft to slightly firm, calcareous zones and	material.
$-V//\lambda$!	nodules, damp; at 11 ft. going into a gray colored	ļ
- ///	ļ	silty clay.	1
			1
			1
2 ///	U/CLLR	Clay: As above; at 13.5 ft. hard limestone zone.	0.2 ft. Recovery.
	İ		i
	i	i	i
$-Y//\lambda$			1
4 ///	I U/CLLR	Clay: As above, still very disturbed.	1
* V//X	l OVERTI	ictor. As above, still very disturbed.	I
	į I		!
	Į.	!	!
. [///]	· !		Ţ
6 ///	U/CLLR	Clay: As above, damp.	1
			1
$-Y//\lambda$	1	1	1
$V//\lambda$			1
-V//X	į	1	i
8.1	U/SDSM	Sand: Light brown, very silty and clayey, saturated,	 Very "muddy".
	-,	minor small gravel, < 1% pebbles.	
-	! 		1
20	 Hannes	 Sanda da abaya	1
·~ . · · · · .	U/SDSM	Sand: As above.	Į,
!	ļ	!	ļ
	ļ.	!	
1 1	1		•

DRIL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 2 SHEETS		
1. PI	ROJECT: CAR	SWELL AFB,	_		7. TOTAL DEPTH OF HOLE: 25.2 ft BGL		
<u> </u>	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
] 2. L	OCATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 11		
1 4. HO	DLE NO.: L	F05-01			11. ELEVATION GROUND WATER: 603.82 ft MS	L (6/18/90)	
		OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/22/90		
	CORDINATES			-	13. SURFACE ELEVATION: 619.30 ft MSL		
<u> </u>	2018791.	38 Y:	399361.24		14. BACKGROUND:		
<u> </u>					15. MEASURING POINT ELEVATION: 621.96 ft	MSL	
Depth	Graphic	Blow	Soil	1		1	
(Ft.)	Log	Count	Class/Code	Visual Descr	iption	Remarks	
 22 			 U/SDLR 	saturated, s	and Gravel: About equal % of each, shells, gravels to 20 mm, silty; 24.5 - 25 and and gravel.	 Still very "muddy". 	
 25 		50	U/MARL		cone, chalky, indurated, oxidation staining.	MOSS sampler refusal at 25 ft.; drive sample 50 blows = 2 in.; Fill probably ended about 18.1 ft. BLS; hole looked like fill all the way TD. T.D. = 25.2 ft.	

DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS	
	ROJECT: CAR				7. TOTAL DEPTH OF HOLE: 27.2 ft BGL		
<u>i</u>	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
<u>] 2. L</u>	OCATION: F	lightline .	Area		9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61		
13. D	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 13		
14. H	OLE NO.: L	<u> F05-02</u>			11. ELEVATION GROUND WATER: 597.83 ft MS	L (6/18/90)	
15. N	AME OF GEOL	OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/22/90		
6. C	OORDINATES	OF HOLE:			13. SURFACE ELEVATION: 620.30 ft MSL		
X:	2019492.	00 Y:	399280.64		14. BACKGROUND:		
<u> </u>					15. MEASURING POINT ELEVATION: 622.69 ft	MSL	
:	Graphic		:				
-	Log	Count	-	Visual Descr		Remarks	
0			•	•	• •	Full sampler	
ţ			!	material, da	mp.	unless noted.	
!			1	ļ		1	
1			1		. 654	10.0 (0.00000000000000000000000000000000	
2			U/CLLR	Clay: As abo	ove, 0.5 ft. caliche zone 3 - 3.5 ft.	1.2 ft. Recovery.	
1			!	1		1	
1			!	1		1	
 4			 U/CLLR	ICIave Bank b	prown, stiff, carbonaceous staining, damp,	 No calcareous	
17) D/CEEK	silty.	nown, still, carbonaceous stalling, daip,	material.	
1			1	1		imace: rac.	
i				! {		1 1	
6			 U/CLLR	Clave As abo	ove, minor gravel, silty.	1	
1			1	I	ric, milo, gravet, sitty.	1	
1	Y///		i i	i		1	
i	Y///		İ	ì		1	
18	Y///		U/CLAY	iclav: Brown	and tan mottled, distrurbed looking (not	Looks like fill	
i	Y///		1		ering), damp; some greenish/gray clay also.	•	
i	Y///		Ì	1	, comp, comp, comp, g, c, c, c, c, c, c, c, c, c, c, c, c, c,		
i	Y///		i	i			
j 10	Y///		U/CLAY	Clay: As abo	ove, soft calcareous zone at 11 ft.	1.0 ft. Recovery.	
į			İ	i	•	İ	
į	Y///		i	İ			
l	Y///	1	Ì	}		İ	
12	Y///		U/CLAY	Clay: Still	heavily disturbed nature, 3 in. wet seam at	Still fill	
1	Y///		1	13 ft.		material.	
1	Y///		1	1		1	
1	Y///			1		1	
14	Y///		U/CLLR	Clay: Becomi	ing siltier, moist, some greenish/gray		
1	V///		l	coloration.			
1	V///		1	1		1	
1	V///		1	1		1	
16	V///		U/CLLR	Clay: Brown	and green mottling, very disturbed nature,	Still looks like	
1	V///	Ĭ	1	gravel (1 -	5%), shells; 0.4 ft. fine sand seam at 16.6	Ifitt.	
1	V///		1	ft.; wet.		1	
ļ	V///		1	1		1	
18	V///		U/CLLR		ove, silty, not disturbed; greenish/gray at	•	
!			ļ.	19 ft.		material looks	
!	V//		1	1		natural - in situ.	
			1	1			
20			U/CLLR	•	ish/gray, silty, oxidation stained mottling,		
Ţ	V///		Į.		1 - 3% assorted size sand and small gravel,		
l l	V///		1	igravelly sar	nd at bottom.	well completion.	
1]	1	Į.		I	

DRILLING LOG RADIAN COMPORATION INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 2 SHEETS					
1. PROJECT: CARSWELL AFB, IRP PHASE II STAGE 2 8. DATUM FOR ELEVATION SHOWM: sea Level	DRILLING LOG PADIAN COR	RPORATION I	I INSTALLATION - CARSUELL AFR TX SHEET 2	OF 2 SHEETS	
IRP PHASE II STAGE 2 8. DATUM FOR ELEVATION SHOWN: see level					
2. LOCATION: Flightline Area 9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61 3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO. OF SAMPLES TAKEN: 13 4. HOLE NO.: LFD5-02 11. ELEVATION GROUND WATER: 597.83 ft MSL (6/18/90) 5. NAME OF GEOLOGIST: S. E. Fain 12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 620.30 ft MSL X: 2019492.00 Y: 399280.64 14. BACKGROUND:					
3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO. OF SAMPLES TAKEN: 13 4. HOLE NO.: LF05-02 11. ELEVATION GROUND MATER: 597.83 ft MSL (6/18/90) 5. MANE OF GEOLOGIST: S. E. Fain 12. DATE MOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 620.30 ft MSL X: 2019492.00 Y: 399280.64 14. BACKGROUND: 15. MEASURING POINT ELEVATION: 622.69 ft MSL Depth Graphic Blow Soil (Ft.) Log Count Class/Code Visual Description Remarks 16. MEASURING POINT ELEVATION: 622.69 ft MSL Count Class/Code Visual Description Remarks 24.9				Mobile Drill B-61	
11. ELEVATION GROUND WATER: 597.83 ft MSL (6/18/90) 5. MAME OF GEOLOGIST: S. E. Fain 12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 620.30 ft MSL				<u> </u>	
12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: X: 2019492.00 Y: 399280.64 14. BACKGRQUND: Depth Graphic Blow Soil (Ft.) Log Count Class/Code Visual Description Remarks 24.9 15. MARSURING POINT ELEVATION: 622.69 ft MSL 24.9 24.9 25. DEPTH Sand and Gravel: Orange/brown, very clayey, saturated,	· · · · · · · · · · · · · · · · · · ·			SL (6/18/90)	
13. SURFACE ELEVATION: 620.30 ft MSL X: 2019492.00 Y: 399280.64 14. BACKGROUND: 15. MEASURING POINT ELEVATION: 622.69 ft MSL	<u>"</u>				
X: 2019492.00 Y: 399280.64 14. BACKGROUND: 15. MEASURING POINT ELEVATION: 622.69 ft MSL					
15. MEASURING POINT ELEVATION: 622.69 ft MSL	•	_		i	
Depth Graphic Blow Soil				: MSL	
24.9 U/SDGR Sand and Gravel: Orange/brown, very clayey, saturated, numerous shell fragments, gravels to 40 mm, mainly limestone clasts. 27	Depth Graphic Blow	Soil		1	
24.9	(Ft.) Log Count Cl	lass/Code Visual Descri	iption	Remarks	
	24.9	U/SDGR Sand and Grave numerous shell timestone cla	vel: Orange/brown, very clayey, saturated, ll fragments, gravels to 40 mm, mainly asts.		

						C-T WIC	
	ING LOG		CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS	
1. PF	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 27.5 ft BGL		
1	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
<u>] 2. LC</u>	OCATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
1 3. DI	RILLING AGE	NCY: Envi	ronmental Dri	illers, Inc.	10. NO. OF SAMPLES TAKEN: 13		
<u>] 4. HC</u>	DLE NO.: L	F05-03			11. ELEVATION GROUND WATER:		
1 5. NA	ME OF GEOL	0G1ST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90	<u> </u>	
6. CC	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 620.60 ft MSL		
<u> </u>	2019488.	64 Y:	399182.10		14. BACKGROUND:	<u> </u>	
<u></u>					15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1		j	
(Ft.)	Log	Count	Class/Code	Visual Descr	·	Remarks	
0	1///		U/CLLR	Clay: Soft -	firm, moist, clay fraction plastic - semi	Full recovery	
]	! ///		!	•	e to roots, calcareous pebbles, slightly	unless otherwise	
1			!	•	layey silt 1.7 - 2 ft., yellow orange	indicated.	
			1	grading to b		Extremely windy.	
2	1///		U/CLLR	Clay: As above	ve, calcareous pebbles concentrated in	Gradational	
[]			1	intervals, l	ess silty, minor carbonaceous streaking at	changes.	
1	Y///		l	base.			
	Y///		1	1		!	
4	Y///		U/CLAY	Clay: As above	ve, Brown, firm, fairly plastic, layers of	}	
j	Y///		1	concentrated	calcareous debris.	1	
]	$Y//\lambda$		I	1			
	$Y//\lambda$		1	1			
6	$Y//\lambda$		U/CLLR	Clay: As above	ve, dark brown, grading darker, soft to	1	
!	V//X		l	•	ew calcareous pebbles, abundant	j	
	V//X		1	carbonaceous	lamina, very few fine rootlets, moist,	1	
<u> </u>	V//\		1	minor silt i	n lenses, plastic - appears organic rich.	1	
1	///		l	1			
1	///		1	1		1	
]]	///)		1	1			
	[///]			1			
10			U/CLLR	Clay: As abor	ve, dark brown, soft, plastic, moist with	Musky odor.	
!			l	silty/sandy	lenses to 13.2 ft.; leached zones 13.2 -	Caliche zones. 1.5	
			1	13.5 ft., 14	.3 - 14.4 ft., clay is white/buff, brittle,	ft. recovery.	
1			1	damp, with m	ore frequent calcareous pebbles,	1	
1	[///		1	intervening	clay is as above; with silt/sand.	1	
	<i>///</i>		1	I		1	
1	Y///		1	1	•		
1 1	Y///		1	ł			
1 }	Y//A		1			1	
14.4	$Y//\lambda$		U/CLLR	Clay: As abo	ve soft/firm with abundant carbonaceous	1	
1)	V///		1	lamina, fine	roots, dark brown, minor leached pebble	1	
1	<u>///</u>		I	zone 14.8 ft	• •	1	
15.2	· · · · ·		U/SDSM	Sand: Buff.	Moist to wet, very fine grained, silty,	Water in hole - 15	
i]		1	poor - moder	ate sorting.	- 16 ft. Sharp	
1	<u> </u>		1	1		contact.	
16	<u> </u>		U/CLLR	Clay: As abo	ve, dark brown, carbonaceous stains, soft	1	
l	Y///		1	to firm, moi	st, calcareous pebbles, minor oxidation	1	
}	Y///		1	stains.		1	
16.5	{· · · · · · · ·		U/SDLR	Sand: As abo	ve, silty, color lamina (oxidation layers),	Few pebbles.	
l	P.O.O.		1	fine roots,	gravel - 17,6 - 18 ft.; buff; sand is	1	
I	10.0.d		İ		th > 95% quartz, minor cohesive clay	1	
1	D.0.0.1		1	lenses, othe	rwise loose, minor carbonaceous streaking;	İ	
1	10.0.4		1		and intermitent pebbles decrease to 20 ft.		
20	h.n.n.		U/SDGR	Sand: As abo	ve, buff yellow, and gravel to 22 ft., sand	Not likely fill	
				·	<u> </u>	·	

1.6-								
DRILLING LOG RADIAN CORPORATION 1. PROJECT: CARSWELL AFB,					INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 2 SHEETS			
1. PRO		•			7. TOTAL DEPTH OF HOLE: 27.5 ft BGL			
1		PHASE II			8. DATUM FOR ELEVATION SHOWN: sea level			
		lightline /		_	9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill 8-61		
			ronmental Dri		10. NO. OF SAMPLES TAKEN: 13			
	LE NO.: L		B 81		11. ELEVATION GROUND WATER:			
		OGIST: S.	8. Blount		12. DATE HOLE ESTABLISHED: 3/22/90			
•	ORDINATES 2010/88		399182.10	•	13. SURFACE ELEVATION: 620.60 ft MSL			
1 ^:-	2017400.	<u>04 1;</u>	399 102.10		14. BACKGROUND:			
Depth	Graphic	Blow	 Soil	ı	1 13. HEASON ING POINT ELEVATION.			
(Ft.)			Class/Code	ı İVisual Descr	intion	Remarks		
	7 9 9				ty sorted; gravel approximately 20%, 2 - 15			
i Ł	.0.0.0		•	•	ith clay content increasing to bottom.	above. Vague		
i F	5.0.0		İ	, İ	•	'contacts'.		
22	1///		U/CLLR	Clay, silt a	nd gravel: Light to medium grey to 22.3	i i		
1 1	///		l	ft., changin	g to buff/orange. Clay is stiff, wet and	j j		
1 1			1	brittle. Gra	vel appears concentrated in horizontal	İ		
1	///		l	planes. Abru	pt color change to dark grey at 24 ft. Clay	İ		
1 (l	at 24 ft. is	silty with minor calcareous pebbles, firm,	1		
1 (///		1	semi-plastic		1		
1 {	///		{	1		1		
1 [1	1		! !		
26.5	00		U/GRVL	Gravel: Clay	rey, silty, sandy, loose, wet, medium grey,	Auger refusal at		
	000		1	80% of sampl	e calcareous gravel 5 - 50 mm, average size	27.4 ft.; went in		
1 }	000		1	20 mm.		with SS. No		
[ممم		1	1		Recovery.		
27.4		50	U/MARL	Mart: See de	scription from LF05-04 (no sample	T.D. at 27.5 ft.;		
1 1			!	recovery).		WL approximately 24		
!!!			!	!		ft. (grouted		
!!!			!	!		before E - line).		
!!!			}			1		
!!!	l			!				
			1			!		
1 1			1	1		<u> </u>		
			1	1		[1:		
1 1	İ	 	1	1		1		
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	LING LOG		CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
1. PI	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 28.3 ft BGL	
l	IRP	PHASE II S	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
2. L	OCATION: F	lightline /	\rea		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DI	RILLING AGE	NCY: Envi	ronmental Dri	ilers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
4. H	DLE NO .: L	F05-04			11. ELEVATION GROUND WATER:	
5. N	AME OF GEOL	OGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90	
6. C	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 617.30 ft MSL	
<u> </u>	2019719.	98 Y:	399313.92		14. BACKGROUND:	
					15. MEASURING POINT ELEVATION:	<u> </u>
Depth	Graphic	Blow	Soil	I		1
(Ft.)	Log	Count	Class/Code	Visual Descri	iption	Remarks
0	Y//1		U/CLLR	Clay: Sandy,	brown with calcareous pebbles, damp, fine,	1
1	V//1			semi - britt	le, rootlets.	İ
1	V///		U/SDLR	Sand: Brown/g	green, clayey, with gravel up to 15 mm,	İ
1	$V//\lambda$				sorted, moist, quartzose with calcareous	i
	V//x			pebbles.		İ
1.5	V//i		U/CLLR	Clay: As abov	ve, calcareous pebbles increased to 25%,	Probably fill. 3.5
l	V//i				with oxidation blebs and black	ft. Recovery.
1	///i			•	staining within lenses, less sandy.	
	[///i			i	-,,-	i
	[///i			i		i İ
5	ĭ · · · · j		U/SDLR	Sand: Brown.	loose, dry to damp, very fine grained,	Probably fill. 3.5
İ			i		yey, poor - moderately sorted, quartzose	ft. Recovery.
İ					ous pebbles, oxidation lenses and asphaltic	I
	 .		•	pebbles.	person or restruction tenses and aspirately]
7	777			••	brown orange, firm, semi-plastic with]
, · 	///				ebbles to 8 ft.]]
8	500			Sand: As above	! !	
,	1		0/30EK	laur. Ye acc.		!
İ	$\circ \circ \circ$!]
9.5	} 		U/CLLR	I Clay: As abov	VA	! !
10	0.0.0		·		brown, clayey, silty, very fine grained,	 Fill. Concrete
i			•			
					d, oxidation stained, quartzose with > 95%	block in sample ~ 2
] 	0.0.0			•	ounded, with 5% carbonaceous flecks and	in. across. Sarp
! 	1.0.0.d				e (40 mm) gravel chunks, moist to 12 ft.,	contract. 3 ft.
] 	0.0.0]]	we l at 13 ft. 	., minor carbonaceous streaking.	Recovery.
13	 7 7 /			 class=podd	allan one atlant the state of	
ו כו ן	V / / X			•	ellow, wet, silty, oxidized, soft to firm,	Bottom of fill -
] 	V//X				iche at top, minor pebbles (calcareous) to	sharp. Water in
 14	V / / \			14 ft. 15	Attention of the state of the s	hole.
14	V//\				tiff, green/grey, abundant calcareous	<u>!</u>
	///			•	-brittle, wet carbonaceous stained.	!
14.8					roum/black, very brittle, organic rich,	Sharp contract.
					rootlets, gradual color change to	Musky odor.
	<i>[///</i>]				ith an increase in carbonaceous debris and	
!	r///			plasticity; \	very stiff; similar to clay at 14 ft.	
	Y///			ļ.		
18	Y///		U/CLLR	Clay: As abov	ve with an increase in gravel and sand to	Calcareous zones
!	Y///				and gravel). Green/grey, stiff, brittle,	'calichified'.
!	Y///				ebbles concentrated in 0.5 ft. intervals to	1
	V//X			23 ft.; sand)	y in these intervals (CaCO3 sand?).	
l	V//X			I		
1	V//X			I		İ
	V//\			I		Ì
				I		İ
	1///	,				•

DRILLING LOG			
RP PHASE II STAGE 2 8. DATUM FOR ELEVATION SHOWN: see level			
2. LOCATION: Flightline Area 9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61 3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO. OF SAMPLES TAKEN: 14 4. HOLE NO.: LF05-04 11. ELEVATION GROUND WATER: 5. NAME OF GEOLOGIST: S. B. Blount 12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 617.30 ft MSL X: 2019719.98 Y: 399313.92 14. BACKGROUND: Depth Graphic Blow Soil (Ft.) Log Count Class/Code Visual Description Remarks Count Class/Code Visual Description Remarks 23 O.O.			
3. DRILLING AGENCY: Environmental Drillers, Inc. 10. NO. OF SAMPLES TAKEN: 14 4. HOLE NO.: LF05-04 11. ELEVATION GROUND WATER: 5. NAME OF GEOLOGIST: S. B. Blount 12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 617.30 ft MSL X: 2019719.98			
11. ELEVATION GROUND WATER: 5. NAME OF GEOLOGIST: S. B. Blount 12. DATE HOLE ESTABLISHED: 3/22/90 6. COORDINATES OF HOLE: 13. SURFACE ELEVATION: 617.30 ft MSL X: 2019719.98 Y: 399313.92 14. BACKGROUND:			
12. DATE HOLE ESTABLISHED: 3/22/90			
13. SURFACE ELEVATION: 617.30 ft MSL 14. BACKGROUND: 15. MEASURING POINT ELEVATION: 15. MEASURING POINT ELEVATION: 15. MEASURING POINT ELEVATION: 16. MEA			
14. BACKGROUND: 15. MEASURING POINT ELEVATION: 15. MEASURING POINT ELEVATION: 15. MEASURING POINT ELEVATION: 16. MEASURING			
Depth Graphic Blow Soil]		
Depth Graphic Blow Soil			
Count Class/Code Visual Description Remarks			
U/SDGR Sand and Gravel: Sand is very fine to coarse grained, Very sharp saturated, very poorly sorted, buff/tan, sub-rounded, contract. quartz and CaCO3, (60% quartz) and < 5% heavy minerals, minor oxidation staining, 'gravel' average size 5 mm, but up to 35 mm, quartz and CaCO3, approximately 40% of	1		
saturated, very poorly sorted, buff/tan, sub-rounded, contract. quartz and CaCO3, (60% quartz) and < 5% heavy minerals, minor oxidation staining, 'gravel' average size 5 mm, but up to 35 mm, quartz and CaCO3, approximately 40% of			
U/MARL Hart: Fissile, calcareous, hard, wet, chalky, w/ shell 1 ft. Recovery fragments; (description from bit sample and portion of 1 ss sreduced. Hent 1 st. Recovery 1 ss recovery). Ss refusal. Hent 1 st. Recovery 1 st. Recover			

		1			1	AF 2 411274
	ING LOG		CORPORATION	_	INSTALLATION: CARSWELL AFB, TX SHEET 1	UP 2 SHEETS
ı. Pi	ROJECT: CAR			•	7. TOTAL DEPTH OF HOLE: 26.2 ft BGL	
		PHASE II			8. DATUM FOR ELEVATION SHOWN: sea level	W-11 & 11 & 11
	OCATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
			<u>ronmental Dri</u>	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
	DLE NO.: L				11. ELEVATION GROUND WATER:	
			B. Blount	_	12. DATE HOLE ESTABLISHED: 3/22/90	
	CORDINATES	-			13. SURFACE ELEVATION: 616.10 ft MSL	
X:	<u>2019785.</u>	85 Y:	399388.49		14. BACKGROUND:	
				_	15. MEASURING POINT ELEVATION:	
Depth (Ft.)	Graphic Log	Blow	Soil Class/Code	 Visual Descr	intian	 Remarks
0		COUNT	U/SDCL		y: Orange/red, very fine grained, damp,	Full sample unless
Ū			1	•		•
			t 1		, gravel, roots, calcareous fragments, very	
	• • • •		\ !	poorty sorte	d sand, cohesive (clay).	indicated. 1 ft.
			1	1		Recovery. Fill sand
_	!			!		top 2 ft.
2			U/CLLR		with minor orange mottling, firm, semi -	Fill clay.
			ļ.	plastic with	abundant calcareous pebbles (up to 20 mm),	1
	[///			damp to mois	t, minor black (carbonaceous?) streaking.	I
4	r///		U/CLLR	Clay: As abo	ve - light brown, mottling increased.	Fill clay?
	Y///		1	Asphalt? mix	ed with sample.	1
	Y///		i	1		1
	$Y//\lambda$		1	1		1
6	$Y//\lambda$		U/CLLR	Clay: As abo	ve.	1
	$V//\lambda$		1	ĺ		Ì
	V//X		İ	Ī		İ
			i	i		i
8			U/CLLR	Clav: As abo	ve, few large (50 mm) gravel chunks.	i
			1	1	ve, real targe (so many grover entance	!
	<i>Y///</i>		i	i i		!
 	Y///		1	1		1 1
9.9	1221		U/ASPH	 Acobalt: Sol	id "asphalt" - tar and pea gravel with some	 Eill Could not
,.,			i O/ASFII	brown clay.	id aspiratt - tal and pea gravet with some	push at 10 ft.;
			1	DIOWICTAY.		!'
 			1	1		material very hard.
12		11 17 17	1 11/01/5	 Class Dank	manufactory doubt annu matted 4:	I images
1 2	///	11,13,17	U/CLLR		rey/very dark grey mottled, firm,	Limestone
	V//		1	•	with abundant calcareous pebbles (1 to 15	lithoclast?
			!	•	ments, damp to moist with indurated sandy	
	[///		1		r - light orange/buff at base.	!
14	! ///		U/CLLR	•	12 ft. Few very large cobbles (80 mm);	
	<i>[///</i>		ļ.	silty 14.4 -	14.8 ft.; color lightening.	!
	Y///		1	<u>l</u>		!
	Y//A		ļ	ļ	•	ļ.
16	$Y//\lambda$		U/CLLR	Clay: As abo	ve, color change at 16.4 ft. to	
	$V//\lambda$	}	1	buff/tan/yel	low; continued large cobbles to 18.5 ft.,	
	$V//\lambda$		1	calcareous d	lebris abundant at 17.2 - 17.6 ft. then ends	1
	$V//\lambda$		1	abruptly.		
18	$V//\lambda$		U/CLLR	Clay: Soft t	o slightly firm, buff/yellow, 20% small	
			1	calcareous f	ragments and sand and silt, moist to wet,	1
			İ		, few 15 mm pebbles.	İ
İ	K///		i	1	•	i
20	<u>~~~~</u>	ĺ	U/SOLR	 Sand_Grave	and Clay: As above, sand or gravel up to	 Samples
i			1	:	et at top. Firm, plastic at base;	preferentially wet
			1		e due to inclusions; calcareous fragments	(soggy) on top;
	$\mathcal{L}^{\bullet}(U)$!	I	Jacks - NI LEFFE	we to inclusions, calcaleous insyncits	1/2022/ 01/10/
		l	1	lincreses to	base, clayey sandy gravel to base (clayey	probably a function

DRILLING LOG	RADIAN C	ORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	OF 2 SHEETS	
1. PROJECT: CARS	SWELL AFB,	-		7. TOTAL DEPTH OF HOLE: 26.2 ft BGL		
	PHASE II S	TAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: FI				9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61		
3. DRILLING AGE			llers, Inc.	10. NO. OF SAMPLES TAKEN: 14		
4. HOLE NO.: LI		_	-	11. ELEVATION GROUND WATER:		
5. NAME OF GEOLG		B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90		
6. COORDINATES (13. SURFACE ELEVATION: 616.10 ft MSL		
X: 2019785.8		399388.49	•	14. BACKGROUND:		
			•	15. MEASURING POINT ELEVATION:		
Depth Graphic	Blow	Soil	1		1	
[(Ft.)] Log	Count	Class/Code	Visual Descr	iption	Remarks	
1 1.0.0.0			gravely sand	•	of the sampler.	
0.0.0	i	i			Clay, sand, and	
1 1 1	ľ	Ì	İ		gravet equat	
1.0.0.9	ľ	i	i		proportions.	
p.o.o.	i		i		Ï	
10.0.4]			i	
0.0.0	į t		1		i	
1.0.0.4	i	1 	i			
24.9		I U/GRCL	 Gravel: Clay	vev gravel.	; 	
25.3		•	•	ound gravelly sand; sand composed of shell	1	
		l U/SUSA I	•	fragments, coarse grained, wet, poorly	1	
		 	sorted.	inagments, coarse granned, wet, poorty	1	
1 1 1 1	50 l	 	•	milau fiamila shalta slavav shala	 	
26 1 - 1 - 1	ן טכ	U/MARL	•	rellow, fissile, shells, clayey shale	Refusal at 26 ft.,	
		ļ	appearance,	semi-indurated, chalky.	Drive SS. T.D. at	
!!!!!!		! :	!		26.2 ft.	
!!!!!!		ļ	!		!	
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RILL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 1 SHEETS		
. PRO	DJECT: CARS	WELL AFB,			7. TOTAL DEPTH OF HOLE: 7.7 ft BGL			
	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level			
. LO	CATION: FI	ightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	<u> Mobile Drill B-61</u>		
. DR	ILLING AGE	ICY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 5			
. HO	LE NO.: LI	05-06			11. ELEVATION GROUND WATER:			
. NA	ME OF GEOLG	GIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90			
. co	ORDINATES (OF HOLE:			13. SURFACE ELEVATION: 598.30 ft MSL			
X:	2020129.	8 Y:	399156.86		14. BACKGROUND:			
					15. MEASURING POINT ELEVATION:			
pth	Graphic	Blow	Soil	1				
t.)	Log	Count	Class/Code	Visual Descr	<u>iption</u>	Remarks		
ı t	10.0.d		U/SDGR	Sand, Gravei	, and Clay: Buff/yellow, very poorly	Full recovery		
į			1	sorted; sand	is very fine to very coarse grained,	unless otherwise		
Í	.0.0.4		1	quartzose wi	th calcareous pebbles/fragments, moist to 3	noted.		
ĺ	0.0.0		1	ft., wet bel	ow; clay content increases below 3 ft			
Ì	0.0.0		1	Gravel (20%)	up to 20 mm, size increases at base. Unit			
ŀ			1	is brittle.		1		
ŀ	0.0.0		1	1		1		
}	0.000		1	1		1		
, }	0.0.0		U/SDGR	1		1.5 ft. Recovery,		
Ì	$\cdot \circ \cdot \circ \cdot $		i	į		ST refusal at 5.5		
Ì	0.0.0		i	i		ft., go in with		
j	0.0.0		İ	i		auger to 5 ft.		
ì	0.0.0		i	i		samples.		
.a [U/GRSM	Gravel: Aver	age 70 mm, minor fine sand and clay,	1		
	000		1	:	ell sorted, subrounded, composed of	i		
ì	0 0 q		i	limestone li	• • •	i		
5.5 T	777		U/CLAY	•	to very stiff, buff/yellow, with grey	i		
ľ			1	•	ittle, moist; oxidation staining	1		
ł			i		fissile in zones.	1		
, 8		50	U/MARL	•		Refusal at 7.5 ft.		
ï			1	- I	leached 'caliche' type zone at base (0.1	(limestone), drove		
i	, I		i	ft.).		ISS at 7.5 ft Les		
, 1	¦		i	1		than 3 in. with 50		
i I			1	1		blows. T.D. at 7.7		
1	·		1	i l		ft WL = 3.38 ft.		
1			1	1		BGL.		
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DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 1 SHEETS		
1. P	ROJECT: CAI	RSWELL AFB,			7. TOTAL DEPTH OF HOLE: 7.2 ft BGL		
<u> </u>		PHASE II			8. DATUM FOR ELEVATION SHOWN: see level		
T -	OCATION: I			_	9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 6		
	OLE NO.: L				1 11. ELEVATION GROUND WATER:		
			B. Blount		1 12. DATE HOLE ESTABLISHED: 3/22/90		
0. C	OORDINATES	.22 Y:	399192.73	•	13. SURFACE ELEVATION: 598.00 ft MSL 14. BACKGROUND:		
1 ^-	2020230	<u> </u>	377 172.73		15. MEASURING POINT ELEVATION:		
Denth	Graphic	Blow	Soil	1	13. HEASURING POINT ELEVATION.	1	
(Ft.)		Count	Class/Code	 Visual Descr	intion	Remarks	
0	77/		U/CLLR	+	grey, moist, soft, plastic, roots, sandy,		
1			1		ed sand to 0.8 ft. becoming clayey sand.	1	
į 1	10.00	ĺ	U/GRSM	•	ey, light brown/grey, calcareous gravel up	Sharp contact. 2	
i	0.0.0		i	•	stly 2 - 3 mm), moist, very poorly sorted.	•	
1.4			U/SDGR	•	vel: Very fine grained, poorly sorted,	Sharp contact.	
İ	h.n.n	ĺ	İ	clayey, oran	ge, dry to damp, with moisture increasing	Assume some gravet	
İ		İ	İ	to base. Cla	y content variable, clayey and cohesive in	•	
İ			1	lenses; grav	el - 20%, 3 - 25 mm, very poorly sorted.	sample.	
3.8	h.n.n]	U/GRSM	Gravel: Quar	tz and calcareous pebbles with minor sand,	Sharp contacts.	
1	M.O.	1	1	wet, very po	orly sorted; 98% gravel, average 10 mm up	1	
1	6.0.0		1	to 20 mm.		1	
5	1777]	U/CLAY	Clay: Stiff	to very stiff, buff/yellow with gray	3 ft. Recovery.	
			 	mottling, ox moist.	idation seams, semi-fissile, brittle,	Refusal at 5.8 ft	
5.8		50	U/MARL	Mart: Dark g	ray, semi-indurated, very fissile, highly	Drilled into mark	
1	Ī	Ì	į	calcareous,	alternating with stiff 'clay', minor	1.4 ft. to good	
1	1	l	İ	oxidation mo	ttling.	auger refusal. T.D.	
1	1	1		1		= 7.2 ft No WL	
1	}	I	1	1		hole caved to 3.5	
1						ft.	
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L DRILL	LING LOG	PADIAN	CORPORATION		I INCTALLATION - CARCUELL AFR TY CHEFT 1	OF 1 SHEETS	
					7. TOTAL DEPTH OF HOLE: 18.3 ft BGL		
 	IRP PHASE II STAGE 2			•	8. DATUM FOR ELEVATION SHOWN: sea level		
1 2. LI	2. LOCATION: Flightline Area 3. DRILLING AGENCY: Environmental Drillers, Inc.				9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill 8-61		
:				llers Inc.	10. NO. OF SAMPLES TAKEN: 9	MODILE BITTE B	
	OLE NO.: L		TOTAL DIT	1101	11. ELEVATION GROUND WATER:		
			B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90		
	OORDINATES		o. broan	<u></u>	13. SURFACE ELEVATION: 606.80 ft MSL		
:			399030.31	•	14. BACKGROUND:		
1	202,000	<u> </u>	377030131		15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1		1	
	Log		Class/Code	 Visual Descr	iption	Remarks	
1 0	1///		U/CLAY		soft, damp, brittle, root bound with fine	1	
i	Y///		i		nor other plant debris.	i '	
i	Y///		i	1		i	
i	Y//A		i	i		i	
2	Y///		U/CLAY		brown, firm, plastic, moist, minor	i	
i	$Y//\lambda$		1	•	w calcareous flecks at base.	i I	
ì	$Y//\lambda$		i	1		1	
i	$V//\lambda$		i	i		1	
1 4	$V//\lambda$		U/CLAY	 Clay: Grev/d	rey, mottled, very stiff, dry to damp, very	 Could not cut w/	
i	V//		1	•	ootlets, abundant calcareous debris.	carpet knife.	
i	///		i	1	,	1	
i	///		1	ì		! 	
i			1	i		1	
ì			1			1	
i			1	1) }	
1	(///		i t			1	
8	Y///		 U/CLLR	IClave As abo	ve, calcareous pebbles up to 15 mm; stiff.	Pabbles affervasce	
1	Y///		1		y debris 1 - 2 mm.	in HCl solution.	
i	Y///		1	l coommercer	y Octor is 1 · 2 non.	in her solution.	
1	Y///		1	1		1	
1 10	Y//A		U/CLLR	 Clay: As abo	ove, firm, plastic.	1	
1	Y//A		1	l	ve, trim, prestre.	1	
1 11	Y///		U/CLLR	llav Sand	and Gravel: Very poorly sorted, rounded	 Musky odor.	
¦ ''	Y//A		1	•	et. Clay dominates to 12 ft. with small soil	•	
1			1	_	top, buff/yellow. Sand content increases	(Soil).	
i	$V//\lambda$		}	to base.	top, builty ections during content incidence	1	
1 12	 		I U/SAND	•	rellow, very fine to fine grained, slightly	 Water in hole at	
1			0/3580		rive at top, loose below 12.3 ft., moderate	12 ft.; go to 5 ft.	
	• • • •				ell sorted, > 95% quartz.	samplers.	
1 14.5			U/LMSN	•	rey to light grey, marly, fissile,	Drilled slowly	
			5/2/15/4	:	0 mm indurated layers with thin marks	linto limestone.	
1			i	•	shells, micritic appearance.	Refusal at 14.5 ft.	
1	1		1	Jacketti, 10	onecco, miericie appedianes.	0.5 ft. Recovery.	
1			1	1		Driller says	
i I			1	1		layered mart, drive	
1	1-1-1-		1	1			
1 17.5		50	U/LMSN	limesteres !	lali indunated colourance chair - ficails	SS; 1 ft. Recovery. T.D. at 18.3 ft	
17.J		}) Of Chian	•	Pell indurated, calcareous shale - fissile, . slightly 'carbonaceous'; contiguous 'bed'		
1	? 	; {	1	from 17.5 -		ft. (BGL).	
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DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 1 SHEETS		
1. PI	ROJECT: CAR	RSWELL AFB,			7. TOTAL DEPTH OF HOLE: 14.5 ft BGL		
İ	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level		
2. L	OCATION: F	lightline /	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DI	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 6		
4. H	OLE NO.: L	.F05-09			11. ELEVATION GROUND WATER:		
5. N	AME OF GEOL	OGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90		
6. C	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 604.90 ft MSL		
X:	2020361.	.60 Y:	<u> 398918.32</u>		14. BACKGROUND:		
L	_				15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1		!	
(Ft.)	Log	Count	Class/Code	Visual Descr	iption	Remarks	
0			U/CLLR	Clay: Orange	/brown mottled, very sandy, silty with some	Full recovery	
			1	gravel, brit	tle, dry to damp, fine rootlets to 3.5 ft.,	unless otherwise	
			1	few calcareo	us flecks, alternating zones: brown then	indicated.	
			1	orange appro	ximately 0.5 ft. thick.		
			1	I		1	
	Y///		1	1		1	
	Y///		1	1		1	
3.5			U/SDSM	Sand: Buff/y	rellow with orange color laminations,	Sharp contact.	
1	1.	Ì		slightly cla	yey at top, loose below, rounded quartzose		
ĺ			ĺ	grains; clay	lenses 5 - 5.3 ft., 5.7 -5.9 ft.; damp to	1	
ĺ	· · · · ·		İ	moist, > 95%	quartz, well sorted, cohesive in clayey	Ì	
Ì	1		i	intervals, t	oosely consolidated otherwise.	į	
ĺ			İ	i		i	
i	$\left\{ \cdot \cdot \cdot \cdot \cdot \right\}$	Ì	İ	i		İ	
i			i	i			
i		i	i	i		i	
I 8	}	ì	U/SDSM	Sand: As abo	eve, thinly laminated orange color laminae	i	
i	1	}	1	•	ed, slightly clayey at base.	i	
i	1	ì	i	1		1	
i I	}	}	Ì	! 		1	
1 10		}	U/SDSH	 Sand: As abo	ove, moist to wet, clayey at top. Shell	 Water in hole ~ 11	
	\		1	•	rer 10.6 - 11.4 ft Clayey and silty below.		
! 		}	1	I agricult tay	ter 10.0 11.4 1tt. Ctayey and Sitty Deton.	1	
1		ł 1	1	1		1	
1 12		j I	U/SDLR	 Sanda Onessa	, very minor gravel, wet loose, few	3 - 6 pieces of 10	
1 12	0.0.0		i U/SULK	carbonaceous	•	- 20 mm gravel.	
1	2.0.0.1	ŧ .	1	carbonaceous	S Streaks.	1 20 HER GIEVEL.	
1	0.0.0	}	1	1		1	
		150		1			
14		50	U/MARL	-	ited, dark grey/green shale, very	Refusal at 14 ft.;	
!	!	1	!	-	some orange oxidation, fissile, few shell	drove SS, bottomed	
!	1	i	1	iragments, a	minor carbonaceous debris, dry to damp.	less than 0.5 ft	
!	Į.	Į.		ļ	•	T.D. at 14.5 ft.	
!		!	!	!]	
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DRILL	LING LOG	I PADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS	
	ROJECT: CAR				7. TOTAL DEPTH OF HOLE: 36.2 ft BGL	0. 2 0.122.10	
1		PHASE II		•	8. DATUM FOR ELEVATION SHOWN: sea level		
1 2. 10	2. LOCATION: Flightline Area				9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61		
				illers. Inc.	10. NO. OF SAMPLES TAKEN: 13		
				1110.01	11. ELEVATION GROUND WATER:		
	AME OF GEOL	_	R Rigunt		1 12. DATE HOLE ESTABLISHED: 3/22/90		
	OORDINATES		B. Brown	_	13. SURFACE ELEVATION: 623.90 ft MSL		
) X:			398656.87	•	14. BACKGROUND:		
1	2017430.		370030107		1 15. MEASURING POINT ELEVATION:		
Inenth	Graphic	Blow	Soil		131 hendanina / dini eccinitani	1	
•	Log		Class/Code	 Visual Descr	intion	Remarks	
10	V 777 1	000.11	U/CLLR		dark brown with minor carbonaceous	Full recovery	
i		•	1		irm, plastic, moist. Calcareous pebbles	unless otherwise	
1		 	1		0.4 ft., minor roots, few pebbles to 3 ft.	noted.	
3.2			U/CLLR	streaking, m hard, sand t rootlets and ft. Clay: Calich firm, shell	tiff, dark brown with obvious carbonaceous ninor sandy lenses, damp to moist, brittle, amination at upper contact is parting; fine i intervals with coarse sand/pebbles to 6 diffed (leached) white to buff, brittle, fragments, damp, abundant calcareous	seems too dense to	
 7.5 					as above, interlayered with calichified 2 ft.; stiff clay has intervals of abundant debris and grades into caliche then abruptly clay as 6 - 7 ft.		
 13.2		 	 U/CLLR 	•	n brown/yellow, moist to wet, brittle, dant calcareous debris.	! 	
14.5			U/MARL	Mari: Weathersoft, oxidiz	ered limestone mark at 14.5 ft.; clay rich, ted in seams, abundant broken micritic ragments, wet (saturated - soggy), c., buff/yellow.	Water in hole 14.5 - 19.5 ft 3.5 ft. recovery.	
16] 	U/CLLR 	Clay and Gra stiff, moist with coarse	 		
18 			U/MARL	•	grey, semi-indurated, highly calcareous, sile, dense, dry to damp.	1	
19.5 			U/GRSM 	orange/yello Sand very po subangular,	d, and Clay: Gravel up to 80%, bu, brittle/friable, soft, wet to moist. borly sorted, very fine to coarse grained, wet, gravel up to 40 mm, quartz and CaCO3 mell fragments, slightly cohesive.	4.2 ft. Recovery. 	

DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS	
1. PROJECT: CARS				7. TOTAL DEPTH OF HOLE: 36.2 ft BGL		
	PHASE II			8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: FL				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DRILLING AGEN			llers, Inc.	10. NO. OF SAMPLES TAKEN: 13		
4. HOLE NO.: LE				11. ELEVATION GROUND WATER:		
5. NAME OF GEOLG	GIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/22/90		
6. COORDINATES C	OF HOLE:			13. SURFACE ELEVATION: 623.90 ft MSL		
X: 2019456.1		398656.87		14. BACKGROUND:		
		_		1 15. MEASURING POINT ELEVATION:		
epth Graphic	Blow	Soil	1		1	
Ft.) Log	Count	Class/Code	Visual Descr	iption	Remarks	
0.0.0.0 0.0.0.0 0.0.0.0 0.0.0.0		 	oxidation st	, clayey (slightly), wet, soft, minor aining in laminae, very uniform lithology nterval, saturated.	 Very sharp contact.	
28.5		U/SDLR	saturated, > subrounded g oxidation po	Pyellow, very fine grained, loose, 95% quartz, moderately well sorted, prains, no sedimentary structures, minor eds, very minor carbonaceous flecks; with 50 - 100 mm gravel fragments)	 Very sharp contact. 	
33.2 · O · O · O · O · O · O · O · O · O ·		U/GRSM	wet, slightl	etz and calcareous fragments, poorly sorted, y sandy, slightly silty, loose, average 2 - ungular fragments up to 75 mm; buff/orange.	34.5 - 36 ft. = NR Auger refusal at 36 ft.; drive SS. Grout SS	
36	50	U/MARL	•	cone fragment - well indurated, micrite. ecrystallized fossils, chaulky exterior.	refusal. T.D. at 36.2 ft Poor recovery SS, description from one fragment. WL: 26.2 ft.	

				1 10 - 12
DRILLING LOG RADIA	AN CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	1 OF 1 SHEETS
1. PROJECT: CARSWELL AT			7. TOTAL DEPTH OF HOLE: 10.1 ft BGL	
	II STAGE 2	•	8. DATUM FOR ELEVATION SHOWN: see level	
2. LOCATION: Flightlin			9. MANUFACTURER'S DESIGNATION OF DRILL:	
3. DRILLING AGENCY: E		illers, Inc.	10. NO. OF SAMPLES TAKEN: 6	
4. HOLE NO.: LF05-11	<u>-</u>		11. ELEVATION GROUND WATER:	
5. NAME OF GEOLOGIST:	S. E. Fain	· · · · · ·	12. DATE HOLE ESTABLISHED: 3/19/90	<u> </u>
6. COORDINATES OF HOLE	_	-	13. SURFACE ELEVATION: 597.60 ft MSL	
X: 2020446.51 Y		•	14. BACKGROUND:	
			15. MEASURING POINT ELEVATION:	_
Depth Graphic Blo	w Soil	1		1
(Ft.) Log Coun	•	Visual Descr	iption	Remarks
0 ///	U/CLAY		orown, damp, calcareous nodules, roots.	Full recovery
				unless otherwise
2	U/CLLR	 Clay: As abo	we, slightly silty and sandy.	
4	 U/CLLR	 - Clay: Dark b	огомп, hit root at 5.5 ft., wet.	
		 	various vary fire arrived good	
6	U/CLLR 		orange, very fine grained sand.	W.L. measured at
7	U/SDLR 	quartzose; a	e/tan, fine to medium grained, wet, it 8 ft., brown, musky odor. 8.5 - 10 ft.	
	ļ		gravel to 20% at bottom of sampler.	ļ
	ļ	Saturated, s	inells.	!
		1		1
10	 U/MARL 	 Mart: Green/ 	gray, indurated, fissile, exogyra fossils	10 ft. Drove S.S. (1 1/2 ft.); 50 blows = 0.1 ft.;
				T.D. = 10.1 ft.
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DRILLING LOG RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 1 SHEETS			
1. PROJECT: CARSWELL AFB,			7. TOTAL DEPTH OF HOLE: 9.2 ft BGL			
IRP PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level			
2. LOCATION: Flightline	Агеа		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill 8-61		
3. DRILLING AGENCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 6			
4. HOLE NO.: LF05-12			11. ELEVATION GROUND WATER:			
5. NAME OF GEOLOGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/19/90			
6. COORDINATES OF HOLE:			13. SURFACE ELEVATION: 594.40 ft MSL			
X: 2020606.71 Y:	398699.09		14. BACKGROUND:			
1			15. MEASURING POINT ELEVATION:	<u> </u>		
Depth Graphic Blow	Soil			1		
[(Ft.) Log Count	Class/Code	Visual Descr	iption	Remarks		
10 1//1	U/CLLR	Clay, Sand,	Gravel: Clay is light brown/orange, moist,	Full sample unless		
1 ////	t	semi-plastic	, soft with abundant oxidation. Gravel is	otherwise		
i ///	1	10 - 20 mm c	alcareous pebbles.	indicated.		
1.5	U/SDSM	Sand: Orange	, moist, clayey 2 - 2.5 ft., silty, very	Gradational		
	İ	fine grained	, poorly sorted.	contact.		
2.5 ///	U/CLLR	Sandy Clay:	Clay as above, without gravel (calcareous	Water in hole at 5		
1 1///	1	debris minor), sandy and silty to 4 ft.; silty to 6.8	ft.		
1 Y///	1	ft.; clay is	grey/brown, moist, soft; very soft and wet	1		
$\Gamma Y//A$	1	at 5 ft., mi	nor oxidized sand seams, few very fine	}		
	Ī	rootlets, se	mi-plastic.	1		
i <i>Y//</i> /	i	i				
i <i>Y//</i> /	Ì	Ì		Ì		
i ///	i	ì		ĺ		
i <i>V//</i> /	i	i		İ		
6.8	U/CLAY	Clav: Dark o	rey/black, soft, plastic, wet, highly	Sharp contact.		
	1	•	fine rootlets, silty (minor).	Musky odor. 1 ft.		
: [///]	<u> </u>	1	The located, sittly (million).	Recover ST. Mari at		
	;	¦		sample bottom.		
8.8	I U/SDVF	 Sand: Very	fine grained, moderately sorted, dark grey,	1		
0.0	1 0,321.	•	streaking, wet, quartzose.	¦		
50	U/MARL	•	grey, fissile, well indurated, micritic,	T.D. at 9.2 ft.;		
1 1 1	Official		chaulky zones.	WL = 2.73 ft.		
1 1 1	l I	i i	Hadiky Lores.	1		
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			CORPORATION_		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 1 SHEETS	
1. P	ROJECT: CAR	RSWELL AFB,		-	7. TOTAL DEPTH OF HOLE: 17.1 ft BGL		
<u> </u>		PHASE II			8. DATUM FOR ELEVATION SHOWN: sea level		
	OCATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
13. D	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 9		
<u> </u>	OLE NO.: L	. F05 - 13			11. ELEVATION GROUND WATER:		
5. N	AME OF GEOL	.OGIST: S.	E. Fain		1 12. DATE HOLE ESTABLISHED: 3/19/90		
6. C	OORDINATES	OF HOLE:			13. SURFACE ELEVATION: 605.00 ft MSL		
<u> X:</u>	2020738.	.54_ Y:	398406. <u>77</u>	_	14. BACKGROUND:		
<u> </u>					15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1		1	
(Ft.)	Log	Count	Class/Code	<u> Visual Descr</u>	<u>iption</u>	Remarks	
10			U/CLAY	Clay: Dark b	rown, damp, roots, plastic; calcareous zone	Full recoveries	
1			1	starts at 1.	8 ft.	unless noted.	
1	Y///		Ì	1		ĺ	
1	Y///		Ì	Ì		İ	
2	Y///		U/CLLR	Clay: Orange	/brown, very silty, abundant calcareous	1.6 ft. Recovery.	
i	V///		i	•	liche), dry, slightly cohesive.	i	
i	$V//\lambda$		i	i	· · · · · · · · · · · · · · · · · · ·	i	
i	V///		i	i			
14	$V//\lambda$		U/CLLR	Clav: As abo	ve, 20 - 30% calcareous material.	1	
1	V//		1	1		1	
1			1	1		1	
1			!	!			
1			1	101		14 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
6			U/CLLR	•	ve, moist; increased calcareous material,	11.4 ft. Recovery.	
ļ	Y///		!	18.7 - 9.3 ft	. Aalmost completely calcareous material.		
1	V///			1		}	
ł	V///	Į.	1	}			
1	V///	į	1	1			
1		ļ	1	1			
1]	1	1		1	
9.3		j	U/SAND	Sand: Orange	/tan, fine to medium grained, loose, damp,	Pushed S.S.	
1	1	1	1	subround, qu	artzose, minor oxidation staining.	sampler (1.5 ft.).	
1		!	1	1		Ì	
i	· · · · ·	Ì	Ì	İ		İ	
i		j	i	i		1	
12		i	U/SDLR	Sand: As abo	ve, calcareous zones (~ 0.5 ft.) at 13 ft.	Could not get W.L.	
i	h]	1	•	also gravelly in these zones. Material	down hole after	
i	Y_{α}	1	1	saturated at		augers pulled; 4.5	
-	1.0.0.0	{		Saturated at	- 13.5 11.	•	
1	b ·0·0		1	1		ft. Recovery.	
1	10.0.0	1	1				
	0.0.0	1	1 1140015	leans a s			
15	0.00	{	U/SDLR	Sand: As abo	ve.	!	
	\(\frac{1}{2} \cdot \frac{1}{2	1	1	1			
16	$b.\tilde{o}.\tilde{o}$	ļ	U/SDGR		vel: 50/50, very fine sand to pebble size	Sampler refusal at	
1	1.0.0.0	ļ	(gravel, satu	rated, numerous shells.	17 ft.	
17		 50	U/MARL	Marl: Gray/g	reen, fissile, indurated, iron stained in	Driving 1 1/2 ft.	
1	1	1	1	fractures, c	alcareous.	s.s. 1 1/4 in. for	
1	1		1	1		50 blows; T.D. =	
1	1	1	1	1		17.1 ft.	
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İ	i	ĺ	i	i		i	
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DRILL	ING LOG	PADIAN	CORPORATION		I INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 1 SHEETS	
1. PROJECT: CARSWELL AFB.					7. TOTAL DEPTH OF HOLE: 13.3 ft BGL	Of 1 SHEETS	
		•			8. DATUM FOR ELEVATION SHOWN: sea level		
2 10		PHASE II					
2. LOCATION: Flightline Area 3. DRILLING AGENCY: Environmental Drillers, Inc.						Mobile Drill B-61	
			rormental Dri	itters, inc.			
	4. HOLE NO.: LF05-14 5. NAME OF GEOLOGIST: S. B. Blount				11. ELEVATION GROUND WATER: 594.14 ft MS	L (0/10/9U)	
			B. Blount		12. DATE HOLE ESTABLISHED: 3/19/90		
	ORDINATES		200//7 57		13. SURFACE ELEVATION: 603.20 ft MSL		
<u> </u>	20 20 910.	08 Y:	398467.53		14. BACKGROUND:		
Denth I	Graphic	Blow	Soit	<u>-</u>	15. MEASURING POINT ELEVATION: 602.98 ft	MSL	
(Ft.)		Count	SOIC Class/Code	 Visual Descr	intion	 Remarks	
0	777	Count	U/CLLR		lark brown, soft, dry to damp,		
Ĭ	////		U/CLLX			Full recovery	
l	///		!		bly, fine rootlets and calcareous pebbles,	unless noted	
			!	aouncant cat	careous debris 1.5 - 2 ft.; silty, sandy.	otherwise. 3 ft.	
_ [1			Recovery.	
2			U/CLAY	debris, 'cru	tan, firm, dry to damp, abundant calcareous mbly' carbonaceous particles, stiffens to	! !	
				base.		<u></u>	
3.5	////		U/CLLR		ve, calichified to 4 ft., very stiff, dry,	3.5 ft. Very hard	
ł	////		1		to 4.7 ft., clay below is orange brown,	to cut.	
ł	////		1	very stiff,	damp with abundant calcareous debris and		
			 	carbonaceous	streaks/particles, brittle, sandy.	 	
7.2			 U/MARL 		grey, very stiff, silty clay with abundant fragments, oxidized in seams, brittle,	 	
Į			1	moist, 'slic	kensided'.	1	
8.5			U/SDFN	Sand: Fine g	rained, orange tan, oxidized, moderately	2.5 ft. Recovery.	
-)		1	sorted, subr	ounded, wet, loose, quartzose with > 95%		
ļ	<u>· · · · ·</u>)		1	quartz and <	5% heavy minerals.		
8.7	0.0.0		U/SDGR	Sand and Gra	vel: Sand as above with gravel at 8.7 ft.,	Water in hole at 9	
	0.0.0		 		edominately CaCO3 fragments, poorly sorted) average 3 mm, up to 30 mm. Approximately	ft. 	
Ţ	0.0.4		1	40% of sampl	e; subrounded.		
10.5			U/GRSM	Gravel and S	and: As above, only gravel 60 -70% of	Driller says	
ſ	<u>~~~</u>		1	sample, few	large > 70 mm fragments.	limestone at 13 ft.	
13		50	U/MARL	Mari: Very h	ard - no recovery.	Drove SS; 50 blows	
1	1		1	1		went 1 in.; no	
1			1	Ì		recovery; T.D. at	
i	İ		i	İ		13.3 ft.; WL - 9.43	
i	i		i.	i		ft.	
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DRIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 3 SHEETS	
1. P	ROJECT: CAR	RSWELL AFB,			7. TOTAL DEPTH OF HOLE: 40.6 ft BGL		
<u></u>	<u>I</u> RF	PHASE II	STAGE 2	<u> </u>	8. DATUM FOR ELEVATION SHOWN: sea level		
2. L	OCATION: F	lightline	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
			ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 26		
	OLE NO.: L				11. ELEVATION GROUND WATER:		
			B. Blount		12. DATE HOLE ESTABLISHED: 3/19/90		
6. C	OORDINATES	OF HOLE:			13. SURFACE ELEVATION: 626.50 ft MSL		
x:	2019457	.49 Y:	398082.81		14. BACKGROUND:		
Ĺ					15. MEASURING POINT ELEVATION:		
Depth	Graphic	Blow	Soil	1		1	
(Ft.)	Log	Count	Class/Code	Visual Descr	iption	Remarks	
0			U/CLLR	Clay: Dark b	rown, firm, moist, semi-plastic to 1.8 ft.;	Full recovery	
İ	V///		İ	•	ebbles aligned horizontal in "beds" to 1	unless otherwise	
i			i	•	s, organic, slightly silty 1 - 2 ft.	indicated.	
i			i	i	· · · · · · · · · · · · · · · · · · ·	İ	
2			U/CLLR	Clay: As abo	we, leached to buff color with oxidation	i	
i	ľ///	S	i	, ,	undant calcareous pebbles 1.8 - 2.1 ft.	i	
2.1	Y///		U/CLLR		st clay with peobles and semi-leached zone,	Alternating zones	
i	Y///	ſ			clay 3 - 3.2 ft., interval from 2.1 - 4.4	3 - 6 ft. each	
i	Y///	ſ	i	•	•	approximately 0.3	
i	Y///	{	i		undant calcareous debris and orange/brown,	ft. thick.	
i	Y///	{	i		pebbbles; thin sand 3.6 - 3.8 ft., very	i	
i	////	ł	i	fine gra	, , , , , , , , , , , , , , , , , , , ,	i	
6		<u> </u>	U/CLLR		ly sandy, silty, minor calcareous debris,	 Water in hole at 7	
1	V///	1		•	aturated (soggy), oxidation stained	ft. Perched?	
1	V///	1	i	•	minor carbonaceous streaking, few very fine		
<u> </u>	V//	1	i	rootlets, or		i I	
 8			I I U/CLLR	•	we, firm, dark brown clay with few pebbles	1	
0		}	O/CLLK	•	O ft.; no silt, very sandy at top.	1	
1			:	1	o it., no sitt, very samy at top.	1	
- [Y///]	1	1		1	
1 10	1///	}	I I U/CLLR	l Iclav: Ac abo	ove, very sandy at top with dark brown, firm	 Clavey sand?	
.0	Y///	1	1 0/0222		by at 11 - 12.1 ft., oxidation streaked.	l	
1	Y///	1	1	I to still cta	y at II It., Unidelial Streaked.	1	
i I	Y///	1	1	-		1	
l i	Y///	1	1	1		I I	
12.1	Y///	1	I I U/CLLR	 Claye #c abo	ove, no roots, minor calcareous debris.	 Sandy/engry +on	
12.1	Y///	1	l OVERTI	juley: AS 6D0	ove, in tools, millot cattereous ucults.	Sandy/soggy top very regular -	
I	V///	1	! !	!		function of	
1	V//	ł	1	1		sampler?	
 		.) .1	I I U/SDCL	 	Orange - very fine grained, saturated,	lambie:	
14.1 	' '	1	0/30CL	1	ery poorly sorted, quartzose, minor	1	
1	 · · · · ·		1			1	
	 	4	1 11/01/2	•	s stain, 14.1 - 14.8 ft.	1	
15	V//	1	U/CLLR		prown-black, firm to stiff.	1	
15.9	14-4-4	1	U/CLLR		: As above, 15.9 - 16.3 ft.	1	
17			U/SDCL	Sand: As abo		1	
17.9	' ///	Į.	U/CLLR	• •	ove, dark brown to black, minor calcareous	1	
· l	V//	1	1	!'	rm to stiff, moist to wet, abundant	1	
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ 	4	1	•	s stains, minor oxidation.	 	
18	 	.[U/SDSH	Sand: Silty,	, clayey, saturated, as above 18 - 18.6 ft.	Very regular -	
	1777	1	1			ffill?	
19	\$///	Γ	U/CLLR	Clay: As abo		1	
19.9	Y///	1	U/CLLR		he layer between 19.9 - 20 ft. and between	!	
!	1///	1	!	21.8 - 22 ft	t. with intervening clay, as above.	!	
I	Y///	1	1	1		1	
	1///	1					

						
		DRPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 3 SHEETS		
1. PROJECT: CARS	· •			7. TOTAL DEPTH OF HOLE: 40.6 ft BGL		
	PHASE II S			8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: FL					Mobile Drill B-61	
3. DRILLING AGENC		onmental Dri	(lers, Inc.	10. NO. OF SAMPLES TAKEN: 26		
4. HOLE NO.: LFO		D Dl		11. ELEVATION GROUND WATER:		
5. NAME OF GEOLOG		B. Blount		1 12. DATE HOLE ESTABLISHED: 3/19/90		
6. COORDINATES OF		398082.81	•	13. SURFACE ELEVATION: 626.50 ft MSL 14. BACKGROUND:		
X: 2019457.49	9 <u>Y:</u>	370002.01		15. MEASURING POINT ELEVATION:		
Depth Graphic	Blow	Soil	1	13. HEASORING POINT ELEVATION.		
(Ft.) Log			t Visual Descri	intion	l Remarks [
1///	l l	ctuss/cooc	1		l l	
22	 	U/CLLR	 Clay: As abov	ve, with abundant calcareous debris.	 	
23.4	 	U/SLCL	•	ange, slightly clayey, wet, slightly sandy, ry structures, cohesive.		
25.4	 	U/SDSM	Sand: Tan/ord sorted, quar- lamina, subre silt.	Sharp contact. Driller says hard and soft layers when augering between 15 and 25 ft.		
26	 	U/SILT	Silt: As above above); silty			
29.3	i	U/SDSM	•	ve, no silt, no sediment structures, except	i i	
	 	IIICDSM	1 1	arbonaceous laminae.		
32.2 O · O · O	; 	U/GRSM	CaCO3 fragment smaller; sub-	ge, very poorly sorted, CaCO3 and quartz; nts all > 15 mm; quartz fragments most of rounded, slightly sandy, wet, loose, ment equals 5 - 10 mm up to 75 mm, slight ess.	Sharp Contact.	
36 000	, 	U/GRVL	1	'clean', better sorting, predominately and/clay, minor shell fragments.	Sharp Contact.	
37.1000	 	U/GRVL	Gravel: Clean	n as above.		
39.5000	 	U/GRVL	 Gravel: Dark	er in color, black staining throughout.	 TCE? No reading	
40 0.0.0 1 0.0.0 0.0.0		U/SDGR	:	vel: Fine grained gravel and sand, poorly loose, with broken shell fragments.		
0.0.0	 		 			

DRILLING LOG	PADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEE	T 3 OF 3 SHEETS	
1. PROJECT:				INSTALLATION: CARSWELL AFB, TX SHEET 3 OF 3 SHEETS 7. TOTAL DEPTH OF HOLE: 40.6 ft BGL		
	IRP PHASE II	-		8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION:			-	9. MANUFACTURER'S DESIGNATION OF DRILL:		
		ironmental Dr	illers Inc	10. NO. OF SAMPLES TAKEN: 26		
4. HOLE NO.:		11 OFFICING DI	11101	11. ELEVATION GROUND WATER:		
5. NAME OF G		R Rigent		12. DATE HOLE ESTABLISHED: 3/19/90		
6. COORDINAT		. b. btount		13. SURFACE ELEVATION: 626.50 ft MSL		
	57.49 Y:	398082.81		14. BACKGROUND:		
		370000101		15. MEASURING POINT ELEVATION:		
epth Graphi	c Blow	Soil	1		1	
Ft.) Log	Count	:	 Visual Descr	ription	Remarks	
40.4	I 50	U/MARL		clayey/chaulky, predominantly welded	39.5 - 44.5 ft.	
i	1	0,12412	•	shell fragments, fissile to brittle,	recovered 2.5 ft.,	
i	İ	i	semi-indurat		but 1.5 ft. was	
i	i			,	sluff. Auger	
1	İ	1	i	,	refusal at 40.5	
1	İ				ft., went in with	
	i	i	i		SS; 50 blows and	
i	i	1	i		1.5 in. recovery;	
i	i	i	i		T.D. at 40.6 ft.	
	i	i	i			
i	i	i	i			
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DRIL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 2 SHEETS			
1. PI	ROJECT: CAR	SWELL AFB,		j	7. TOTAL DEPTH OF HOLE: 23.1 ft BGL			
<u></u>	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: see level			
] 2. LO	OCATION: F	<u>lightline</u>	Area		9. MANUFACTURER'S DESIGNATION OF DRILL:	Hobile Drill B-61		
1 3. DI	RILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 12			
1 4. H	DLE NO.: L	F05-16			11. ELEVATION GROUND WATER:			
5. N	AME OF GEOL	OGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/19/90			
6. 0	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 612,30 ft MSL			
<u> x:</u>	2021041.	70 Y:_	398229.39		14. BACKGROUND:			
<u> </u>					15. MEASURING POINT ELEVATION:			
Depth	Graphic	Blow	Soil	1				
<u> (Ft.)</u>	Log	Count	Class/Code	Visual Descr	iption	<u>Remarks</u>		
0	[///]		U/CLAY	Clay: Brown	with orange cast, soft to firm, soil top,	Full sample		
1	[///		1	rootlets to	bottom, dry to damp, semi-plastic.	recovery unless		
1	<i>[///</i>]		1	1		otherwise noted.		
1	ľ///		1	1				
2	r///		U/CLLR	Clay: Brown,	very stiff, brittle, abundant calcareous	Can not cut with		
1	Y///		1	fragments/sh	ells, very minor rootlets, minor	knife.		
1	Y//A		1	carbonaceous	flecks, dry to damp.			
Ì	$Y//\lambda$		1	1		j i		
j 4	$V//\lambda$		U/CLLR	Clay: 'Calid	he' - dessication cracked, white/brown/buff	0.2 ft. Sample		
i	$V//\lambda$		i	mottled, cale	careous debris up to 10 mm, dry, 'hard' -	recovery.		
i			i	stiff/brittle.				
i	V//X	l	i	1		i i		
6			U/CLLR	' Clav: 'Calic	he' as above, well indurated intervals,	1 ft. Recovery to		
1			1	•	; limestone inclusions up to 20 mm.	refusal at 7 ft.		
7		,	 U/CLLR		Driller says			
1	Y///		1	•	e as above, thin indurated zones; mostly iff, highly calcareous buff/orange clay	limestone; will		
¦ i	Y///			with inclusion	drive 7 - 8.5 ft.;			
-	Y///		1	:	full recovery SS.			
	/ 		l uteness	sandy from 8	nt calcareous debris to 9.6 ft red, fine	•		
9			U/SDSM			· ·		
!			ļ	· -	silt, quartzose, dry and angular to 9.6	Full recovery.		
!			ļ		low 9.6 ft. is orange/yellow, very fine			
!	1 to 1		ļ	•	se, subangular, > 95% quartz, dry.			
10	0.0.0		U/SDLR	•	ve, thin gravel horizions developed 10.5 -	ļ		
	, ×, ×, ;			10.8 ft., 12	! - 12.6 ft.; color laminae - 3 mm -			
	0.0.0		1	orange/yello	w. Gravel up to 30 mm; minor gravel in sand	1		
1	1.0.0.0			very fine gr	ained - fine grained, orange to 15 ft.			
1	0.0.0		1	1		1		
İ	1.0.0.0		1			1		
14	6.0.0		U/SDLR	Sand: As abo	ove.			
i		ĺ	1	1		1		
i			İ	İ				
i	h.n.n		i	i		İ		
1 16	1.0.0.0	1	U/SDLR	Sand: As abo	ove, few gravel/calcareous concretions	Not sufficient		
1	0.00		1	•	moist at 16.5 ft, wet at 18.5 ft., gravel	gravel to be		
ł	0.0.0	}	1		minor color laminae.	classified as sand		
ļ	hinn		-	ا سود دی سوست. ا	, miral cotor tamilac.	and gravel (10%);		
-	MAN	}	1	1				
- !	1.0.0.0	}	Į.	!		water at ~ 19 ft.		
! .	0.00	!	!	1		1		
19	0.0.0	[U/SDLR		ove, minor very coarse sand/fine gravel,	!		
ļ	6.0.0	Į	Ţ	•	orange, very fine grained, saturated,	!		
l		1	1	quartzose, s	subangular, > 95% quartz with moderate	<u>,</u>		
1	1.0.0.0	1	1	sorting.		1		
	$b.\tilde{0}.\tilde{0}$]	1	1		1		
	1.0.0.0	1	1	1		1		
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DRILLING LOG RADIAN CORPORATION			INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 1 SHEETS		
1. PROJECT: CARSWELL AFB,			7. TOTAL DEPTH OF HOLE: 16.6 ft BGL		
IRP PHASE II STAGE 2			8. DATUM FOR ELEVATION SHOWN: sea level		
2. LOCATION: Flightline Area			9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61	
3. DRILLING AGENCY: Envi	ronmental Dri	llers, inc.	10. NO. OF SAMPLES TAKEN: 9		
4. HOLE NO.: LF05-17			11. ELEVATION GROUND WATER:		
5. NAME OF GEOLOGIST: S.	B. Blount		12. DATE HOLE ESTABLISHED: 3/19/90		
6. COORDINATES OF HOLE:			13. SURFACE ELEVATION: 606.50 ft MSL		
X: 2021241.43 Y:	398317.23		14. BACKGROUND:		
			15. MEASURING POINT ELEVATION:		
Depth Graphic Blow	Soil	1			
(Ft.) Log Count	Class/Code	Visual Descr	iption	Remarks	
10 [//]	U/CLLR	Clay: Brown,	soft - firm, silty with minor very fine	Full recovery	
1 [///]	1	grained sand,	, roots, moist, minor calcareous pebbles	unless otherwise	
	1	and carbonace	eous staining, semi-plastic.	noted.	
1 1///		1		1	
! 1///	1				
! ! ///	1	1		1	
3 / /	U/CLLR	Clay: As above	ve at 3 ft., with abundant calcareous		
! (///	I	pebbles.		1	
3.2 · O · O · 9	U/GRCL	Gravel, Clay	, and Sand: Gravel is calcareous, dry to	Gravel Contacts.	
[[D:0:0]	I	damp, calich	ified, < 15 mm, buff, wetness increases	1	
1 1.0.0.1		with depth,	very poorly sorted with clay lenses. Clay		
	1	is as above.			
4.5	U/SAND	Sand: Sand is	s very fine grained - fine grained, orange	Sharp Contact.	
1 1:::::1	1	oxidized at	top grading to buff/yellow at 5 ft.,		
	1	subrounded, a	moderately well sorted, moist, quartzose		
1 [1	with > 95% qu	uartz, small shell fragments abundant to 10	1	
	1	ft. Grain si:	ze up to sand/gravel at 6.8 ft., then very	İ	
1 (1	fine grained			
<u> </u>		1		İ	
9.4	U/CLLR	Clay: Minor :	shell fragments.		
10	U/SDVF	Sand: As above	ve, very fine grained, well sorted,	2.5 ft. Recovery.	
 	1	subangular to	o subround, moist to wet, color laminated,		
1 [• • • • [1	> 95% quartz	•		
1 17.7.7.7	1	1			
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14 (• • • • (U/SDVF	Sand: As above	ve.	No visible	
	1	1		contamination, but	
	1	1		high Drager	
	1	1		readings 1 ft.	
1 (1.1.1.1)	1	1		Recovery.	
16	U/SDVF	Sand: As above	ve.	No odor.	
16.5	U/MARL	Marl/Limeston	ne: Micritic, light grey, dense, many small	Sample description	
	1	1	rystallized), well indurated, chaulky	from small	
1 1	1	surface.		fragments,	
	1	1		apparently very	
	1	1		hard. T.D. at 16.6	
1 1 1	1	1		ft.	
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1 1 1	1	1			
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DRILLING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET	2 OF 2 SHEETS
		7. TOTAL DEPTH OF HOLE: 24.0 ft BGL			
IRP PHASE II STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level			
2. LOCATION:				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
		1 10. NO. OF SAMPLES TAKEN: 10			
4. HOLE NO.:			_	11. ELEVATION GROUND WATER: 594.11 ft	ISL (6/18/90)
5. NAME OF GEO		E. Fain		12. DATE HOLE ESTABLISHED: 3/21/90	
6. COORDINATES	-			13. SURFACE ELEVATION: 612.10 ft MSL	
x: 2021280		398169.30		14. BACKGROUND:	
1				15. MEASURING POINT ELEVATION: 611.84	ft MSL
Depth Graphic	Blow	Soil	1		
(Ft.) Log	•	Class/Code	Visual Descr	iption	Remarks
		 	 		completion. No
		 -	 		
23.2	ł	 U/MARL	 Marl: White/	gray, indurated, oxidation staining in	 Drove 1 1/2 ft.
1 1	1	1	fractures.		S.S., 50 blows. 2
	1	1	1		in. recovery. T.D.
	1	1	1		= 23.95 ft.
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DRILLING LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB, TX SHEET 1 OF 2 SHEETS
1. PROJECT: CARSWELL AFB,	7. TOTAL DEPTH OF HOLE: 20.8 ft BGL
IRP PHASE II STAGE 2	8. DATUM FOR ELEVATION SHOWN: sea level
2. LOCATION: Flightline Area	9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61
3. DRILLING AGENCY: Environmental Dril	
4. HOLE NO.: LF05-19	11. ELEVATION GROUND WATER: 593.54 ft MSL (6/18/90)
5. NAME OF GEOLOGIST: S. E. Fain	12. DATE HOLE ESTABLISHED: 3/21/90
6. COORDINATES OF HOLE:	13. SURFACE ELEVATION: 606.30 ft MSL
X: 2021663.85 Y: 397850.57	14. BACKGROUND:
	15. MEASURING POINT ELEVATION: 606.08 ft MSL
Depth Graphic Blow Soil	
	Visual Description Remarks
	Clay: Dark brown first 1 ft., then orange/brown with 0.3 ft. Recovery.
	abundant calcareous material, damp, cohesive. Stuck in shelby tube.
2 U/SDMD :	Sand: Orange, cemented 3 - 4 ft., medium grained, dry.
	Sand: Orange, fine to medium grained, quartzose, damp, 1 ft. Recovery. loose.
i i	Limestone: 1 in. limestone bed underlain by 2 in. cemented sand at 6.0 ft.
0.0.0	Sand and Gravel: Orange, poorly sorted, very fine 1 ft. Recovery. grained sand to pebble size gravel, damp. Gravel is subround.
	Sand and Gravel: Orange, 60% sand, 40% gravel, damp, 4.2 ft. Recovery. oxidation staining 11 - 13 ft; occasional limestone cobbles and thin beds, saturated at - 13.5 ft.
	Gravel and Sand: As above but > 80% gravels (mainly 2 - W.L. measured at 10 mm), saturated, assorted sand sizes, gravels mainly 13.6 ft. 3.6 ft. subround chert and angular limestone clasts. Recovery.
0.0.0.0	Gravel and Sand: 80% gravels 2 to 25 mm, 20% assorted sand sizes, saturated, numerous shells (gryphea?); 19 - 19.3 ft. medium sand bed.

DRILLING LOG RADIAN CORPORATION			CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2 OF 2 SHEETS		
1. PROJECT: CARSWELL AFB,		7. TOTAL DEPTH OF HOLE: 20.8 ft BGL					
IRP PHASE II STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level					
2. LOCATION: Flightline Area		9. MANUFACTURER'S DESIGNATION OF DRILL: Mobile Drill B-61					
3. DRILLING AGENCY: Environmental Drillers, Inc.		10. NO. OF SAMPLES TAKEN: 9					
4. HOLE NO.: LF05-19		11. ELEVATION GROUND WATER: 593.54 ft MSL (6/18/90)					
		OGIST: S.	E. Fain		12. DATE HOLE ESTABLISHED: 3/21/90		
	OORD INATES			<u> </u>	13. SURFACE ELEVATION: 606.30 ft MSL		
		.85 Y:	397850.57_	•	14. BACKGROUND:		
L					15. MEASURING POINT ELEVATION: 606.08 f	t MSL	
Depth	Graphic	Blow	Soil	1			
(Ft.)	Log	Count	Class/Code _	Visual Descr	iption	Remarks	
20.5		50	U/MARL	Marl: Limest	one, weathered, tan/white, indurated but	Sampling hard at	
i]	i	•	tured, oxidation staining on fracture	20 - 20.5 ft.;	
i		į	į	faces.		Drove 1 1/2 ft.	
i		İ	i	j		S.S., 50 blows =	
i]	i	i		2.5 in. T.D. =	
i	i	İ	i	i		20.75 ft.	
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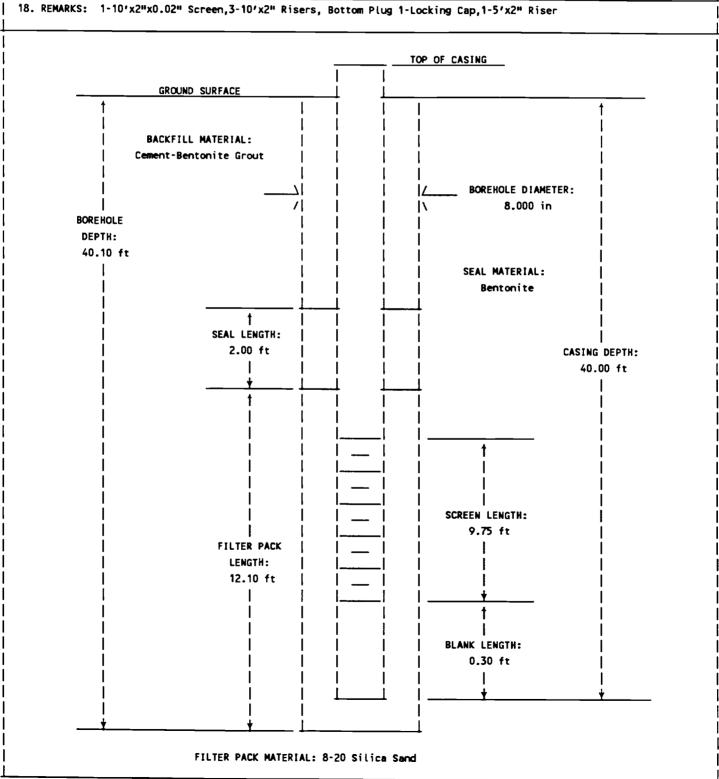
APPENDIX B

Well Completion Summaries

(Previous Well Completion Summaries may be found in CH2M Hill (1984), Radian (1986), and Radian (1989))

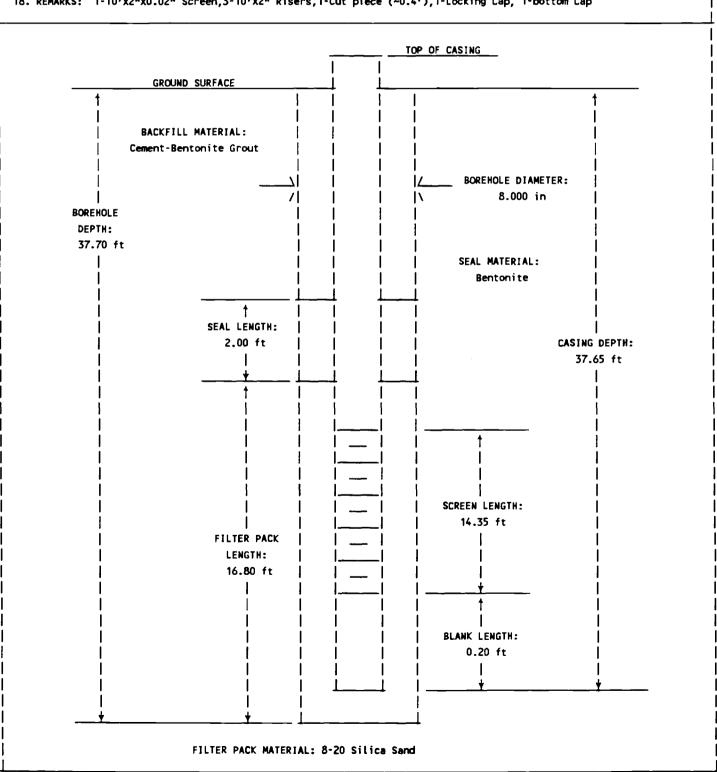
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WELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
1. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/23/90
	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
2. LOCATION: Site LF04	11. ZONE OF COMPLETION: Aquifer
3. INSTALLING CO.: Radian Corporation	12. SEAL END DEPTH: 28.00 ft
4. WELL NO.: LF04-01	13. MEAS. POINT ELEV.: 629.24 ft MSL
5. WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 2.00 in
6. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 40 PVC
7. FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 29.95 ft
8. LOCATION TYPE: WL	17. SCREEN SLOT SIZE: 0.02 in

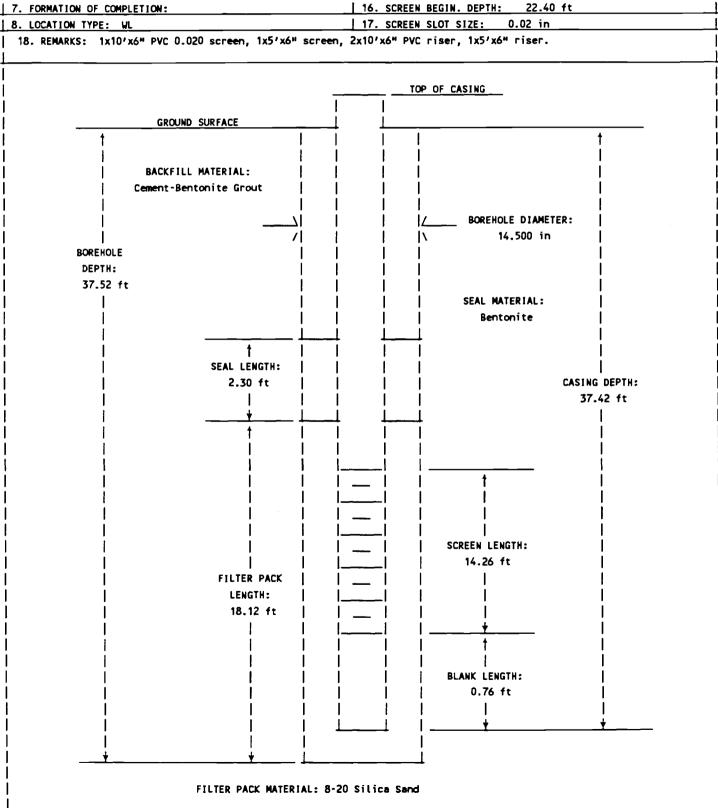


WELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
1. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/28/90
	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
2. LOCATION: Site LF04	11. ZONE OF COMPLETION: Aguifer
3. INSTALLING CO.: Radian Corporation	12. SEAL END DEPTH: 20.90 ft
4. WELL NO.: LF04-02	13. MEAS. POINT ELEV.: 623.68 ft MSL
5. WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 2.00 in
6. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 40 PVC
7. FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 23.10 ft
8. LOCATION TYPE: WL	17. SCREEN SLOT SIZE: 0.02 in





ELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 4/3/90
	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
LOCATION: Site LF04	11. ZONE OF COMPLETION: Aquifer
. INSTALLING CO.: Radian Corporation	12. SEAL END DEPTH: 19.40 ft
WELL NO.: LF04-03	13. MEAS. POINT ELEV.: 623.25 ft MSL
WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 6.00 in
. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 80 PVC
FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 22.40 ft
. LOCATION TYPE: WL	17. SCREEN SLOT SIZE: 0.02 in



ELL COMPLETION LOG RA	DIAN CORPORATION	INSTALLATION: CARSWELL AFB		
. PROJECT: IRP PHASE II STAGE		9. INSTALLATION DATE: 3/20/90		
		10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN		
. LOCATION: Site LF04		11. ZONE OF COMPLETION: Aquifer		
. INSTALLING CO.: Radian Con	poration	12. SEAL END DEPTH: 13.20 ft		
. WELL NO.: LF04-04		13. MEAS. POINT ELEV.: 612.07 ft MSL		
. WELL OWNER: U.S. AIR FORCE	<u> </u>	14. CASING DIAMETER: 2.00 in		
. WELL TYPE CLASS: MONITORIN	IG WELL	15. CASING MATERIAL: Schedule 40 PVC		
_ FORMATION OF COMPLETION:		16. SCREEN BEGIN. DEPTH: 15.20 ft		
. LOCATION TYPE: WL	Zana Banalanian 257 BLB	17. SCREEN SLOT SIZE: 0.02 in . * Cave-in from 25.2' - 24.8'		
		TOP OF CASING		
GROUI	ID SURFACE			
†	1			
	i	i i i		
BACKFI	L MATERIAL:	i i		
Cement-B	entonite Grout			
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1		BOREHOLE DIAMETER:		
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BOREHOLE	1			
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25.20 ft	Į.			
!	ļ	SEAL MATERIAL:		
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	, ,	SCREEN LENGTH:		
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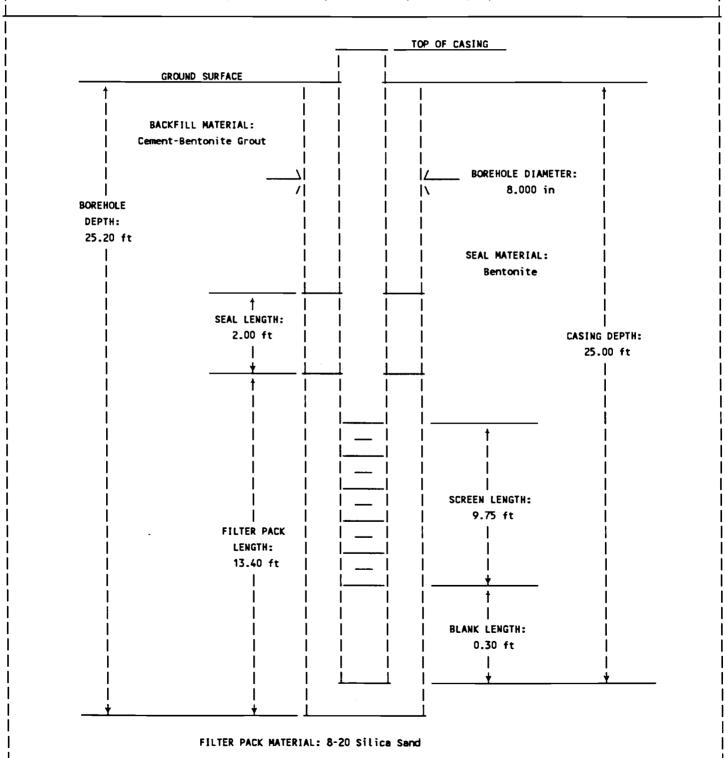
WELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
1. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 4/2/90
	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
2. LOCATION: Site LF04	11. ZONE OF COMPLETION: Aquifer
3. INSTALLING CO.: Redian Corporation	12. SEAL END DEPTH: 30.00 ft
4. WELL NO.: LF04-10	13. MEAS. POINT ELEV.: 626.54 ft MSL
5. WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 2.00 in
5. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 40 PVC
7. FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 39.22 ft
B. LOCATION TYPE: WL	1 17. SCREEN SLOT SIZE: 0.02 in en (0.020 SL), 1x2"x0.2' Sed. Trap, 1 - Locking 2" topcap,
Flush mount in cast iron vault - grout	
	TOP OF CASING
GROUND SURFACE	<u> </u>
<u> </u>	1 1 1
BACKFILL MATERIAL:	
Cement-Bentonite Grout	!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
}	BOREHOLE DIAMETER:
BOREHOLE }	
DEPTH:	
49.50 ft	
1	
	Bentonite
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SEAL LENGTH:	i i i
4.20 ft	CASING DEPTH:
	49.10 ft
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	SCREEN LENGTH:
	9.73 ft
FILTER PACK LENGTH:	-
LENGTH: 19.50 ft	
19.30 ft 19.30 ft	
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	0.15 ft
	+
<u> </u>	1

FILTER PACK MATERIAL: 8-20 Silica Sand

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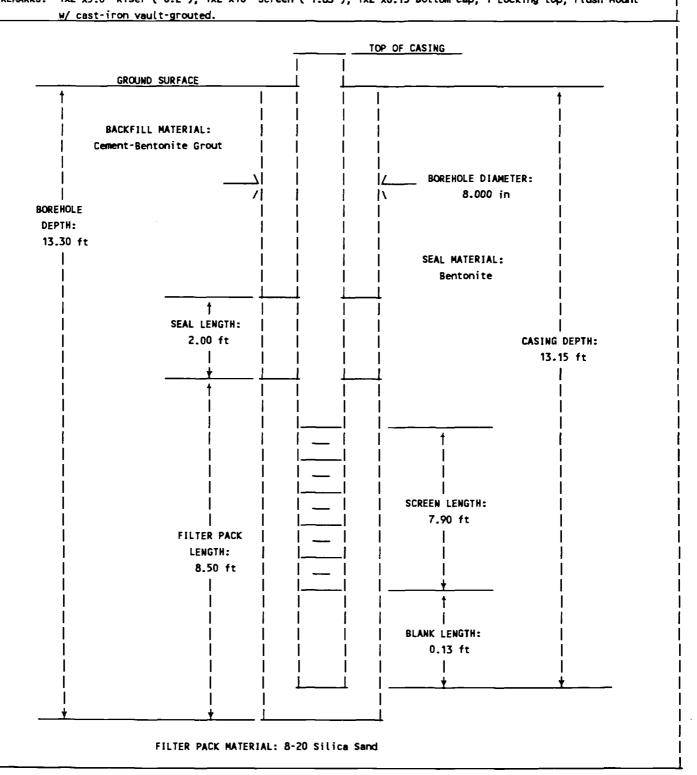
WELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
1. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/22/90
	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
2. LOCATION: Site LF05	11. ZONE OF COMPLETION: Aquifer
3. INSTALLING CO.: Radian Corporation	12. SEAL END DEPTH: 11.80 ft
4. WELL NO.: LF05-01	13. MEAS. POINT ELEV.: 621.96 ft MSL
5. WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 2.00 in
6. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 40 PVC
7. FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 14.95 ft
8. LOCATION TYPE: WL	17. SCREEN SLOT SIZE: 0.02 in
46	

18. REMARKS: 1-10'x2"x0.02" Screen, 2-10'x2" Risers, 1-0.2 Bottom, 1-Locking Cap



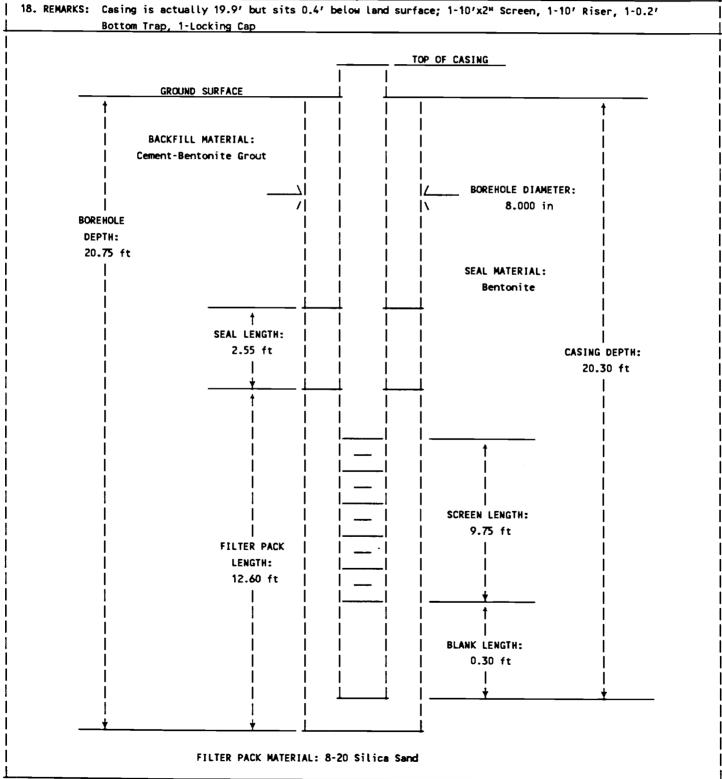
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	RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
PROJECT: IRP PHASE	II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/22/90
		10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
LOCATION: Site LF		11. ZONE OF COMPLETION: Aquifer
INSTALLING CO.: R	· · · · · ·	12. SEAL END DEPTH: 15.00 ft
WELL NO.: LF05-02		13. MEAS. POINT ELEV.: 622.69 ft MSL
WELL OWNER: U.S.		14. CASING DIAMETER: 2.00 in
WELL TYPE CLASS:		15. CASING MATERIAL: Schedule 40 PVC
FORMATION OF COMPL LOCATION TYPE: WL		16. SCREEN BEGIN. DEPTH: 16.95 ft 17. SCREEN SLOT SIZE: 0.02 in
	2"x0.02" Screen, 2-10'x2" Risers,	_
		TOP OF CASING
	•	
	GROUND SURFACE	
Ţ		!
	BACKFILL MATERIAL:	
i 1	Cement-Bentonite Grout	
i	\id	
İ	; i	8.000 in
BOREHOLE	Ì	i i i
DEPTH:	1	
27.20 ft	1	
1	1	SEAL MATERIAL:
Ţ	Į.	Bentonite
1		<u> </u>
į.	† j	
į,	SEAL LENGTH:	
} !	2.00 ft	CASING DEPTH:
l f		27.00 ft
, 1	<u> </u>	}
i	i i	
i	i i	
i	i i	
i	i i	i <u> </u>
ļ	i i	
1	1 1	<u> </u>
1	1 1	SCREEN LENGTH:
ļ	1 1	9.75 ft
ļ	FILTER PACK	
[LENGTH:	<u> </u>
ļ	12.20 ft	! ! ! ! !
	1 1	
 		1 1 1 1
 	1 1	
1 1	! !	
1 1		1 0.30
1 1		1
1		
1	<u> </u>	
₩	▼ • • • • • • • • • • • • • • • • • • •	

INSTALLATION: CARSWELL AFB
9. INSTALLATION DATE: 4/2/90
10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
11. ZONE OF COMPLETION: Aguifer
12. SEAL END DEPTH: 4.80 ft
13. MEAS. POINT ELEV.: 602.98 ft MSL
14. CASING DIAMETER: 2.00 in
15. CASING MATERIAL: Schedule 40 PVC
16. SCREEN BEGIN. DEPTH: 5.12 ft
17. SCREEN SLOT SIZE: 0.02 in



			64 254
L COMPLETION LOG RA	DIAN CORPORATION	INSTALLATION: CARSWELL AF	В
PROJECT: IRP PHASE II STAGE	2, CARSWELL AFB	9. INSTALLATION DATE: 3/	/21/90
		10. WELL COMPLETION METHO	
LOCATION: Site LF05		11. ZONE OF COMPLETION:	
INSTALLING CO.: Radian Cor	poration	12. SEAL END DEPTH: 11.6	
WELL NO.: LF05-18		13. MEAS. POINT ELEV.:	
WELL OWNER: U.S. AIR FORCE		14. CASING DIAMETER: 2	
WELL TYPE CLASS: MONITORIN	<u>G WELL</u>	15. CASING MATERIAL: Sch	
FORMATION OF COMPLETION:		16. SCREEN BEGIN. DEPTH:	
LOCATION TYPE: WL B. REMARKS:		17. SCREEN SLOT SIZE:	0.02 in
		TOP OF CASING	
		<u> </u>	
GROUN	D SURFACE	<u> </u>	
1 1			1
RACKETI	L MATERIAL:	, , , , 	i I
· ·	ntonite Grout	i i i	i
		i i i	i
į		BOREHO	LE DIAMETER:
j	<u></u> ;	i i i	8.000 in
BOREHOLE	1	1 1 1	1
DEPTH:	I	ļ ļ	1
23.95 ft	!	!!!	
	ļ.	SEAL MA	•
	ļ	Bento	oni te
ł		 	· ·
l l	SEAL LENGTH:		-
	2.00 ft	i i i	CASING DEPTH:
i	1 1	i i i	23.95 ft
i	<u>+</u> i	i i <u> i</u>	1
İ	<u> </u>	ī	İ
İ	i i	i i i	ĺ
1	1 1	ll l	
l			<u>Į</u>
ļ.	į į	!!!!!!	ļ.
<u> </u>	ļ ļ	!!!!	ļ.
<u> </u>			
 		SCREEN LEN 9.74 f	•
↓ 	 FILTER PACK		1
 	LENGTH:	-	- 1
<u> </u>	12.75 ft		i
! 		-	i
i	ii	i i †	 i
i	i i	i i i i	i
į	į į	BLANK LENG	TH:
j	i i	0.30 f	ft j
j	i i		1
1	1 1		<u> </u>
1	1 1	I	
l	•		

WELL COMPLETION LOG RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
1. PROJECT: IRP PHASE II STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/21/90
<u> </u>	10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
2. LOCATION: Site LF05	11. ZONE OF COMPLETION: Aquifer
3. INSTALLING CO.: Radian Corporation	12. SEAL END DEPTH: 8.15 ft
4. WELL NO.: LF05-19	13. MEAS. POINT ELEV.: 606.08 ft MSL
5. WELL OWNER: U.S. AIR FORCE	14. CASING DIAMETER: 2.00 in
6. WELL TYPE CLASS: MONITORING WELL	15. CASING MATERIAL: Schedule 40 PVC
7. FORMATION OF COMPLETION:	16. SCREEN BEGIN. DEPTH: 10.25 ft
8. LOCATION TYPE: WL	17. SCREEN SLOT SIZE: 0.02 in



APPENDIX C

Well Development Information

(Previous Well Development Information may be found in CH2M Hill (1984), Radian (1986), and Radian (1989))

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				Specific			Specific		
Location		Cumulative	Cumulative	Conductance					
<u>e</u>	Log Date	Gallons	Bore Volumes	(micromhos/cm)	Ŧ.	Temp_F	Comments	Method	
LF04-01	8/4/90	7.00		860	6.9	88.88		Bailmaster 36" Teflon Fluoroware	
		10.00		840	88.	67.82		100	
		17.00		850	88.98	68.00			
		23.00		980	6.87	68.36			
		28.00		850	6.88	68.18			
		35.00		098	6.83	68.18			
		43.00		980	6.86	68.54	Full bailer every pull, not getting		
							sed. off bottom		
		52.00	3.08	860	6.89	68.18			
LF04-02	8/4/90	5.00		098	6.91	67.28		Breinard Killmen 1 1/2" Hend Pump	
		15.00		850	6.94	67.64		-	
		20.00		840	6.91	67.10			
		30.00		840	6.91	79.79	20 Minute stop to repair		
							pump; pulled pump 4' off bottom to		
C-							keep sed. from clogging		
·3		38.00		840	6.91	68.72			
		48.00		840	6.91	68.36			
		53.00		840	6.93	68.00	Go to 2nd 55 gal. barrel		
		63.00		850	6.94	68.00			
		82.00		840	6.95	68.36			
		87.00	68-7	840	6.94	68.36			
LF04-03	12/4/90	8.00		750	6.53	70.79		Brainard Killman 1 1/2" Hand Pump	
		34.00		810	6.74	95.79	Break to check on crew	-	
		68.00		820	6.63	68.90			
		90.00		920	6.65	77.69			
		115.00		830	6.68	80.69	Break to check on crew		
		152.00		820	6.63	69.80			E ,4
		174.00		840	\$.6	80.69			ł
		195.00	3.72	850	92.9	22.89			2
LF04-04	10/4/90	7.00		840	6.77	65.12	Full bailer every pull	Bailmaster 36" Teflon Fluoroware	58
		15.00		850	6.79	%.%		פפורפו	

Location		Cumulative	Cumulative	Specific Conductance				
2	Log Date	Gallons	Bore Volumes	(micromhos/cm)	풉	Temp_F	Comments	Method
		23.00		860	6.81	64.58		
		31.00		860	6.72	64.76		
		38.00		850	6.73	64.78		
		46.00		860	6. 7	76.79		
		55.00	3.71	850	6.77	64.58		
LF04-10	13/4/90	3.00		730	7.40	67.10		Bailmaster 36" Teflon Fluoroware
		24 00		020		9		Bailer
					7.0	00.80		
		32.00		076	6.93	67.82		
		43.00		950	6.90	67.64		
		75.00		950	6.90	67.64		
		55.00		076	6.83	79.79		
		90.09		076	6.91	67.28		
		70.00		950	6.87	79.79		
		82.00	3.25	076	6.86	67.82		
LF05-01	8/4/90	3.00		1440	6.78	66.92		Railmater 34H Tetlon Elucrouste
		10.00		1170	6.83	67, 10		Bailer
		18.00		1370	24	67 10	or contract to the second	
		24.00		1080	6.80	27 29	ABISO (SIGNIE) SILES TOOLS	
		29.00		1020	8. 85	77 27		
		40.00	4.56	096	6.81	68.00		
LF05-02	06/7/2	7.00		1110	6.58	66.20		Brainard Killman 1 1/2" Hand Pimm
		10.00		1120	6.68	66.56		
		25.00		1120	6.61	66.56	Pumping at approx. 5 apm W/ no draw	
		32.00		1120	6.54	66.56	5 min. down time: visitor at site	
		43.00		1120	6.63	8.8		
		49.00		1110	6.63	\$.3		
		53.00	5.96	1120	69.9	64.76		
;	;	;						64
LF05-14	06/7/6	2.00		920	6.64 4	63.50	Temp taken after 2 min ≈ low	Bailmaster 36" Teflon Fluoroware
		10.00		910	7.24	63.32	Orig Temp ok	25
		16.00		910	6.64	62.60	Some pulls only 85% full	
		22.00		910	6.63	62.60		

WELL DEVELOPMENT DATA - CARSWELL AFB

					HHHHHH	10 10 10 10 10 10 10 10 10 10 10 10 10 1		
•				Specific			H DANKER III II II II II II II II II II II II I	计时间时间计算计算计算计算计算计算计算计算计算计算计算计算计算计算计算计算计算计
Location		Cumulative	Cumulative	Conductance				
<u> </u>	Log Date	Gallons	Bore Volumes	(micromhos/cm)	₹	Temp_F	Comments	Method
		31.00	5.28	910	6.65	62.60		
LF05-18	06/7/6	7.00		930	6.71	65.48	6	Bailmaster 36" Teflon Fluoroware
		10.00 18.00 26.00		920 920 920	6.70 6.71 6.67	65.84 65.66 66.02	B Full bailer every pull	Bailer
		38.00	۲.۶	920	6.65	65.84		
LF05-19	10/4/90	3.00		890	89.9	04.40	Full beiler each pull Be	Bailmaster 36" Teflon Fluoroware
		12.00 21.00		910 920	6.71	86.58	ā	Bailer
		29.00			6.76	64.22		
		36.00			6.71	07.79	Rechecked probe u/ 4 0 etd = 3 pp	
		45.00	4.41	006	6.76	66 23	46.5 - Die oit / Die oit	

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APPENDIX D

Water Quality Sampling Records

(Previous Water Quality Sampling Records may be found in CH2M Hill (1984), Radian (1986), and Radian (1989))

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PAGE 1 OF 2

_						SAMPLE DEPTH (FT.) 29.45	
IITIAL AMPI II	GROUND'	WATER DEPT D: Start <u> </u>	H (FT) <i>0950</i>	<u> 19.45 Bī</u>		T.D=41.4 BTC (SON LOES) 11.95 0.18 = 2.03 3 = 4.09g OMPLETE	ral 3 o LASM
AMPLIN	HTEM DI	OD			LOGGE	R CODE ADD	
AB CO	DE <u>RA</u>	ON	1/20		DATE	SENT <u>4-25-90</u>	
RESERV OMMEN		THOO 40C	, HNUZ	-MEIALS			
		.		_		DET	ECTIO
INAL PA	RAMETER	R MEASUREME	NTS:				TIML
		HYDROGEN	•	d S.U.			7. <i>01</i>
	C CONDI	JCTANCE	S(E)		s/cm	94.2	/
	ATURE	~ L		mvoi			21
LKALI	NITY (Ca	CO ₃)		LK mg/i	•		
PAKU. TOTAL	ALK = 0 UNFILTER	100 ALK = 565"	nig/L	TOTAL	FILTE	ALK = 364 Mg/L	•
TIME	_	VOLUME DRAWN	pН	SC (umhos/cm)	TEMP.	COMMENTS	
Ĺ		Boss Maturas			. 0,		
	(GALS)	Bore Volumes	! 				
0910	(GALS) 0.0	0.0	-	-	-	START PUMPING	
0910			- 6.81	950	70°F	START PUMPING OF ANGE BROWN MOR. TARBIT)
	0.0		- 6.81	960	70°F 70°F	,)
0915	1.0		- 6.81 6.89		70°F 70°F 70°F	DRAWSE BROWN MOD. TARBIT)
U915 U91B	0.0 1.0 2.0 3.0 4.0		- 6.81 6.89 6.97 6.93	960 956 95B	70°F 70°F 70°F 70.5°F	ORANGE BROWN, MOD. TARSIN)
U915 U91B O974	1.0 2.0 3.0 4.0 5.0		- 6.81 6.89	960 956 95B 959	70°F 70°F 70°F 70.5°F 70.5°F	ORANGE BROWN, MOD. TARBIT)
U915 U91B O971 U930	0.0 1.0 2.0 3.0 4.0		- 6.81 6.89 6.97 6.93	960 956 95B	70°F 70°F 70°F 70.5°F	ORANGE BROWN, MOD. TARSIN	2
U915 U91B O971 U930	1.0 2.0 3.0 4.0 5.0		- 6.81 6.89 6.97 6.93 6.87	960 956 95B 959	70°F 70°F 70°F 70.5°F 70.5°F	ORANGE BROWN, MOA. TARBIT	2
U915 U91B O971 U930	1.0 2.0 3.0 4.0 5.0		- 6.81 6.89 6.97 6.93 6.87	960 956 95B 959	70°F 70°F 70°F 70.5°F 70.5°F	ORANGE BROWN, MOA. TARBIT	2
U915 U91B O971 U930	1.0 2.0 3.0 4.0 5.0		- 6.81 6.89 6.97 6.93 6.87	960 956 95B 959	70°F 70°F 70°F 70.5°F 70.5°F	ORANGE BROWN, MOA. TARBIT	?
U915 U91B O971 U930	1.0 2.0 3.0 4.0 5.0		- 6.81 6.89 6.97 6.93 6.87	960 956 95B 959	70°F 70°F 70°F 70.5°F 70.5°F	ORANGE BROWN, MOA. TARBIT	

LB - LAB BLANK PP - PERISTALIC PUMP

N - NORMAL

KNOWN

SL - SUCTION LIFT PUMP

BP - BLADDER PUMP

PAGE 1 OF 2

SAMPLE T	YPE/	SAI	MPLE ID			NO	
Bamplii Bamplii Lab Co Preserv	NG PERIOD NG METHOR DE	START_	1157		LOGGE Date	R CODE RADN SENT 4-17-90	
POTENT SPECIFI REDOX TEMPER ALKALII	NITY (CAC	DROGEN TANCE	pi Si E Ti	h mvol EMP °C LK mg/l	s/cm ts	433	DETECT LIMIT D. O.
TIME	TOTAL WITHOU	FALLS ALK: OLUME RAWN	рН	SC (umhos/cm)	TEMP.	COMMENTS	
1138	(GALS) 0.0	O. O	-	-	-	START PUMPIN	
1140	1.0		6.75	843	700%	LT. BRUNN SLILHTLY	TUABIL
11:45	15		6.78	833	70.5°F	ii _	
1146	3.0		6.951	834	70.5°F	ii	
1149	4.0		6.83	831	70.8°F	//	
1150	5.0		6.63	830	70.7°F		
1156	7.0		6.86	833	71.0%	ALMOST CLEAR	
				- 1		·	
	TYPES (WSACC			SAMPLE METH	DS: (WSW		
		FB - FRELD BL FB - TRUP BLA		G - GRAB '		SP - SUBMERSIBLE (
176		THE THE PARTY OF T		D - DAKEN		We - WHATEL SWILL	. التقد

64 266

PAGE 1 OF 2

						NO	
SAMPL SAMPL ABC PRESE COMME	ING PERIO ING METH ODE RVATION ME	DD: START IOD	: Hn	0 102 IN ME	LOGGI DATE) h= 10.07' 3V - 5.14 COMPLETE	go
POTEN SPECI REDOX	TIAL OF I	AL CO ₃)	P S E T	H S.U. C µmhc h mvol EMP °C	os/cm its	6.82 U.	T C
TIME	TOTAL	VOLUME DRAWN	<u>l</u>	SC (umhos/cm)	TEND		<u>o)</u>
8:25	0.0	0.0	-	-	-	START PUMPING	—
8.35	2	1.17	6.66	790	18.5	orange tan mod turbic	T
8: 40	4	2.34	6.46	765	18.7	"	
B: 43	5.5	3.22	6.8.2	199	185	" "/	
						·	
BALCO							
D - R - S -			(SAMPLE METHO G - GRAB B - BAILER PP - PERISTA SL - SUCTION	LIC PUMP	SP - SUBMERSIBLE PUMP AL - AIR-LIFT SAMPLER BP - BLADDER PUMP	

PAGE 1 OF 2

AMPLE T	YPE	SAN	IPLE ID			NOSAMPLE DEPTH (FT.) _31.48 BTG
AMPLIN AMPLIN AB COI PRESERV	IG PERIOD IG METHO	: START D	///		C	OMPLETE //45 R CODE //AON SENT +//HAU VITH METALS
OTENT SPECIFIC SEDOX SEMPER	IAL OF HY C CONDUC POTENTIAL ATURE NITY (CAC	CTANCE L O3)	P S E TI	h mvol EMP °C .LK mg/l	s/cm ts	6.06 D.01 850 1 19.7 0.1
TIME TATE	TOTAL Y WITHD	Filtered = 370	1	Filtered SC (µmhos/cm)	TEMP.	COMMENTS
10:25	0.0	0.0	-	-	-	START PUMPING
1036	2.0	0.69	5.95	968	18.5	pura water clear no ide
1047	4.0	1.37	5.45		18.5	
1054	7.0	2.41	5.99	820	19.45	"
1100	8.0	2.75	6.15	840	19.5	11
1107	9.0	3.09	6.06	850	19.7	light tan slightly turbic
						·
D - D		ODE) FB - FIELD BLA TB - TRIP BLAN		SAMPLE METHI G - GRAB B - BARER	DDS: (WSM	SP - SUBMERSIBLE PUMP AL - AIR-LIFT SAMPLER

SL - SUCTION LIFT PUMP

D-6

_.. __

N - NORMAL

K - KNOWN

PAGE 1 OF 2

						O	
STIAL	GROUND	WATER DEPT	'H (FT)	7 B.10'	DIC	1.D. = 24.85' &T (SON 8.54 gal. = 3 WC MPLETE /600	MOED HECK CUSIN
AMPLI	NG METH	DD: START			LOGGER	CODE REDN	_
AB CO	DE RA	on	· ·		DATE S	ENT _5/7/90	
RESER	VATION ME	THOO 4°C	HNO	3-NIETALS			
OMME	៣ទ						
INAL P	ARAMETER	R MEASUREME	NTS:				DETECTI
OTENT	TAL OF	HYDROGEN	pi	H S.U.	-	6.96	12.0
		UCTANCE	S		s/cm .	668	
	POTENTI. RATURE	AL		h mvol EMP °C	ts .		12.1
·-		CDa)	· A		•		
FH TV	MITY (Ca EN ALK =	O.D.					/.8
		VOLUME	= 20.			TERED ALIC = 2	
TIME		DRAWN	рн	SC (umbos/cm)	TEMP.	COMMENTS	
	(GALS)	-	<u> </u>		-		
1531	0.0	0.0	-	•	-	START PUMPIN	
	2.5		62.43	672		IT. TAN SLIGHTLY	TURBIL
1535	,	1	6.99	664	65.8°A		
1537	4.0	-	1			//	
1537 1539	5.0		1,97	661	65.67		
1537 1539 1541	5.0 6.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		+		65.99A	"	
1537 1539 1541	5.0 6.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		6.94	668	65.99A	"	
1537 1539 1541 1544	5.0 6.5 8.5		6.94	668	65.99A	"	

PP - PERISTALIC PUMP

NORMAL $_{\rm D-7}$ SL - SUCTION LIFT PUMP

BP - BLADDER PUMP

LB - LAB BLANK

N -

PAGE 1 OF 2

_						SAMPLE DEPTH (FT.) 15.0	_
AMPLIN	IG PERIC	D: START	1465		c	1 D. = 25.44 BTC (Sound 5.31 gol = 3 werted call OMPLETE 1450 (N) ye.s.
AR CO	DE K	100 <u>B</u>			DATE	R CODE RADN SENT 5/7/90	
RESERV	ATION ME	THOO 4°C	HND	2-METALS			
TNAL PA	RAMETER	R MEASUREME!	vis:			_	ETEC
		HYDROGEN	pi			1.74	1). (
	C CONDI POTENTI	JCTANCE AL	S	_	s/cm	<u> </u>	
EMPER		~ C		EMP °C	••		12.
LKALI	NITY (CA HEN. ALK:	CO ₃)	A	LK mg/l	•		
Tor	AL INFI	LITEMEN ALIC:	= 531	TOTA	LFILT	TENER ALK. = 286"	7/1
TIME	WITH	DRAWN	рН	SC (umhos/cm)	TEMP.	COMMENTS	
	(GALS)	Bore Volumesi	_		_	START PUMPING	
1:100	0.0	1 11.10	,			- JIANI TOMFING	
1300	0.0	0.0	4.0	CCD	1500	William Comme	
1411	1.0	0.0	6.50	550 532		XIGHTLY CLOUDY	
-	1.0 2.0	0.0	662	532	64.20		
1411	1.0	0.0			64.2°F	11	74 (
1411 1414 1416	1.0 2.0 3.0	0.0	6.62 6.67	532 533	64.2°F	" ALMOST CLEAR SLIGHT	74 (
1414 1416 1416	1.0 2.0 3.0 4.0	0.0	6.62 6.67 6.70	532 533 521	64.2°F 63.1°F 640°F	" ALMOST CLEAR SLIGHT	7 <u>4</u>
1414 1416 1416 1414,	1.0 2.0 3.0 4.0 5.5		662 6.67 6.70 6.72 6.74	532 533 521 529	64.2°F 63.1°F 64.0°F 63.4°F	" ALMOST CLEAR SLIGHT	747
1211 1414 1416 1414, 1417	1.0 2.0 3.0 4.0 5.5		662 6.67 6.70 6.71 6.74 MENT 6.20	532 533 521 529 533 BLANK 0.01	64.2°F 63.1°F 64.0°F 63.4°F 63.0°F	" ALMOST CLEAR SLIGHT " " CLEAR	747
1414 1416 1414, 1417 1422	1.0 2.0 3.0 4.0 5.5		662 6.67 6.70 6.71 6.74 MENT 6.20	532 533 521 529 533	64.2°F 63.1°F 64.0°F 63.4°F 63.0°F	" ALMOST CLEAR SLIGHT " " CLEAR	74 (

PP - PERISTALIC PUMP

N - NORMAL $_{\mathrm{D-8}}$ SL - SUCTION LIFT PUMP

BP - BLADDER PUMP

LB - LAB BLANK

PAGE 1 OF 2

BP - BLADDER PUMP

					777	EAMPLE DEPTH (FT.) 1	, -
AMPLINAMPLINAB COPRESERV	IG PERIO IG METH	THOO 4	7535		CO	DMPLETE 1555 R CODE 1ADN BENT 4-24-90	et lasing volu
POTENT SPECIFI SEDOX SEMPER ALKALII	IAL OF P C CONDU POTENTI ATURE NITY (CA	CO3)	pt SC EI TE A	m wol EMP °C LK mg/l	s/cm ts	6.40	DETECTION LIMIT D.01 /
TOTA	TOTAL WITH	VOLUME DRAWN	рН	SC (umhos/cm)	TEMP.	COMMENTS	
ن وسرا	(GALS)	Dore Volume	• <u>4</u>		_	START PUMP	ING
1520	1.0	1	6.27	1265	69°F		
しっごフフト	2.0		6.36	1262		LT. BROWN, SLIGHTLY	TUASID
1522			633	1257	68.5°C		
1524					690=	"	
1524 1526	3.0		6.35	1269	10, - 1		
1524			6.35	1263 1263	69° F		
1524 1526 1528	3.0 4.0			1263	69°F	ORANGE/BLOWN, SCIEN	ny Cloudi
1524 1526 1528 1530	3.0 4.0 5.0		6.39	1263	69°F		TLY CLOUDT
1524 1526 1528 1530	3.0 4.0 5.0		6.39	1263	69°F		TLY CLOUD'T

PP - PERISTALIC PUMP

SL - SUCTION LIFT PUMP

LB - LAB BLANK

NORMAL

PAGE 1 OF 2

BP - BLADDER PUMP

amplin Amplin Ab Coi	IG PERIO IG METHO DE ATION ME	D: START OD	1307		CO	SUBJECT SOME SOME SOME SOME SOME SOME SOME SOME	wy v
OTENT PECIFIC EDOX EMPER LXALII	IAL OF H C CONDU POTENTIA ATURE NITY (CAC W. AUX =	AL CO+)	pH SC Eh TEN AL	дтho mvois MP °C K mg/i	.	1.81 1843 1844 ALK = 570	DETEC LIM D. d
TIME	TOTAL	VOLUME DRAWN Bore Volumes		SC umhos/cm)	TEMP.	COMMENTS	-/_
1254	0.0	0.0	1 - 1	-	-	START PUMPING	3
1256	1.0		679	905	6187	LLEAR	
1301	2.5		680	845	70.0°A	U. BADUN SUGATIY TU	ALL
1303	4.0		681	845	455	ST. ORANGE BROWN	
	5.0		682	B41_	69.5°A		
1505	6.0	1.	6.81	8,43	695°F		
t		5	1 1	_	1		
1307			1 1		1 1		
t							
i						·	
1307 1307						·	

PP - PERISTALIC PUMP

N - NORMAL $_{D^{\hspace{-0.05cm}-\hspace{-0.05cm}10}}$ SL - SUCTION LIFT PUMP

LB - LAB BLANK

PAGE 1 OF 2

NAL PARAMETER MEASUREMENTS: OTENTIAL OF HYDROGEN PH S.U. 475 PECIFIC CONDUCTANCE SC MMhos/cm 786 EDOX POTENTIAL EN mvolts TEMP °C LKALINITY (CacO3) ALK mg/l PHEM ALK - 0 TOTAL VOLUME WITHDRAWN PH (amhos/cm) (°C) (GALB) Bore volumest (GALB) Bore Volumest (105 0.0 0.0 START PUMPIN (112 2.5 GLB 786 785 "1 (115 3.5 G70 787 408"E" "1 (116 5.0 675 786 705"E" "1	
INTAL GROUNDWATER DEPTH (FT)	71.31 P
MPLING PERIOD: START	SONNOF
B CODE RAON ESERVATION METHOD 4°C AND METHOD WAL PARAMETER MEASUREMENTS: OTENTIAL OF HYDROGEN PH S.U. 475 DECIFIC CONDUCTANCE SC MMHOS/CM 786 DOX POTENTIAL EN TOWN COLUMN SC METHOD COLUMN SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD AND SC METHOD COMMENTS OF TOTAL VOLUME WITHDRAWN PH ("C) COMMENTS OF TOTAL VOLUME SC TEMP ("C) COMMENTS OF	Y
NAL PARAMETER MEASUREMENTS: DIENTIAL OF HYDROGEN PH S.U. 6.75 PECIFIC CONDUCTANCE SC MMHOS/CM 786 EDOX POTENTIAL EN MVOITS EMPERATURE TEMP °C LKALINITY (Cacos) ALK mg/1 PITOTA UNIVITEDED ALK = 2449 M9/L TOTAL FILTERED ALK = 5 TOTAL VOLUME WITHDRAWN PH (umhos/cm) (°C) COMMENTS (GALS) Bore Volumeex PH 788 780° F REMOS CLEAR SLEAT 118 5.0 670 784 785° F " 1118 3.5 670 784 785° F " 1118 5.0 675 786 785° F "	
DIMMENTS NAL PARAMETER MEASUREMENTS: DIENTIAL OF HYDROGEN PH S.U. 155 PECIFIC CONDUCTANCE SC 4mhos/cm 786 EDOX POTENTIAL Eh mvoits EMPERATURE TEMP °C LKALINITY (CaCO ₃) ALK mg/I PITOTA UNIVERSED ALL 2349 Mg/L TWENT FILTERED ALL = 2 TOTAL VOLUME WITHDRAWN PH (4mhos/cm) (°C) COMMENTS (IGALS) 180re Volumes PH (4mhos/cm) (°C) 1/105 0.0 0.0 START PUMPII 1/107 1.0 644 788 700° ALMOS WEAR SUENT 1/118 3.5 670 784 705° E " 1/118 5.0 675 786 785° "	
PECIFIC CONDUCTANCE EDOX POTENTIAL EMPERATURE EL TEMP °C LKALINITY (CaCO ₃) Present of the conductance of	
OTENTIAL OF HYDROGEN PECIFIC CONDUCTANCE EDOX POTENTIAL EMPERATURE TEMP *C LKALINITY (CACO3) PHEN ALK = 0 TOTAL UNFITZED ALK = 2449 M9/L TOTAL UNFITZED AL	DETE
PECIFIC CONDUCTANCE EDOX POTENTIAL EMPERATURE EL TEMP °C LKALINITY (CaCO ₃) Present of the conductance of	LIN
EDOX POTENTIAL EMPERATURE EMPERATURE ITEMP °C ALK mg/I PHEN ALK = 0 TOTAL VOLUME WITHDRAWN (GALS) IBORO VOLUME (IGALS) IBORO VOLUME (IGALS) IBORO VOLUME (IGALS) IBORO VOLUME (IGALS) IBORO VOLUME (IGALS) IDOS 0.0 0.0 START PUMPII IIII 2.5 666 766 705 71 IIII 5.0 475 766 705 "	<u></u>
EMPERATURE LKALINITY (CaCO3) PHEN ALK = 0 TOTAL WILLIAMS TOTAL VOLUME WITHDRAWN (GALB) Bore Volumest 1105 0.0 0.0 0.0 START PUMPII 1112 2.5 6.66 766 786 786 786 786 786 78	
Caco Alk mg/ Phew alk = 0 Total watered alk = 349 mg/ Total filtered alk = 349 mg/ Total volume	0
TOTAL UNKITERED ALK = 249 M9/L TOTAL FILTERED ALK = TIME TOTAL VOLUME WITHDRAWN PH SC (14mhos/em) (°C) COMMENTS 105	
TIME WITHDRAWN (GALS) Bore Volumes (105 0.0 0.0 START PUMPII (1104 1.0 6.64 780 700° F RUMOS CLEAR, SUEAT (1115 3.5 6.70 70.7 70.8° F " (1118 5.0 6.75 786 70.8° F " (1119 5.0 6.75 786 70.8° F "	10011
	339 -
1109 1.0 6.64 788 700° F RIMOS CIERR, SUEHT 1112 2.5 6.68 786 70.5° F " 1115 3.5 6.70 787 708° F " 1118 5.0 6.75 786 705° F "	
1112 2.5 6.68 786 70.5° 7 " 1115 3.5 6.70 787 708° 7 " 1118 5.0 6.75 786 705° 7 "	NG
1115 3.5 6.70 787 786 11 1118 5.0 6.75 786 705° = "	- 61040.
1118 5.0 6.75 786 7057 "	
AMBI ST TYPE AND	
AMBI ST TYPE AND ACCORD	
AMPLES TYPES AND ACCOUNT.	
SAMPLES TYPES ANSACCOS	
SAMPLES TYPES AND ACCORD	
SAME ET TYPES ANSACOOD	
SAME ET TYPES ANSACOOD	
SAMPLES TYPES AVEACOOD	
PAMPI ST TYPES AND ACCORD	
SAMPLES TYPES: (WSACODE) SAMPLE METHODS: (WSMCODE)	
D - DUPLICATE FB - FIELD BLANK G - GRAB : SP - SUBMERSIBLE R - REPLICATE TB - TRIP BLANK B - BALER AL - AIR-LIFT SAME	

N - NORMAL $_{D=11}$ SL - SUCTION LIFT PUMP

PAGE 1 OF 2

TIAL (GROUNDY IG PERIO	WATER DEPT D: START	PLEID TH (FT)	2696 M	COLOGGE	T.D.= 37.3' BTL (SOUNDER 5.27 pp 1= 3 wested cas DMPLETE 1025 R CODE 140 N
NAL PA	RAMETER	MEASUREME				DETEI LIN
EDOX I EMPER LKALIN Pa	PETENTIAL OF HYDROGEN ECIFIC CONDUCTANCE DOX POTENTIAL EMPERATURE LKALINITY (CACO ₃) PHEN. ALK = 0 TOTAL UNFILTERED ALK = 44		E: T: A	SC µmhos/cm Eh mvoits TEMP °C ALK mg/l		1510 10 10 10 10 10 10 10 10 10
TIME	TOTAL WITH	VOLUME DRAWN	рH	SC TEMP		COMMENTS
1251	(GALS)	C. O	-	-	-	START PUMPING
			4.78	332	19.5°F	ALMOST CLEAR SLIGHTLY
	1.0	ł	10.77			
0955				795	67.2"F	
0959	1.0 2.0 3.5	+	681	795 802	69.2°F	"
1955 1959 1905	2.0 3.5		6.80	802	69.5° F	"
0959	2.0		681	802 9,64	69.5° F	"
1955 1959 1005 10045	2.0 3.5 5.0		681 683	802 9,64	69.5° F	11 11
1955 1959 1005 10045	2.0 3.5 5.0		681 683	802 9,64	69.5° F	11 11

PAGE 1 OF 2

NITIAL AMPLIN	GROUNDW IG PERIOD IG METHO	ATER DEPT	TH (FT) 0944	2430 BTC	CI	SAMPLE DEPTH (FT.) 24 0. = 335, BTC (Survoto) 4.12.0.17=1.55.3== OMPLETE 1013 R CODE		
RESERV	ATION MET	HOO_4"6	AT L	ATEL DATE				
INAL PA	RAMETER	MEASUREME				/ 00	DETECT	
	OTENTIAL OF HYDROGEN PECIFIC CONDUCTANCE			H S.U. C umhc	s/cm	6.9B 845	0.01	
	EDOX POTENTIAL			h mvoi				
EMPERATURE				EMP •C			0.1	
	LKALINITY (CaCO3) PHEN. ALK = 0			LK mg/i				
TIME	TOTAL VOLUME			SC T	TEMP	ALIC = 358 MA/L COMMENTS		
-		Bore Volumes	 - '	i limina es e mis [[a []]				
0925	0.0	0.0	-	-	-	START PUMPIN	IG	
0427	1.0		6.92	826	680°F	ALMOST CLEAR, SUCH	24 CLO	
0933	2.0		6.92	843	68°F	LT. Blank, SLIGHTLY	THASI	
0935	3.0		6.94	842	60.00	: //		
0937	3.5		6.97	841	67.5%	"		
0938	4.0	<u>. </u>	6.97	842	675%	"		
0943	5.0		6.98	845	67.5°A	"		
			+					
	_							
	TYPES: (WSAC	DDE, FB - FIELD BL		SAMPLE METHO	MSW) :ECK	CODE) SP - SUBMERSIBLE		

64 275

PAGE 1 OF 2

TIAL	GROUND	WATER DEPT	H (FT)	17.72	370	SAMPLE DEPTH (FT.) TD= 3-0'BTC 3.20-0.17=Z26-3=67
MPLII B COI ESERV	NG METH	OD	400,	- METALS	LOGGE:	R CODE RADY SENT 4-27-90
TENT ECIFI DOX MPER	IAL OF P C CONDI POTENTI ATURE NITY (CA	CO ₃)	P ⁽ S)	h mvol EMP °C LK mg/l		6.99 0.0 878 1
IME	TOTAL	VOLUME DRAWN Bore Volumes	рН		TEMP	COMMENTS
1/35	0.0	0.0	-	-	-	START PUMPING
039	1.0		6.87	852	66.00	ALMUST CLEAR
1941	2.0		6.96	882	66.0°F	", ROOTLETS
-	3.5		6.77	885	65.5°A	"
044	4.5		6.98	884	66.0 A	" , ROOTLETS IN WAT
044			6.77	877	65.50	ALMUST CLEAR
	6.0		1	878	45.5%	" , ROOTLETS
045	7.0		699	070		
047	_		6.59			

PP - PERISTALIC PUMP

NORMAL $_{D=14}$ SL - SUCTION LIFT PUMP

LB - LAB BLANK

MPLIN MPLIN B COD ESERV	g perior g metho	THOO 400	1427		CO Logge	7.55 BFC (SULA DED); 10.3: 0.17= 1.75:3=5.25 ggs. to 7 DMPLETE 1543 R CODE 11ADN SENT 4-25-90	
PECIFIC EDOX F EMPERA LKALIN	AL OF HE CONDUCTION OF THE CON	30 ₃)	pi SC EI TE	D µmho n mvo!! EMP °C LK mg/I	t s	6.89 0.0 1250 1	
TOT			pH (umhos/cm) (°C)		TEMP.	COMMENTS	
1409	(GALS)	D. O	-	-	-	START PUMPING	
1411	1.0		6.70	1645	6950	DK. BROWN VERY TURBIO	
1414	2.5		6.78	1629	69.5%	"	
1416	3.5		4.82	1605	450	"	
1418	4.5		685	1520	625°A	. //	
1420	5.0	1.	686	1440		MED. BROWN, MOD. TO VERY	
1423	6.0		6.86	1360	69.5%		
1425	7.0		6.87	1320	69.5%		
1427	8.0		688		6957	"	
1428	9.0		6.89	1250	69.5"7	<i>ν</i> .	
SAMPLES	TYPES: (WSA	COOR) FB - FIELD St.		SAMPLE METHO	DDS: (WSM	CODE) SP - SUBMERSIBLE PUMP	

N - NORMAL D-15 SL - SUCTION LIFT PUMP

K - KNOWN

64 277

GROUND WATER QUALITY SAMPLING RECORD

PAGE 1 OF 2

						SAMPLE DEPTH (FT.) 22.70	
MPLIN MPLIN	NG PERIO	DE START	<u> 1303</u>		C: Logge Date	30.1' Bic (Swade) 7.4.0.17 = 1.26.3 = 3.78 OMPLETE 13/9 R CODE <u>RADN</u> SENT <u>7-25-90</u>	
ESERV	ATION ME	THOO	HNO	03-METALS	<u> </u>		
ML PA	RAMETER	MEASUREME	NTS:			DET	
		IYDROGEN JCTANCE	pi Si		s/cm	1250	
	POTENTI.		E				
	ATURE		_	EMP °C			
TOM	NITY (CA EN. ALK = TL UMFILTE	COSI C THES ALK = 480		LK mg/l		ALN = 476 M/L	
IME		. VOLUME DRAWN	рН		TEMP.		
251	(GALS) 0.0	Bore Volumes	-	_	-	START PUMPING	
<u> 25/ 1</u>	1.0		6.55	1250	IG° F	ALMOST CLEAR, PINK TINE	
754	2.0		659	1260	68.5F		
754 756	2.0		10	1254	68°F	"	
256	3.0	<u> </u>	6.63	1637			
$\overline{}$			6.63	2.1	-	"	
25.Y	3.0			2.1	-	11	
25.Y	3.0			2.1	-		
25.Y	3.0			2.1	-		

NORMAL D-16 SL - SUCTION LIFT PUMP

PAGE 1 878

AMPLE '	TYPE	N SAA	APLE ID			SAMPLE DEPTH (FT.) 2.98 (3)
-						
NITIAL	GROUND	WATER DEPT	H (FT	1 8.98	BTC	1.87-898=384 x 0.17=0
A MPLI	NG PERIO	D: START— OD———	1/35	5	0	COMPLETE
AB CO	DE KA	00 <u></u>			LOGGE	SENT 4/18/91
RESER	VATION ME	THOO 4°C	400	5-METALS		SENT 4/18/90
	ന്ട					
INAL P	ARAMETER	MEASUREME	 NTS:			DETECTION
OTENT	IAL OF H	HYDROGEN	n	H S.U.		<u>6.63</u> <u>0.0</u>
	=	JCTANCE	•		s/cm	410
REDOX	POTENTI	AL	Ε	h mvol	ts	
	RATURE			EMP °C		
Phenopth	NITY (CA) alein (P) All Kalindi, Un-	colonity = 0.0 mg filtered 1.212	/L	LK mg/l Filtered =		3/L
TIME		VOLUME	рН	SC TE		COMMENTS
	(GALS)	+			1 67	
0840	0.0	0.0	-	-	-	START PUMPING
	1.0	1.50	6.54	980	61°F	Lt. orange - ten mad turbi
0845						
0845	2.0	3.03	6.61	960	615	"
-		3.03	6.61	960 960	61.5	"
0848	20					"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55				"
0848	2.0	4.55 5.30	6.63		61.5	End purge.

D-17

€4 279

_	_	_	_				
,	A	G	F	1	n	F	-

SAMPLE TO THE SAMPLE SAMPLE	NG PERIO NG METHO DE <u>Ao</u> VATION ME	NATER DEPT D: START THOO	IPLE ID H (FT 15/3	LOT C	ONTROL	SAMPLE DE 23.7 BTC OMPLETE R CODE	23.7-16 5.49 x 00 1600 RADU	B21 BTC B-Z1 = 5.44 F = 0.93 x 3
POTENT SPECIF REDOX TEMPES ALKALI Thens pt	FIAL OF HIC CONDU POTENTIA RATURE NITY (Ca)	MEASUREME! IYDROGEN ICTANCE AL CO3)	NTS: P S E T	th mvo EMP °C LK mg/	os/em lts	6.4 92. 18.	2	DETECTION LIMIT (P. O.)
Total of	TOTAL	VOLUME DRAWN CASING		SC (umhos/cm)	TEMP.		MMENTS	
	(GALS) 0.0	0.0	-	-	-	STAF	RT PUMPII	NG
14.58	1.0	1.07	6.48	960	18.5		Ivery tor	
1502	5.0	2.14	6.56	900	18.5	11	**	5.0(
1506	3.0	3.21	6.44	970	18.5	11	ı	
1511	4.0	4.29	6.46	922	18.5	V E	11	
_	S TYPES: (WSA	_	MIM'	SAMPLE METH	•	-•	011014E30101 =	
R - R S - S	PIKE	TB - TRIP BLAN	K C	B - BAILER PP - PERIST. SL - SUCTIO	ALIC PUMI	AL -	SUBMERSIBLE AIR-LIFT SAM BLADDER PUI	PLER

FAGE 1 OF 2

	TYPE	N SAM				NO
AMPLI AMPL	ING PERIO	WATER DEPT DD: START	<u> 7350</u>		C	R CODE RADN
reser Omme	IVATION ME NTS	THOO_4°C,	HWD,	(PH < 2)	WITH	SENT 4/17/90 METALS
NAL P		FINAL GW. DER R MEASUREME!		2.88 BTC		DETECTION
OTEN	TIAL OF	HYDROGEN	pł	ı s.u.		6.84 0.0
	IC CONDU		SC µmhos/cm			<u>830</u> /
	POTENTI.	AL	E	n mvol EMP °C	ts	18.6 0.1
	RATURE INITY (CA	COa)		LK mg/i		
	PHENUPHTH	CO3) +CEN = 0.0		•	_	110
		75 Mg/L (NON-1	FILTER	Ey) F	INTERES	1 = 376 419/L
TIME	WITH	DRAWN	рН	SC (umbos/cm)	TEMP.	COMMENTS
13/19	(GALS) 0.0	0. 0	-		-	START PUMPING
1327	1.5	1.29	6.70	850	18.7	- ORANGE/DRUNN, MOD VELY
1331	7.5	2.15	6.84	8340	185	orance Brown MOD TURBIC
1335	4.0	3.45	6.84	830	18.6	"
1340		3.88	-			"
						-
	 					
					1	
					+ -	•
	 			<u>_</u>		
	<u> </u>		<u> </u>	SAMPLE METH	208: 445:	2005
SAMP	TYPES MAR				NCM) CUL	
	ES TYPES: (WSA DUPLICATE	FB - FIELD BLAN		G - GRAB		SP - SUBMERSIBLE PUMP
D - R -	DUPLICATE REPLICATE		NK K			AL - AIR-LIFT SAMPLER

PAGE 1 OF 2

amplii Amplii Ab co Reser\	GROUND NG PERIC NG METH	WATER DEPT DD: START HOD HADN ETHOD_400	H (FT)	22.38	<i>BTC</i> C	T.D. = 30.52'BTC (SOUNDS) 4.15qq1 = 3 werted St. OMPLETE 1113 R CODE RADU SENT 57-90
OTENT PECIFI EDOX EMPER	TIAL OF I IC CONDI POTENTI RATURE NITY (CA EN. ALK =	CO3)	pi Si E Ti	h mvol EMP °C LK mg/l		6.73 C.C. 886 1
TIME	TOTAL VOLUME WITHDRAWN		- 348 рН	SC (umhos/cm)	TEMP.	COMMENTS
2.50	(GALS) 0.0	Bore Volumes			-	START PUMPING
1350 1352	1.0	 ""	130	Befet		
	2.0		6.76	8.99		DRANGE BROWN MOD. TURBIL
1255			6.73		66.0°F	DRANK /3 DOWN. SLIGHTLY - MOD
1355	20	1				
1357	3.0		124	893	1.600	Six current trase of
1357 1359	4.0		6.74			SINGST CIFAR
1357		<u> </u>	6.74	893 886		SLIEHTLY TURGIO ALMOST CLEAR
1357 1359	4.0		1			
1357 1359	4.0		1			
1357 1359	4.0		1			

N - NORMAL $_{\mathrm{D}^{-20}}$ SL - SUCTION LIFT PUMP

K - KNOWN

PAGE 1 OF 2

		05-513						
	_					SAMPLE DEPTH (FT.) 310 BTC		
	GROUNDY	MATER REPT	M (ET	3.10' BT	TC 7	1.0. = 12.65 BTC (SOUNDED) 4.87 gal to purge		
AMPLIN	IG PERIO	D: STARI	1317	-				
AMPLIN	IG METH	0D 3			LOGGE	R CODE		
AB CO	DE/(A	THOO YOU	. <i>i</i>	'n Arm				
RESERV	ATION ME	THOO GOVE	ANDIN	UN WELL	<u>، د</u>			
OMMEN	15		TITE U					
INAL BA	DAMETER	MEASUREME	vite.			DETEC		
						6.83 O.C.		
		YDROGEN	pH S.U. SC umhos/cm			974		
	POTENTI/	ICTANCE	5 E	_				
EMPER		••	_	EMP °C	••	<i>D</i> .		
	WTY (Ca	CO3).		LK mg/l	•			
Phen All	r=0.0 k = 504	Filtered	= 50	2				
		VOLUME		SC	TEMP			
TIME		HDRAWN	pН	(mmhos/cm)		T COMMENIS		
1202	(GALS)	Bore Volumes	_		-	START PUMPING		
1307	1.0	+	6.79	969	المام ا	ALMOST CIENC		
	2.5		6.80	967	660°A			
1311	35	 	6.79	975	65.5°A			
			_					
1315	<u> </u>		6.83	77-7	(25.) A	Science / Wile		
		 	 -					
+			 					
			1		1			
			 					
			-			· .		
			┼		 	· · · · · · · · · · · · · · · · · · ·		
- T		1	1	ļ	1			
								

N - NORMAL D-21 SL - SUCTION LIFT PUMP

PAGE 1 OF 2

MPLII MPLII MPLII B COI	GROUNDW	ATER DEP START_ D D	TH (FT)	9.45 8	CO LOGGER	AMPLE DEPTH (FT.) 9.45 D. = 20.41 ATC COURSED) S.5740/= 3 worked cos. MPLETE /S20 CODE RADIN ENT S-1-90	
TENT ECIFI DOX MPER KALII	RAMETER I	rdrogen Stance L	pi Si Ei Ti	C µmhq h mvoi EMP °C LK mg/I		6.52 1173	
		FILTERISH ALIC = !	599	SC	F-11-acd	597	
ME	WITHD	DRAWN	рн	(umhos/cm)	TEMP.	COMMENTS	
1-1	(GALS) 0.0	O. O	-			START PUMPING	
156	2.0		6.48	1054	66 2:51	Tinkews SUGHTLY	
20	4. C		6.44	1150	6650	11	
125	5-0		6.60	1190		ALMUST MEML SLIEM	
14	5.5		6.77			"	
506	60		4.89		66.1%	//	
507	6.5		6.47			pet was wandering up	
509	7.0		6.52	1173	66.1°F	ALMOST CLEAR	
\neg							

N - NORMAL D-22 SL - SUCTION LIFT PUMP

PAGE 1 OF 2

	ATION METH	100 400		1	C	1.0. = 21.25 BTC Iso and ED
OTENTIA PECIFIC EDOX F EMPERA LKALIN Phen	AL OF HYD CONDUC POTENTIAL ATURE HTY (CACC A(F = 00	TANCE	pi Si E Ti	h mvoit EMP °C .LK mg/i		6.63 1155 0.63
TIME	TOTAL V	OLUME	рН	-	TEMP.	COMMENTS
0976	0.0	0.0	-	-	-	START PUMPING
0428	1.5		6.59	1145	6.5.0°	LT. BROWN, SLIETTLY TUR
0433	3.0		6.68	1/51	65.5%	"
0136	4.5		6.63	1166	65.6°	
0938	6.0	·	663	1155	65.8°A	
		\				

N - NORMAL D-23 SL - SUCTION LIFT PUMP

PAGE 1 OF 2

	IG METHO DE <u>RAZ</u> TATION MET	START_	<u> 1124</u> 5		C: Logge Date	1.0. = 36 20 OTE (SOUNDEN) 4.9-1901 = 3 NOTE OF COST TRICODE RAD N SENT 5-1-90
NAL PA		CTANCE	NTS: pi Si E	C umho	s/cm	6.77 0. 802
PHE	HTY (CAC	O3) O.O ENED ALK		EMP °C LX mg/1 7.		FILTERED ACK = 356
TIME	TOTAL WITHD	TOTAL VOLUME WITHDRAWN	рН	SC	TEMP.	COMMENTS
1115	(GALS)	Q. O	-	-	-	START PUMPING
1119	1.0		6.75	FIVE	67.97	DRANKE/BROWN VERY TH
1/21	2.5		6.76	800	67.7A	
112.3	3.0		6.80	801	671°A	"
1125	4.0		6.79	801	67.6°A	<i>i1</i>
1127	5.0		6.77	BOZ	67.8°F	il .
						•
	TYPES: (WSAC	COE) F8 - FRELD BLA		SAMPLE METHO	DDS: (WSM	CODE) SP - SUBMERSIBLE PUMP

- 64 286 PAGE 1 OF 2

ITIAL MPLII MPLII MPLII	GROUND' NG PERIO NG METH DE	WATER DEPT	H (FT) 1406	22.76 B	TC CI	T.O. = 30.40 BTC (SOMOED) 17.04 0.13=2.59; 7.34. DMPLETE 1445 R CODE RADIN BENT 4-76-90	g=7.17
OTENI PECIFI EDOX EMPEF LKALI PHEN	TIAL OF PIC CONDUCTION OF POTENTIAL RATURE NITY (Ca		PI Si E TI	h mvoi EMP °C LK mg/i		6.89	UMI U.U.
TIME	TOTAL WITH	. VOLUME DRAWN	pН		TEMP.	COMMENTS	<u> </u>
1345	(GALS) 0.0	Bore Volumesi	-	-	-	START PUMPING	
13416	1.0	 	685	705	6B.07	LIGHT DEANGE / CHOWN MOD. T.	WRF113
1352	2.0		6.87	B73	68.0°=	" Scienty	
1354	3.0		6.89	910	C8.0%=	./	_
1356	4.0		6.90		67.50=	,,	
, , ,	5.0	1.	687	928	68.0°F	"	
1358			6.50	923	68°F	17	
	6.0		10.00	, , , , , , , , , , , , , , , , , , , ,			
1358	6.0 7.5		6.69		68°F	"	
1358 1400		EQU	6.69		\leftarrow		
1358 1400		EQU	6.69	129 T BLAUK	\leftarrow	CLEAR	

LB - LAB BLANK PP - PERISTALIC PUMP BP - BLADDER PUMP

N - NORMAL D-25 SL - SUCTION LIFT PUMP

S - SPIKE K - KNOWN

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PAGE 1 OF 2

CATIO		6 LF05-	5 <i>G</i>	LOT C	ONTROL			
MPLE	TYPE	SAM	IPLE ID			SAMPLE DEPTH (FT.) 20.15 (
MPLI MPLI B CC	GROUND WING PERIOD NG METHO DDE / AD VATION MET	W	IDLL		LOGGE	T.D. = 30.3 : 30.3 - 20.15 = 10.15 1615 × 0.17 = 1.73 g/m OMPLETE		
NAL P	TIAL OF H	MEASUREME!	P	H S.U.		b. 67 0.0		
EDOX Empei	IC CONDU POTENTIA RATURE	L	SC µmhos/cm Eh mvoits TEMP °C ALK mg/l		its			
PILLE	NITY (CAC CLPNTHALEN CATELEN TO	ALKALINITY = TAL ALK. = 4	0			FILTERED = 405 mg/L		
TIME	TOTAL	VOLUME	рH	SC (umhos/cm	TEMP.	COMMENTS		
22.00	(GALS)	O. O	_		-	START PUMPING		
1002	1.0	0.5%	6.43	960	65° F			
1005	2.5	1.45	6.50	980	65° F	1/		
1009	4.0	2.3/	663		65°F	LICHT TAN SLIGHTLY THE		
1015	5.0		6.67		645 A			
013	6.0	. 3.47				"		
	S TYPES: (WSAC	·		SAMPLE METH				
	UPLICATE IEPLICATE	TB - FIELD BLAN		G - GRAB B - BAILER		SP - SUBMERSIBLE PUMP AL - AIR-LIFT SAMPLER		
		LB - LAB BLAN				· · · · · · · · · · · · · · · · · · ·		

PAGE 1 OF 2

SAMPLE		N SAM	IPLE ID		<u> </u>	SAMPLE DEPTH (FT.)	
SAMPLI	GROUNDY NG PERIO NG MEIH	NATER DEPT D: START	H (FT 162	<u></u>	c	27.96 TD 713.04 3 NETTES CAS OMPLETE 1647 B CODE RADN	10.17 = 2.29 105 = 6.65 g
	DE <u>//AU</u>		,			R CODE <u>KAON</u> Sent <u>4/18/90</u>	
	ATION ME	1111	: H	UD3 IN M.	ETALS	(PHZZ)	
COMMEN							
FINAL P	RAMETER	MEASUREME	NTS:				DETECTIO
BOTENI		YDBOCEN		ш еп		6.40	UMIT <i>O. 01</i>
	IC CONDU	IYDROGEN ICTANCE	•	H S.U. C umbo	s/cm	1000	<u> </u>
	POTENTIA		_	h mvol			<u></u>
TEMPER			T	EMP °C			0.1
ALKALI	NITY (Cal	CO3)	ALK mg/I				
Unt.	Ippenale.n I Iterial To	414=0 +=1=395 mg/L	•	Filtered =	392 4	<u> </u>	
TIME	TOTAL	VOLUME DRAWN - Pains		SC	TEMP.	COMMENTS	<u> </u>
	(GALS)	Bere-Volumes					
1555	0.0	0.0	-		-	START PUMPI	NG
1600	2.0	0.91	6.20	1010	63.5	Fo light gray sligh	Hy Cloudy
1606	2.5	1.14	6.20	1010	63.5 °F	"	
1609	4.0	1.82	5.60	1010	64° F	Almost Year	
1611	5.0	2.27	6.30	990	635°	"	
1614	6.0	2.73	6.45	1010	63.5°		
1616	7.0	318	640	1000	6350	44	
	7.5	3.41	1-		-	End purge-	
1618	· ·					1-1	
1618		-					
1618		į.	1				
1618							
1618	.00						

LB - LAB BLANK PP - PERISTALIC PUMP BP - BLADDER PUMP

N - NORMAL D-27 SL - SUCTION LIFT PUMP

K - KNOWN

PAGE 1 OF 2

MPLET	YPE		MPLE ID	 _		SAMPLE DEPTH (FT.) BAB A = 17.08'BTC (SOMNED) 4.44 gm to purge
MPLIN MPLIN MB COI MESERV	G PERIC	DE START BOOK BOOK BOOK BOOK BOOK BOOK BOOK BOO	1102		C: Logge	R CODE RAON SENT 5-11-90
•		R MEASUREME				7.05 DETI
_	_	HYDROGEN JCTANCE	•	H S.U. С µmhc	s/cm	779
	POTENTI	AL	E		ts	
-	ATURE UTY (Ca	CO ₃)	TEMP °C Alk mg/l			
		let thispa Filte		_		· ·
TIME	TOTAL	. VOLUME DRAWN	рН	SC	TEMP.	COMMENTS
10.40	(GALS)	Bore Volume	5 1	-	_	START PUMPING
1044	1.0	0.0	7.07	723		LI. BROWN, SLIENTLY TUR
1054	2.5		7.04	762	65.5°F	
1057	35	 	7.07	756	155°A	
1059	5.0		7.05	4	65.3°A	
1101	5.5		7.05		655°A	
						· · · · · · · · · · · · · · · · · · ·
				<u>!</u>		C005.↑

PAGE 1 OF 2

CATION		CSNI LOG				_	
AMPLE T	YPE	SAN	IPLE ID			SAMPLE DEPTH (FT.) 734 OTC	
UTIAL	GROUND	WATER DEPT	H (FT	7.34 B	TC 7	D= 17.18'8Te (SOUNDED) 5.02 gal to purye	
AMPLIN	IG PERIC	D: START	1023		c	OMPLETE 1027	
AMPLIN	IG METH					R CODE ROOM	
	DE		· An	DI-MESTE	DATE	SENT	
	TS	•					
INAL PA	RAMETER	R MEASUREME	NTS:			DETECT	
OTENTIAL OF HYDROGEN PECIFIC CONDUCTANCE EDOX POTENTIAL				u e 11		<u>6.78</u> 0.01	
			pH S.U. SC umhos/			1237	
			SC µmhos/cm Eh mvoits				
EMPER	ATURE		TEMP °C				
	NITY (CA	CO ₃)	ALK mg/l				
Phen Al NFILTERE	U ALK = N	OT TAKEN	•	Fil	TERE	D ALK = 562 mg/L	
TIME	TOTAL	VOLUME DRAWN	рН	SC	lieurd	COMMENTS	
	(GALS)		_				
1012	0.0	0.0	1/34	11.11.1	سرن مر	START PUMPING	
1014	1.0		675	1144		LT. BADUN, SLIENTLY TUP	
1017	2.5		6.80		65.6°A		
1019	4.0		6.78		653°F		
1021	5.5		6.78	1237	65.2 A	<u>"</u>	
			<u> </u>				
			ļ				
			<u> </u>				
						<u> </u>	
				_	1		
SAMPLE	TYPES: (WS.	ACODE)	1	SAMPLE METHO	DOS: (WSM	ICODE)	
D - D	UPLICATE	FB - FFELD BLA	INK	G - GRAB '		SP - SUBMERSIBLE PUMP	
R - R	EPLICATE	TE - TRIP BLAS	₩.	B - BAILER		AL - AIR-LIFT SAMPLER	
	PIKE	LB - LAB BLAN		PP - PERISTA		BP - BLADDER PUMP	

PAGE 1 OF 2

1007	YPE	SA	MPLE ID _		\$	NO SAMPLE DEPTH (FT.) <u>15.17 </u>	
TIAL	GROUNDW	ATER DEP	TH (FT) .	15.17' 3	7.0. = 2.	7.4 BTC (SULVACE) 6.49 gal = 3 WOTTED COS DMPLETE 1043	
MPLIN	IG METHO	D <u> </u>			LOGGEF	R CODE	
			· Anon-	METALL	HAL -	DET. H. C.	
	RAMETER I		ENTS:			DETEC	
				6.11			
OTENTIAL OF HYDROGEN PECIFIC CONDUCTANCE EDOX POTENTIAL			pn SC	S.U. umho		574 1	
			Eh				
	ATURE			MP °C			
LKALII <i>Phe</i>	MTY (CAC)	03)	AL	K mg/i	•		
TUT.	AL UNFILTER	ED ALK = 2	293	Tot	AL FILI	TELES ALK = 286	
TIME	WITHD	RAWN		SC umhos/em)	TEMP.	COMMENTS	
	(GALS)	Bore Volume	- 1	_	-	START PUMPING	
11:13	/ 2?		7.00	63B	700 F		
1020	2.0		7.00	5B1	-	SLIGHTY CLOUDY	
1074	3.5		7.09	580	655%		
	5.5		7.09	578	65.5A		
	7.0	<u> </u>	7.10	579	155 F	"	
1016	$\mathcal{T}\cup\mathcal{T}$		17 . / / / 1		r/- / 1		
	7.0		7.10				
1016	F- U		7.112	37/		· · · · · · · · · · · · · · · · · · ·	
1016	7-17		1.10	37/			
1016	7-0		1.10	37/			
1016	7-0		11.10	37/			
1016	7-0		1.10	37/			
1016	7-0		1.10	37/			

NORMAL $_{D=30}$ SL - SUCTION LIFT PUMP

KNOWN

N -

PAGE 1 OF 2

MPLIN MPLIN MB COI MESERV	IG PERIO	ID: START IOD _/2 -ON THOO _4°C'	.//35		CO Loggei	DETROLEMAN HYDRO	
OTENT PECIFI EDOX EMPER LKALII	IAL OF I C CONDI POTENTI ATURE NITY (CA FEN. ALK. OTAL: UN	CO3) = 00 FILTERED ALK	pi Si E TI	C µmho h mvo! EMP °C LK mg/l	•	6.77 322 FILTERED ALK =	DETECTI LIMIT 17.01 1
	IOIAL	. VOLUME		SC	TEMP	COMMENTS	
TIME	(GALS)	Bore Volumesi	рH	(umhos/cm)	(°.C)	COMMENTS	
TIME ///9			р Н -	(umhos/cm)	- (•.c)	START PUMP	
	(GALS)	Bore Volumesi	рн - 6.67	-	(°°C) - 69.5°F		
1119	(GALS)	Bore Volumesi	-	833	-	START PUMP	
1119	(GAL8) 0.0 0.5	Bore Volumesi	- 6.67	833	- 69.87	START PUMPI	
119 1121 125	(GALS) 0.0 0.5 7.5	Bore Volumesi	- 6.67 6.69	- 833 829 827	- 695°F 695°F	START PUMPI	
1119 1121 1125 1127	1GAL8) 0.0 0.5 1.5 2.5 3.0 4.0	Bore Volumesi	6.67 6.69 670	833 829 827 827 824	69.5°F 69.5°F 69.5°F 69.5°F	START PUMPS	
1119 1121 1125 1127 1129	(GAL8) 0.0 0.5 7.5 2.5 3.0	Bore Volumesi	6.67 6.69 670 673	833 829 827 827 827	69.5°F 69.5°F 69.5°F 69.5°F	START PUMPS	
1119 1121 1125 1127 1129 1132	1GAL8) 0.0 0.5 1.5 2.5 3.0 4.0	Bore Volumesi	6.67 6.69 670 673 6.72	833 829 827 827 827	69.5°F 69.5°F 69.5°F 69.5°F	START PUMPS	
1119 1121 1125 1127 1129 1132	1GAL8) 0.0 0.5 1.5 2.5 3.0 4.0	Bore Volumesi	6.67 6.69 670 673 6.72	833 829 827 827 827	69.5°F 69.5°F 69.5°F 69.5°F	START PUMPS	
1119 1121 1125 1127 1129 1132	1GAL8) 0.0 0.5 1.5 2.5 3.0 4.0	Bore Volumesi	6.67 6.69 670 673 6.72	833 829 827 827 827 824	69.5°F 69.5°F 69.5°F 69.5°F	START PUMPS	

PP - PERISTALIC PUMP

N - NORMAL D-31 SL - SUCTION LIFT PUMP

KNOWN

BP - BLADDER PUMP

PAGE 1 OF 2

MPLE	TYPE N					NO
_	··· ·					·
TIAL	GROUND	WATER DEPT	H (FT	130.04 B	re	40.00 (Santes); 5.03 gol
MPLII	NG PERIC	DD: START	<u> </u>			OMPLETE 14/19
B CO	DE RA	ov			DATE	SENT 4-30-90
ESER	ATION ME	THOO 401	HO	1-METALS	Her.	- PET. ILC-
	rrs		_	·		
			_			nctra
WL P	ARAMETE	R MEASUREME	NTS:			DETEC
TENT	TAL OF	HYDROGEN	P	H S.U.		6.52
		UCTANCE	_	•	s/cm	<i>1</i> 50 /
_	POTENTI	AL	_	h mvol	ts	
	IATURE	CO - 1		EMP °C		
PHE	nity (Ca v. ali(=	00		•		1.50
TOTO	n unfic	TENEY ALK =	622		TOTAL	FILTERES ALL = 458
	TOTAL VOLUME WITHDRAWN				_	
TIME		DRAWN	→ `	SC	TEMP.	COMMENTS
	WITH (GALS)	Bore Volumes		(umhos/cm)	(°.C)	COMMENTS
1326	(GALS) 0.0	DRAWN	-	(umhos/cm)	- (•.C)	START PUMPING
1326	(GALS) 0.0 /. 0	Bore Volumes	- 6.Sb	(umhos/cm) - 9/3	(°C) - th.oF	START PUMPING LT BROWN FROM SLIEHTLY
1326 1331 1376	WITH (GALS) 0.0 1.0 2.5	Bore Volumes	- 6.56 6.59	(umhos/cm) - 9/3 878	(°C) - <i>th.oʻF</i> 68.2 F	START PUMPING LT BROWN ENRY SLIENTLY
1326 1331 1376 1342	WITH (GAL8) 0.0 /.0 2.5 3 ()	Bore Volumes	- 656 659	(umhos/cm) - 9/3 878 880	1°C) - - 	START PUMPING LT BROWN FROM SLIEHTLY
1326 1331 1376 1342	WITH (GALS) 0.0 1.0 2.5	Bore Volumes	- 6.59 6.51 6.51	(4mhos/cm) - 9/3 8:78 880 868	1°C) - - 	START PUMPING LT BROWN ENTRY "" ""
1326 1331 1376 1342 1345	WITH (GAL8) 0.0 /.0 2.5 3 ()	Bore Volumes	- 656 659 651 651	(4mhos/cm) - 9/3 878 880 868 847	1°C) - - 	START PUMPING LT BROWN ENMY SLIENTLY
1326 1331 1326 1342 345 350	WITH (GALS) 0.0 1.0 2.5 3.0 4.0	Bore Volumes	- 6.59 6.51 6.51	913 878 880 868 847 860	1°C) - - 	START PUMPING LT BROWN ENTRY "" ""
1326 1331 1376 1342 1345 1350 352	WITH (GALS) 0.0 /.0 2.5 3.0 4.0 5.0	Bore Volumes	- 656 659 651 651	(4mhos/cm) - 9/3 878 880 868 847	1°C) - 	START PUMPING LT BROWN ENTRY "" ""
1326 1331 1376 1342 1345 1350 352	WITH (GALS) 0.0 /.0 2.5 3.0 4.0 5.0 6.0	Bore Volumes	- 6.59 6.51 6.51 6.52 6.49	913 878 880 868 847 860	(°C) - - 	START PUMPING LT BROWN ENTRY "" "" "" "" "" "" "" "" ""
1326 1326 1326 1342 1345 1350 352 354	WITH (GALS) 0.0 /.0 2.5 3.0 4.0 5.0 6.0	Bore Volumes	- 659 651 651 652 649 652	913 878 880 868 847 860 850	(°C) - - 	START PUMPING LT BROWN ENTRY "" "" "" "" "" "" "" "" ""
1326 1331 1376 1342 1345 1350 352	WITH (GALS) 0.0 /.0 2.5 3.0 4.0 5.0 6.0	DRAWN Bore Volumes 0.0	6.51 6.51 6.52 6.49 6.52	(umhos/cm) - 913 878 880 868 847 860 850	(°C) - - 	START PUMPING LT BROWN ENRY SLIEHTLY "" "" "" "" "" "" "" "" ""
1326 1331 1376 342 345 350 352	WITH (GALS) 0.0 /.0 2.5 3.0 4.0 5.0 6.0	DRAWN Bore Volumes 0.0	6.51 6.51 6.52 6.49 6.52 6.49	(umhos/cm) - 913 878 880 868 847 860 850	1°C)	START PUMPING LT BROWN ENRY SLIEHTLY "" "" "" "" "" "" "" "" ""

PP - PERISTALIC PUMP

N - NORMAL D-32 SL - SUCTION LIFT PUMP

BP - BLADDER PUMP

LB - LAB BLANK

KNOWN

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MPLIN MPLIN B COI ESERV	IG PERIO	DD	1537		CC	MPLETE 1602 REODE RADIN BENT L-PET: H.C.	,
OTENT PECIFIC EDOX EMPER LKALIN	IAL OF HE CONDUPOTENTIAL ATURE	\L 30₃) : ७0	pH SC EH TE	дтho mvo! MP °C LK mg/l		<u>6.76</u>	DETEC LIM U.
TIME	TOTAL	VOLUME DRAWN	pН	SC (umhos/cm)	TEMP.	COMMENTS	
1500	(GALS) 0.0	Bore Volumes	1 -		-	START PUMPIN	
1524	1.0		6.81	BOI	68.72	DRONGE/Brown MOD	
1527	2.0		7.04	812	67.87	11	. ,
1529	3.0		6.79		68.2°A	//	
1531	if.0		6.78		68.2°F	"	
1533	4.5		6.76	813	682°F	//	
						·	
		1	1 1		1 1		

N - NORMAL D-33 SL - SUCTION LIFT PUMP

KNOWN

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4PLII	GROUND	WATER DEPT	H (FT	29.42 AT	7.D. =	36.6.6 ETC (SOMULES) 4.71 gal = 3 method casing MPLETE 1020
	DE <u>KA</u> ATION ME		HNOZ	-NETALS;	DATE S	ENT 5-1-90 PETRULEUM HYDROCA
TENT ECIFI DOX MPER KALII PHE	TAL OF IC CONDITION OF THE POTENTI ATURE NITY (Ca. W. AUK =	CO ₃)	P S E TI	h mvol EMP °C LK mg/l		6.66 / 258
101	_	TELED ALK =	413	SC		EMES ALK. = 358
ME	WITH	DRAWN	рН	(umhos/cm)	TEMP (°C)	COMMENTS
	WITH (GALS)	DRAWN Bore Volumesi	pН		7	
1785	(GALS) 0.0	DRAWN	-	(umhos/cm)	- (°°C)	START PUMPING
	WITH (GALS)	DRAWN Bore Volumesi	- 673	(umnos/cm)	(°°C)	START PUMPING
131 E	(GALS) 0.0	DRAWN Bore Volumesi	-	14mnos/cm)	- (°°C)	START PUMPING
1215 131 134	WITH (GALS) 0.0 /.0 2.5	DRAWN Bore Volumesi	- 673 6.62	14mnos/cm)	(°C) - - - - - - - - - - - - - - - - - - -	START PUMPING SLEAR AGUST SLEAR VERY SLIGHT
920 931 934	WITH (GALS) 0.0 /.0 2.5 3.5	DRAWN Bore Volumesi	6.73 6.62 6.65	750 755 767 764	(°C) - - - - - - - - - - - - - - - - - - -	START PUMPING SLEAR AGUST CLEAR VERY SLIGHT
920 931 934 936	WITH (GALS) 0.0 1.0 2.5 3.5 4.0	DRAWN Bore Volumesi	6.73 6.62 6.65 6.60	750 755 767 764	(°C) - !B.0°F BB.2'F 6B.2°F	START PUMPING CLEAR FULLY CLEAR VERY SUGAT.
920 931 934 936	WITH (GALS) 0.0 1.0 2.5 3.5 4.0	DRAWN Bore Volumesi	6.73 6.62 6.65 6.60	750 755 767 764	(°C) - !B.0°F BB.2'F 6B.2°F	START PUMPING CLEAR FULLY CLEAR VERY SUGAT.

NORMAL D-34 SL - SUCTION LIFT PUMP

SPIKE

KNOWN

LAB BLANK

PAGE 1 OF 2

DCATION	ID WA	107-10A		LOT CO	ONTROL	LOG TIME
AMPLE T	YPE	SAI	MPLE ID			SAMPLE DEPTH (FT.) 25.91 BT
UTIAL	GROUNDY	VATER DEP	TH (FT	85.91	BTC	1.D. = 37.92 BTL (SOMDED)
AMPLIN	IG PERIO	D: START_	0859	<u> </u>	c	OMPLETE
AMPLIN	IG METH	OD <u>B</u>	_		LOGGE	R CODE _RAW
AB CO	DE <u> </u>	THOO 40C	· Main	-141-11	DATE	SENT <u>5-11-90</u>
	TS		, MIVO3	- MEINCS		
INAL PA	RAMETER	MEASUREME	ENTS:			DETECT
OTENT	IAL OF H	D	H S.U.		680 C.O.	
OTENTIAL OF HYDROGEN PECIFIC CONDUCTANCE EDOX POTENTIAL			S		s/cm	834
			E	h mvoi	ts	
TEMPER				EMP °C		<u> </u>
p	NITY (Ca(henoi Alk = 0.0 hal alk = i= 1	303) o taken filter	red = Da		•	
TIME		VOLUME	рН		TEMP.	COMMENTS
	(GALS)	Bore Volume				
0835	0.0	0.0	-	•	-	START PUMPING
0839	1.0		6.8%	792	68.0°	LT. TAV, SLIGHTLY TYKE
0945	7.5		6.79	833	6.8. OF	"
DEAB	4.0		6.83	835	67.B°	"
0853	5.0		6.84	840	67.8%	= 11
0857	6.5		6.80	47 -	68.07	
						·
SAMPLES	TYPES: (WSA	000E)	<u> </u>	SAMPLE METHO	NSW) :EQC	CODE)
	PUCATE	FB - FIELD BL		G - GRAB		SP - SUBMERSIBLE PUMP
R - RI	EPLICATE	TB - TROP BLA	NK	B - BALLER		AL - AIR-LIFT SAMPLER

N - NORMAL D-35 SL - SUCTION LIFT PUMP

KNOWN

64 297 PAGE & OF 2

AMPLE	TYPE	NP07-10B	APLE IC			SAMPLE DEPTH (FT.) 25.5 B
Uner Alk	: 500	Hered - 390		N.	4.28	5.5 BTU (USEA TAPE, E-
		-		. <i>T</i> .	0 = 34:	SS'BTC NOT WORKER
TIME		. VOLUME DRAWN	рН	SC	TEMP.	SS'BTC NOT WORKER AND PROSERVE PROSERVE COMMENTS
	(GALS)	Bore Volumes	<u> </u>			
512						SPART BAILING
1516	1.0		6.86	I		F ALMOST CLEAR
1519	2.0	1	6.87			LT. BROWN SCIEBELY TUR
1573	3.0		6.85	· · · · · · · · · · · · · · · · · · ·		. "
529	5.0	1	6.84	796	69.5%	=
	•		<u> </u>			
1532	- STAU	SAMPLIN	<u>k </u>			
(537	- END	SAMPING			<u> </u>	
				†		
-	. -		†	 		
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			<u> </u>	<u> </u>		
				⊥		
				D-36	1	

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PAGE 1 OF 2

LOÇATION	NID WA	107-10 es	.	LOT C	ONTROL	NOSAMPLE DEPTH (FT.) IB.30 STC
BAMPLII LAB CO PRESERV COMMEN	MG PERIOD MG METHO DE	DD	°C, 1		LOGGE	T.D. = 29.00 BTC (SOUNDED 5.46 gm = Punge 3 marted 1410) OMPLETE 1410 FR CODE RADN SENT 5-11-90 DETECTIO
POTENT SPECIFI REDOX TEMPER	TAL OF H C CONDU POTENTIA ATURE NITY (CAC	(C ₃)	pi Sc Ei TE	mvol EMP °C LK mg/l		6.68 0.01 9.39 /
TIME	TOTAL WITHD	VOLUME RAWN	рН	SC (umhos/cm)	TEMP.	COMMENTS
1348	0.0	0.0	-	-	-	START PUMPING
1351	1.0	40	6.70	953	69.0°	ALMOST CLEAR
1354	2.5		6.71	951	69.5°A	SLIEHTLY CLOVET
1357	3.5		6.73	949	69.8°A	
1400	5.0		6.68	939	69.80	
1407	5.5					END PURCE
						· ·
D - D	TYPES: (WSAC JPLICATE EPLICATE	DODE) FB - FRELD BLAI TB - TRIP BLAN LB - LAB BLANK	NK K	Sample Metho G - Grab B - Bailer	MSW) :2CIC	CODE) SP - SUBMERSIBLE PUMP AL - AIR-LIFT SAMPLER

N - NORMAL $_{D=37}$ SL - SUCTION LIFT PUMP

KNOWN

SURFACE WATER QUALITY SAMPLING RECORD

64 299

INSTALLATION ID SWL LOG LOCATION ID 1505-51			LOG TIME -08	
LOCATION ID LEGS - 01		LOT CONTROL	NO	
				FT.) D.S' BWS
SAMPLING PERIOD: START	1910	COMPLETE	0936	
SAMPLING METHOD		LOGGER CODE	RAON	
LAB CODE RAON		DATE SENT	5-8-90	
	HNOZ-1			
				DETECTION
PARAMETER MEASUREMENTS:	- 4.1		B.00	DETECTION LIMIT
POTENTIAL OF HYDROGEN	pН	S.U.	644	
SPECIFIC CONDUCTANCE	SC	µmhos/cm	<u> </u>	
REDOX POTENTIAL	Eh	mvoits		
TEMPERATURE	TEMP	•C		
ALKALINITY (CaCO3)	ALK	mg/i		
Phenolphthalein Alkalinity 00 Total Alkalinity = 295 M/L	Ellered -	210 Mg/L	TEMP = 68.2	?° F
	IPLE ID	LOT CONTROL	SAMPLE DEPTH (
SAMPLING PERIOD: START SAMPLING METHOD LAB CODE	IPLE ID	COMPLETE LOGGER CODE DATE SENT	NO SAMPLE DEPTH (
SAMPLING PERIOD: START SAMPLING METHOD LAB CODE	HNOZ-NIC	COMPLETE LOGGER CODE DATE SENT	NO SAMPLE DEPTH (
SAMPLING PERIOD: START SAMPLING METHOD LAB CODE PRESERVATION METHOD LAB CODE LAB COD	HNOZ-NIC	COMPLETE LOGGER CODE DATE SENT	NO SAMPLE DEPTH (FT.) O.S BWS DETECTION
SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADV PRESERVATION METHOD 4°C: COMMENTS WATER CLEAR PARAMETER MEASUREMENTS:	1PLE 1D	COMPLETE LOGGER CODE DATE SENT	NO	DETECTION
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE NATION METHOD COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN	PLE ID	COMPLETE LOGGER CODE DATE SENT	NO SAMPLE DEPTH (FT.) O.S BWS DETECTION
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD 4°C: COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE	PLE ID	COMPLETE LOGGER CODE DATE SENT S.U. µmhos/cm	NO	DETECTION LIMIT O.OI /
SAMPLE TYPE N SAM SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE NAON PRESERVATION METHOD 4°C COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL	PLE ID	COMPLETE LOGGER CODE DATE SENT S.U. µmhos/cm mvoits	NO	DETECTION LIMIT O.OI I
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD 4°C COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE	PLE ID	COMPLETE LOGGER CODE DATE SENT S.U. µmhos/cm mvoits °C	NO	DETECTION LIMIT 0.01
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE ROW PRESERVATION METHOD 4°C COMMENTS WATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃)	PLE ID	COMPLETE LOGGER CODE DATE SENT S.U. µmhos/cm mvoits	NO	DETECTION LIMIT P.OI O.1
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD 4°C COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE	PLE ID	COMPLETE LOGGER CODE DATE SENT S.U. µmhos/cm mvoits °C mg/l	NO	DETECTION LIMIT P.O/ / O./
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD CLEAR COMMENTS WATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) PHEN. ALK. = U TOTAL AMINTELES: 330 SAMPLE TYPES: (WSACODE)	PH SC Eh TEMP ALK	S.U. µmhos/cm mvoits °C mg/I TUTAL	NO	DETECTION LIMIT Q:0/ /- Q:/
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD 4°C CLEAR COMMENTS WATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (Cacoa) PHEN. ALK = U TOTAL AMUTELES: 330 SAMPLE TYPES: (WSACODE) D - DUPLICATE FB - FIELD BLAN	PLE ID	S.U. JIMhos/cm mvoits C mg/l TUTAL	NOSAMPLE DEPTH (1035 RAON 5-8-90 6.96 874 TEMP=66.29 FILTERES AU SP - SUBMI	DETECTION LIMIT O.1 FRIED MIG/L ERSIBLE PUMP
SAMPLE TYPE N SAM SAMPLING PERIOD: START SAMPLING METHOD LAB CODE NAON PRESERVATION METHOD CLEAR COMMENTS NATER CLEAR PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) PHEN. ALK. = U TOTAL AMFILTEMES: 330 SAMPLE TYPES: (WSACODE)	PH SC Eh TEMP ALK MG/L SAMPLE M K G - GR K B - BA	S.U. µmhos/cm mvoits °C mg/I TUTAL	NOSAMPLE DEPTH (1035 RADV 5-8-90 6.96 87.4 TEMP = 66.2: FILTERES AU DE) SP - SUBMI	DETECTION LIMIT P.O/ I O.1

_D-38

LOCATION ID LEUS-54		_ LOG TIME	
.	LOT CONTR	OL NO	
SAMPLE TYPE & SAMP	LE ID	SAMPLE DEPTH (FT.)	5 BNS
SAMPLING PERIOD: START	05 COMPLETE	1315	
SAMPLING METHOD	LOGGER CO	DE RADV	
LAB CODE RADN	DATE SENT	5-8-90	
- ::COC:: (**C:::OD	4NOZ-METALS	·	
COMMENTS POND NATER	 -		
PARAMETER MEASUREMENTS:		DE	TECTION
	-11	7.72	LIMIT
POTENTIAL OF HYDROGEN	pH S.U.	404	D.01
SPECIFIC CONDUCTANCE	SC µmhos/c	m <u></u>	
REDOX POTENTIAL	Eh mvoits		
TEMPERATURE	TEMP °C		0./
ALKALINITY (CaCO3) PHEN. ALK = 0.0	ALK mg/I	TEMP = 70.00E/	
TOTAL YNFILTELED ALL = 13/4	19/4 FILTELES AL	(= 112 Mg/L 75.0°F)	35 =)
	PLE ID	SAMPLE DEPTH (FT.)O	s bus
SAMPLING METHOD	40 COMPLETE LOGGER CO	1352	<u> </u>
SAMPLING METHOD LAB CODE AON PRESERVATION METHOD	40 COMPLETE LOGGER CO DATE SENT HNO3-METRIS	1352 DDE <u>RADN</u> 5-8-90	
PRESERVATION METHOD TONO - K	40 COMPLETE LOGGER CO	1352 DDE <u>RADN</u> 5-8-90	
SAMPLING METHOD LAB CODE 4000 PRESERVATION METHOD 4000	40 COMPLETE LOGGER CO DATE SENT HNO3-METRIS	1352 DDE <u>RADN</u> 5-8-90	
SAMPLING METHOD LAB CODE AON PRESERVATION METHOD YOU COMMENTS SMALL POND - N MUO	40 COMPLETE LOGGER CO DATE SENT HNO3-METRIS	1352 DDE RADN 5-8-90 OT IS WERT SOFT DE	BLACK TECTION
SAMPLING METHOD LAB CODE AON PRESERVATION METHOD YOU COMMENTS SMALL POND - N MUO PARAMETER MEASUREMENTS:	40 COMPLETE LOGGER CO DATE SENT HAVOZ - METALS BOTTOM SERIMEN	1352 DDE <u>RADN</u> 5-8-90 OT 15 NERT SOFT 15	BLACIC TECTION LIMIT
SAMPLING METHOD LAB CODE AON PRESERVATION METHOD YOU COMMENTS SMALL POND - R MUO PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN	40 COMPLETE LOGGER CO DATE SENT HNO3-METALS BOTTOM SEDIMEN PH S.U.	1352 DDE RADN 5-8-90 DE 15 VERT SOFT 15 7-53	BCACIC TECTION
SAMPLING METHOD LAB CODE PRESERVATION METHOD COMMENTS SMALL FOND PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE	40 COMPLETE LOGGER CO DATE SENT HAVOZ - METRIS BOTTOM SERIMEN PH S.U. SC µmhos/c	1352 DDE RADN 5-8-90 DE 15 VERT SOFT 15 7-53	BLACIC TECTION LIMIT
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL	PH S.U. SC umhos/c Eh myolts	1352 DDE RADN 5-8-90 DE 15 VERT SOFT 15 7-53	BLACIC TECTION LIMIT
SAMPLING METHOD LAB CODE PRESERVATION METHOD COMMENTS SMALL FOND PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE	PH S.U. SC umhos/c Eh mvoits TEMP °C	1352 DDE RADN 5-8-90 DE 15 VERT SOFT 15 7-53	BLACIC TECTION LIMIT
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃)	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l	1352 DDE RADN 5-8-90 DE TIS WERT SOFT I	BLACIC TECTION LIMIT
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) PJEN. ALK = 0.0	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l	1352 DDE RADN 5-8-90 DE TIS WERT SOFT I	BLACIC TECTION LIMIT
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃)	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l	1352 DDE RADN 5-8-90 DE 15 VERT SOFT 15 7-53	BLACIC TECTION LIMIT
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) PJEN. ALK = 0.0	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l	1352- DDE RADN 5-8-90 T IS VERY SOFT I DE 7.53 1075 TEMP=81.2°F TAL FILTERED = 435°	BLACIC TECTION LIMIT
SAMPLING METHOD LAB CODE PRESERVATION METHOD COMMENTS SMALL POND PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (Caco ₃) PIEN.	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l SAMPLE METHODS: (WSM	1352- DDE RADN 5-8-90 T IS VERY SOFT I DE 7.53 1075 TEMP=81.2°F TAL FILTERED = 435°	BLACIC TECTION LIMIT 19,0/
SAMPLING METHOD LAB CODE PRESERVATION METHOD COMMENTS SMALL POND - K MUO PARAMETER MEA SUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) PHEN. PIK = 0.0 TOTAL UNIFICTERED ALK = 43 SAMPLE TYPES: (WSACOOE) D - DUPLICATE FB - FIELD BLANK R - REPLICATE TB - TRIP BLANK	PH S.U. SC umhos/c Eh mvoits TEMP °C ALK mg/l SAMPLE METHODS: (WSM) G - GRAB B - BAILER	DE RADN S-B-90 T IS VERY SOFT D DE T-53 1075 TEMP=81.2°F TAL FILTERED = 435 ICODE) SP - SUBMERSIBLE PI AL - AIR-LIFT SAMPLE	TECTION LIMIT P. O/
SAMPLING METHOD LAB CODE PRESERVATION METHOD COMMENTS SMALL POND PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (Caco ₃) PIEN.	PH S.U. SC µmhos/c Eh mvoits TEMP °C ALK mg/l SAMPLE METHODS: (WSM	DE RADN S-B-90 DE TIS WERY SOFT R TEMP= B1.2° F THL FILTERED = 435° AL AIR-LIFT SAMPLE BP - BLADDER PUMP	TECTION LIMIT P. O/

SURFACE WATER QUALITY SAMPLING RECORD

64 301

INSTALLATION ID _ CSUL_ LOG E	ATE 5-8.	-90 LO	G TIME	55
LOCATION ID 1505-36	LO	T CONTROL NO)	
LOCATION ID SAME LOGIC LOCATION ID SAMPLE TYPE N SAMP	LE ID	SA	MPLE DEPTH (F	T.) <u>D.S BWS</u>
SAMPLING PERIOD: START - ///	//CO	MPLETE	1/13	
SAMPLING METHOD,	LO	GGER CODE _	RAON	
LAB CODE	DA	TE SENTS	-8-90	
SAMPLING METHOD GLAB CODE (ADN) PRESERVATION METHOD 4°C; A	WOZ-MET	4LS .		
COMMENTS WATER SLIGHTLY	CLUNOT E	REENISH T	TINT	
		_		
PARAMETER MEASUREMENTS:				DETECTION LIMIT
POTENTIAL OF HYDROGEN	pН	s.u.	B.03	0.01
SPECIFIC CONDUCTANCE	•	umhos/cm	648	
REDOX POTENTIAL		mvoits		
TEMPERATURE	TEMP			0:1
•	-	mg/l		
	44		TEMP= L9.10F	
PHEN = 0.0 HNFILTERED = 231 M	IL FILTE	260 ALK = 220	ng/L	
SAMPLING PERIOD: START 12. SAMPLING METHOD 12. LAB CODE 12. PRESERVATION METHOD 40. COMMENTS NATER SCIENTS	1002 - MET	GGER CODE	RAON	
PARAMETER MEASUREMENTS:				DETECTION LIMIT
POTENTIAL OF HYDROGEN	рH	S.U.	7.99	0-01
SPECIFIC CONDUCTANCE	• _	umhos/cm	629	
REDOX POTENTIAL		nvoits		
TEMPERATURE	TEMP	°C	<u> </u>	0.1
ALKALINITY (CaCO3)		mg/I		
PHEN. ALK = 0.0		- · · · · · · · · · · · · · · · · · · ·	TEUIP = 72.5	
UNFILTERED ALK = 222 MA/L				
122 12	FILTER	ed ALK=20	g ang/L	502
SAMPLE TYPES: (WSACODE)				504
	SAMPLE METH	HODS: (WSMCODE)		SIBLE PUMP
SAMPLE TYPES: (WSACODE)	SAMPLE METH	HODS: (WSMCODE)	SP - SUBMER	
SAMPLE TYPES: (WSACODE) D - DUPLICATE FB - FIELD BLANK	SAMPLE METH G - GRAB B - BAILER PP - PERIST	HODS: (WSMCODE)	SP - SUBMER	ISIBLE PUMP SAMPLER

SURFACE WATER QUALITY SAMPLING RECORD 64 302

LOCATION ID	LOT CONTROL NO SA	O	
SAMPLING PERIOD: START 142 SAMPLING METHOD LAB CODE RADN PRESERVATION METHOD 400; IN COMMENTS NATER CLONDY, IN PLACE UPSTREAM	LOGGER CODE _ DATE SENTS 4NO, -METALS	1445 1140N -8-90	5 TAKING
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CACO ₃) PHEN. ALK = 0.0 / 0.0 TOTAL UNIFILITEMED = 213/210	Dur = 8.11 p Dur = 612 ph S.U. SC jimhos/cm Eh mvolts TEMP °C ALK mg/I Total Filtered Alk	8.10 61B	DETECTION LIMIT O.01 1
LOCATION ID 3013-5/	LOGGER CODE DATE SENT	O	
PARAMETER MEASUREMENTS: POTENTIAL OF HYDROGEN SPECIFIC CONDUCTANCE REDOX POTENTIAL TEMPERATURE ALKALINITY (CaCO ₃) Presignifications alk = 0.0 Takel AK = 397 Filters = 377 SAMPLE TYPES: (WSACODE)	pH S.U. SC µmhos/cm Eh mvoits TEMP °C ALK mg/I Temp = 69.0° F SAMPLE METHODS: (WSMCODE)	<u>6.89</u> 759	DETECTION LIMIT D. 01 / O.1
D - DUPLICATE FB - FIELD BLANK R - REPLICATE TB - TRIP BLANK S - SPIKE LB - LAB BLANK K - KNOWN N - NORMAL	G - GRAB B - BAILER PP - PERISTALIC PUMP SL - SUCTION LIFT PUMP		

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APPENDIX E

Survey Data

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HYDROGEOLOGIC INVESTIGATION CARSWELL AIR FORCE BASE FORT WORTH, TEXAS

Texas State Plane Coordinate and Elevation of Test Wells Soil Gas Probes and Sampling Points

April 8, 1988



(Monitor wells are distinguished from boreholes by having a corresponding elevation of top of P.V.C. value)

NUME	ER	NORTH	EAST	ELEVATION OF	ELEVATION OF NATURAL
		**	"X"	TOP OF P.V.C.	GROUND AT WELL
ass	A(45)	402.068.84192	2,024,357.78905	566.38	566.9
ಹುತ	8(34)	402.390.17981	2,024,331.93158	569.73	567.1
ಹಿತ	C(36)	402,254.07567	2.024.565.70484	559.57	560.0
ಹು	0(38)	402,418.08908	2,024,487.37097	561.45	200.0
മാ	ו פכוט	402,410.00500	2,024,407.57057	301.43	
PΙ	(111)	397,712.30601	2,019,695.14307	*628.5 8	625.5
		397,542.85438	2,020,627.90845	•618.78	615.5
PZ	(96)	397,342.63436	2,020,027.70047	-010.70	615.5
	(1711	ACT 089 90010	2,025,128.18992	570.27	566.5
1A	(131)	401,089.90010	2,025,291.18966	560.2 5	560.49 (ASP)
18	(132)	401,268.84868	2,025,482.01757	560.00	560.31 (ASP)
10	(134)				
10	(137)	-	2,025,642.78693	563.93 563.35	560.5
ΙE	(135)	401,173.20809	2,025,407.532 05	562.25	559.4
1 F	(136)	401,002.55061	2,025,607.46316	562.26	559.5
			- 017 707 70707		433 43
3A	(121)	398,360.53325	2,017,786.72397		633.47
38	(118)	398,345.88397	2,018,291.94176		633.84
30	(117)		2,018,292.28878		635.39
30	(120)		2,017,477.40425	6 25 .25	621.6
JΕ	(119)	398,358.43081	2,019,005.28 69 1		622.87
44	(129)	396,920.99434	2,020,042.19064	625.76	624.6
48		396,940.34767	2,020,463.63663	619.90	618.4
4C	(98)	397,217.02642	2,020,785.315 55	613.04	610.9
40	(97)	397,446.17694	2,020,610.98175	615.35	613.1
4E	(95)	397,651.1294 8	2,020,607.56 23 1	618.54	617.5
4F	(93)	397,680.42416	2,020,25 5 .7 58 92	625.36	622.8
4G	(100)	397,836.73039	2,020,857.61303	620.02	619.1
4H	(99)	397,541.43725	2,020,916.84913	613.43	610.5
5A	(109)	398,061.75689	2,019,781.72 49 7	<i>623</i> . 18	619.4
58	(90)	39 8,520.357 88	2,020,283.72459	600.45	597.4
5C	(104)	<i>398,339.2759</i> 4	2,020,196.97152	608.68	606.8
50	(103)	<i>398,362.32313</i>	2,019,960.197 29	611.71	608.5
5E	(110)	397,802.46440	2,019,748.19597	626.89	623.9
SF	(94)	397,904.64236	2,020,535.56245	618.95	619.4
5G	(8 8)	398,174.57747	2,020,694.69337	615.39	612.0
5H	(89)	398.351.69445	2,020,546.91832	610.62	608.4
		-	•		
10A	(108)	397.913.30549	2.020.009.97063	626.70	624.2
108	(92)	397,899.01251	2.020.243.06886	624.46	621.1
10C	(91)	398,197.02603	2,020,267.33493	617.24	615.4
100	(107)	397.857.53638	2,020,078.59020		623.33
IOE	(106)	397,896.37914	2,020,147.65721		622.52
10F	(105)	397,946.08160	2,020,196.19956		621.47
-0.	, 200 ,	337,340100100	1,020,100.1000		021.47
11A	(101)	398.941.02097	2,020,086.99390	608.22	604.8
118	(102)	398.653.41765	2,020,136.88570	608.14	603.8
	/	,,,	-,,	V	
12A	(124)	397,175.89292	2,019,636.22169	635.66	632.0
128	(113)	397,333.41742	2,019,895.65480	627.55	625.6
120	(115)	397,213.82758	2,019,968.84527	628.05	625.5
120	(112)	397,511.40056	2,019,943.01512	627.45	624.8
12E	(114)	397, 324. 25035	2,020,019.35440	627.48	624.5
12G	(127)	397,111.16499	2,019,819.73011	047.40	
12H	(126)	397,175.34773			629.22
121			2,019,813.89486		629.06
12J	(125)	397,231.20475	2,019,814.97473		269.15
125 12K	(128)	397,175.26975	2,019,858.53625		628.66
12N	(116)	397,222.63773	2,019,904.66442		626.74

(Monitor wells are distinguished from boreholes by having a corresponding elevation of top of P.V.C. value)

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Page	2			,	
NUMBE		NORTH "X"	EAST "Y"	ELEVATION OF TOP P.V.C. PIPE	ELEVATION OF NATURAL GROUND AT WELL
15A	(149)	400,123.22038	2,025,232.61342	570.24	570.7
15B	(148)	399,906.57343	2,025,252.78758	567.12	564.2
15C	(144)	399,884.41824	2,025,168.58849	566.89	564.3
17I	(75)	400,225.13342	2,023,849.67063	578.19	575.2
17J	(56)	400,362.97881	2,023,809.58530	579.79	577.0
17K	(72)	400,193.17235	2,024,001.90555	575.34	573.8
17L	(61)	400,394.21647	2,023,966.04349	577.27	574.4
17M	(65)	400,380.91204	2,024,264.07312	574.28	572.6

*NOTE: WELLS P1 & P2 \sim THE ELEVATIONS SHOWN ARE THE TOP OF THE OPERATOR NUT.

HYDROGEOLOGIC INVESTIGATION CARSWELL AIR FORCE BASE FORT WORTH, TEXAS

Texas State Plane Coordinate and Elevation of Test Wells,
Soil Gas Probes and Sampling Points

July 10, 1990



SITE LF05

NUMBER	TYPE	NORTH "Y"	EAST "X"	ELEVATION TOP OF PVC	ELEVATION NATURAL GROUND AT WELL/BORE
LF05-01 LF05-02 LF05-03 LF05-04 LF05-05 LF05-06 LF05-07 LF05-08 LF05-09 LF05-10 LF05-11 LF05-11 LF05-13 LF05-14 LF05-15 LF05-16 LF05-17 LF05-18 LF05-19	WELL BORE BORE BORE BORE BORE BORE BORE BORE	399,361.2414 399,280.6409 399,182.0957 399,313.9245 399,388.4921 399,156.8559 399,192.7306 399,030.3142 398,918.3183 398,656.8688 398,619.9398 398,669.0930 398,406.7661 398,467.5329 398,082.8055 398,229.3914 398,317.2267 398,169.3001 397,850.5705	2,018,791.3828 2,019,492.0018 2,019,488.6372 2,019,719.9840 2,019,785.8488 2,020,129.6754 2,020,230.2232 2,020,350.8946 2,020,361.5966 2,019,456.1935 2,020,446.5081 2,020,606.7127 2,020,738.5442 2,020,738.5442 2,020,910.0778 2,019,457.4908 2,021,041.6970 2,021,241.4299 2,021,280.2972 2,021,663.8519	621.96 622.69 ~ 602.98 ~	619.3 620.6 620.6 617.3 616.1 598.3 598.0 606.8 604.9 623.9 597.6 594.4 605.0 603.2 626.5 612.3 606.5 612.1 606.3

SURFACE WATER SAMPLES

NUMBER	NORTH "Y"	EAST "X"	ELEVATION OF WATER
LF05-S1	399,327.1085	2,020,155.2125	590.25
LF05-S2 LF05-S3	399,092.2352 398,638.2009	2,021,029.0375 2,020,666.7173	584.73 591.07
LF05-S3	398,564.4359	2,020,956.6955	591.21
LF05-S5	398,383.9429	2,021,422.4749	578.89
LF05-S6	398,458.7264	2,021,661.6152	576.63
LF05-S7	397,873.1003	2,021,549.6706	589.7
STAFF GAUGE	398,445.2564	2,021,286.7444	
ELEVATION OF FLO	WLINE OF CREEK AT GO	JAGE	578.2
WATER ELEVATION	AT GUAGE		579.07
ELEVATION OF 1'	MARK ON GUAGE		579.44

SITE LF04

NUMBER	TYPE	NORTH "Y"	EAST "X"	ELEVATION TOP OF PVC	ELEVATION NATURAL GROUND AT WELL/BORE
LF04-01	WELL	397,653.5721	2,019,579.1905	629.24 -	626.5
LF04-02	WELL	397,732.5422	2,020,510.5024	623.68 -	621.0
LF04-03	PUMP				
	TEST WELL	397,683.4611	2,020,506.7895	623.25	620.5
LF04-04	WELL	397,554.5294	2,021,365.8226	612.07	609.4
LF04-05	BORE	397,347,9116	2,020,805.4209		608.8
LF04-06	BORE	397,210.6006	2,020,593.2486		613.3
LF04-07	BORE	396,819.7427	2,020,897.2163		630.4
LF04-08	BORE	396,935.0825	2,021,021.9109		630.0
LF04-09	BORE	397,136.0543	2,021,145.6966		627.4
LF04-10	WELL	397,025.3443	2,021,275.0320	626.54	626.9

64 311

SITE ST14

					
<u>NUMBER</u>	TYPE	NORTH "Y"	EAST "X"	ELEVATION TOP OF PVC	ELEVATION NATURAL GROUND AT WELL/BORE
ST14-01	WELL	399,886.0854	2,024,309.3181	575.89 -	573.2
ST14-02	WELL	400,102.4353	2,024,311.8094	575.64	572.7
ST14-03 ST14-04	WELL WELL	400,672.3650 400.231.5326	2,024,116.0939 2,024,566.4807	576.72 575.74	574.83 ASP 572.9
5114-04	METT	400,231.3320	2,024,566.460/	3/3./4	3/2.9
				•	
		SIT	E SD13		
NUMBER	TYPE	NORTH "Y"	EAST "X"	ELEVATION TOP OF PVC	ELEVATION NATURAL GROUND AT WELL/BORE
SD13-01	WELL	399,964.3693	2,024,842.2218	573.24	570.3
SD13-02	WELL	400,058.5313	2,024,974.4094	573.39	570.64 ASP
SD13-03	WELL	399,934.0917	2,024,919.8140	571.54	568.6
SD13-04	WELL	399,931.9664	2,024,992.0174	569.24	566.81 ASP
		SURFACE W	ATER SAMPLES		
NUMBER		NORTH "Y"	EAST "X"		WATER
			<u> </u>		ELEVATION
SD13-S1		399,722.7878	2,025,153.1150		551.64
SD13-S2		399,729.5605	2,025,176.1395		551.14
SD13-S3		399,7 47.056 6 399,757. 2 157	2,025,235.6200 2,025,270.1565		549.72 548.95
SD13-S4		399,/3/.213/	2,023,270.1365		240.72

APPENDIX F

Aquifer Pump Test Results June 1990 Pump Test [This page intentionally left blank.]

1.0 INTRODUCTION

The IRP Phase I and Phase II investigations have identified the Flightline Area at Carswell AFB as an on-base site where past waste disposal practices may have led to contamination of soils and ground water. These studies have identified a need to understand the hydrogeologic framework controlling the occurrence of ground water and the factors influencing the direction and rate of ground-water flow. Therefore, an aquifer pumping and recovery test was conducted at the Flightline Area during June, 1990 as part of an on-going IRP Remedial Investigation/Feasibility Study (RI/FS). The objective of the aquifer tests was to determine the hydraulic characteristics of the shallow ground-water bearing zone (Upper Zone Aquifer). The following sections describe the geologic setting of the Flightline Area, aquifer test procedures, and test results.

1.1 <u>Principles of Aquifer Pumping Tests</u>

The value of an aquifer as a source of ground water depends upon water quality and the capacity of the aquifer to store and transmit water. The latter two characteristics are referred to as the properties of storage and transmissivity. The transmissivity is a function of an aquifer's hydraulic conductivity. The hydraulic conductivity is defined as the flow of water in cubic feet per day through a cross-sectional area of one square foot under a hydraulic gradient of one foot per foot (Davis and DeWeist, 1966). Hydraulic conductivity has the dimensions of length/time, or velocity, and is expressed in the units of feet per day.

Transmissivity is a measure of the volume of water which will flow each day through a one foot wide vertical strip of aquifer which extends the fall saturated height of the aquifer. The transmissivity is equal to the product of the hydraulic conductivity and the saturated thickness of the aquifer, and indicates the capacity of the aquifer as a whole to transmit water (Theis, 1935).

The storage coefficient is a dimensionless term defined as the volume of water the aquifer releases from or takes into storage per unit surface area of the aquifer per unit change in the component of head normal to that surface (Walton, 1962). The storage coefficients of unconfined aquifers (e.g., water table aquifers), such as the Upper Zone Aquifer in the Flightline Area, usually range from 0.05 to 0.30 (Ferris, et al., 1962). Unconfined aquifers usually have higher values for storage coefficients than confined aquifers, and these higher values reflect that releases from storage represent mostly pore dewatering, whereas in confined aquifers, releases from storage represent the effects of water expansion and aquifer compaction due to changes in fluid pressure (Freeze and Cherry, 1979). The storage term for unconfined aquifers is also known as the specific yield.

Storage and transmissivity are commonly determined by conducting aquifer tests in wells completed in water-bearing units. Aquifer testing may include constant discharge pump tests, variable rate (step) discharge tests, constant drawdown tests, water level recovery tests, and slug tests.

At the Flightline Area, a constant discharge pump test and water-level recovery tests were conducted to determine the hydraulic properties of the geologic units which contain contaminated ground water. In a constant discharge pump test, a well is pumped at a constant rate and water levels are measured for the duration of the test in the pumping well and in the observation wells which penetrate the water-bearing unit. During the recovery test, the change in the water levels in the wells are recorded after cessation of pumping until near static water levels are attained. Graphs of drawdown and recovery versus time after pumping started and stopped are compared to graphs calculated from mathematical aquifer models to estimate the aquifer parameters.

2.0 GEOLOGIC SETTING

The geologic setting of the Flightline Area at Carswell AFB is described in detail in the main body of this report. Specifically, Section 3.3 provides information about the geologic setting, topography, and stratigraphy. Section 3.4 contains a detailed description of the hydrogeology for the Flightline Area. The reader is referred to these sections prior to proceeding with the remainder of this appendix.

The following paragraphs are provided to supply additional information about the subsurface conditions in the area immediately affected by the aquifer tests.

Soil boring data collected during well installation in the vicinity of the aquifer test location has revealed a coarsening downward sequence of lithologies from land surface to bedrock, which is comprised of the Goodland and Walnut Formations.

The deposits from the surface to bedrock (referred to as "Upper Zone" deposits) are generally 30 to 40 feet thick and consist of 10 to 15 feet of fine grained materials (clay and silt) underlain by 20 to 30 feet of sands and gravels. The thickest sequence of coarser grained materials (sands and gravels) is generally oriented in an east to west trend through the Flightline Area, roughly paralleling White Settlement Road. These deposits are unconsolidated and coarsen downward to predominantly limestone and chert gravels at the contact with the underlying bedrock.

Bedrock of the Goodland and Walnut Formations consists of interbedded, fossiliferous, hard limestone and calcareous shale. The thickness of the Goodland and Walnut Formations in the vicinity of the pumping test location is approximately 30-40 feet. The Goodland and Walnut Formations have been dry when sampled during drilling activities in the area, and with the thickness and hardness of the formations they are believed to form an effective confining layer between the Upper Zone water-bearing deposits and the underlying water-bearing sands of the Paluxy Formation.

The water-bearing zone (Upper Zone Aquifer) immediately adjacent to the pumping well (LF04-03) is an unconfined, or water-table, aquifer. The water table as encountered in the subsurface is under atmospheric pressure, and wells completed in the aquifer will reflect the actual water level. This is in opposition to confined aquifers where wells tapping the aquifer may have water levels considerably above the top of the aquifer.

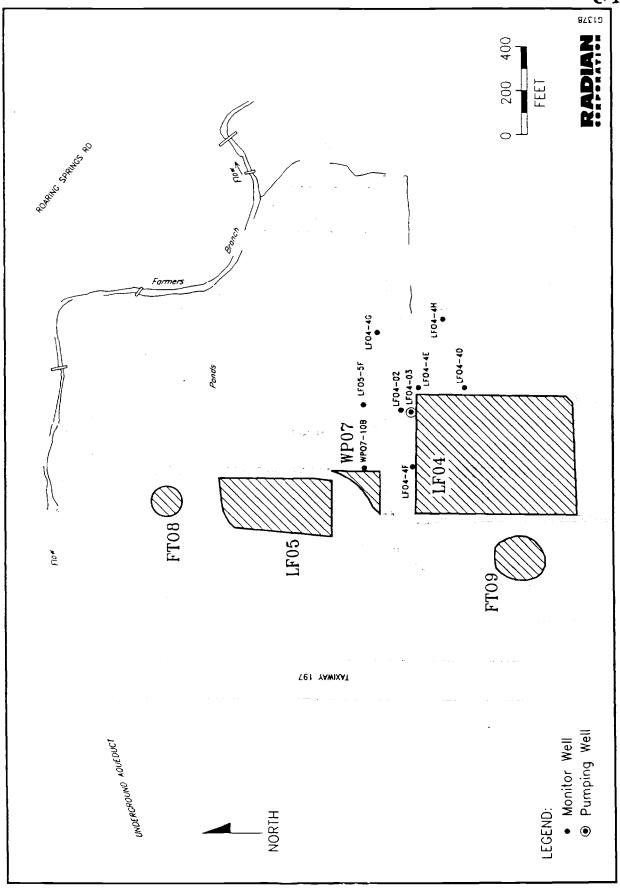
Water levels from wells LF04-02 and LF04-03 were electronically monitored during the pump test and recovery test. The lithologic logs of these wells and well construction data are located in Attachment A.

Well LF04-03, the pumping well, is screened across the lower 14.3 feet of Upper Zone sediments. These sediments are mainly medium grained sand with minor gravels in the upper 10 feet of screened interval, and the lower section of the screen is across predominantly small pebble size gravels (< 10% sand).

Well LF04-02, 50 feet north of the pumping well and the nearest observation well, is screened across similar units as LF04-03. This well also has 14.3 of screen. Again, the screened interval encompasses medium sands, however, the gravel content is not as high near the bottom of the screened interval (approximately 5% gravels) as in LF04-03.

The water table, prior to the start of the aquifer test, occurred approximately 25 feet below land surface in the vicinity of the pump test location. The saturated thickness of the Upper Zone Aquifer was calculated to be 11.7 at the pump well (LF04-03).

In addition to the pump well and near observation well, seven other monitor wells in the vicinity of the pump test location were used as observation wells. These wells are all screened across Upper Zone Aquifer sediments, and vary in distances of 100 to 450 from the pump well (Figure 2-1).



Location of Pumping Well and Observation Wells, Flightline Area Pump Test, Carswell AFB, Texas Figure 2-1.

3.0 FIELD INVESTIGATION

3.1 <u>Pumping Test Procedures</u>

The Flightline Area aquifer pump test was conducted June 21-22, 1990 and ran for 20 hours. The recovery test, which started with the cessation of the pump test, ran for $7 \, 2/3$ hours.

3.1.1 <u>Discharge Water</u>

Discharge water produced during the pump test was run through over 300 feet of polyethylene pipe before being routed into the City of Fort Worth sewer system. Pumping rates were measured approximately every hour using a bucket and stopwatch (volumetrically). The temperature, pH, and conductivity of the discharge water was also measured regularly. The discharge of the pump remained constant through the test, with measured discharges (17) varying from 17.9 to 18.7 gallons-per-minute (gpm). The averaged discharge was 18.3 gpm, leading to an approximate total discharge of 22,000 gallons during the pump test.

At the request of the City of Fort Worth Water Department, the discharge water was aerated for removal of volatile organic compounds (VOCs).

Aeration of the pump test discharge water, prior to sanitary sewer discharge, was accomplished with a trailer mounted 125 cfm air compressor. Air from the compressor was routed to a small holding pond which was receiving water from the pumping well. A hole in the top of the holding pond (swimming pool) allowed for discharge of the aerated water to the sewer system.

Periodically during the pump test, water samples going into the holding pond (pre-aeration) and exiting the pond (post-aeration) were collected. These samples were collected in 40 ml VOA vials, filling each approximately 2/3's with water. These water samples were then allowed to sit in the open sun for several hours prior to a headspace analysis for volatile

organic content. The time spent in the sun allowed volatile organics in the ground-water samples to volatilize to the overlying air column. The volatile organic content of the air (headspace) was then measured with an HNu photoionization detector (PID). This was accomplished by cutting a small slit in the Teflon™ septum in the cap of the vial and quickly inserting the probe of the HNu PID. Table 3-1 summarizes the results of the headspace analyses performed on the discharge water samples from the Flightline Area pump test.

As seen from the table, the aeration of the pump test water prior to discharging to the city sewer system reduced the volatile organic content of the water in every sample analyzed. The average reduction, considering all the analyses, was slightly over 40 percent. The HNu PID is not compound specific, instead measuring the total volatile organic content in the air. The instrument was responding very well, and duplicate (D) analyses performed on the samples from 1630 showed only a three percent relative difference.

3.1.2 <u>Test Types and Measurements</u>

Background water-level data in the pumping well and the near observation well were collected electronically (at 10-minute intervals) for approximately 40 hours with a Hermit electronic data logger prior to the step test. The background data are useful for observing natural trends in the Upper Zone Aquifer water level, such as increases from recharge or decreases due to evapotranspiration. A slight downward trend in water levels, followed by a slight recovery, was observed in wells LF04-02 and LF04-03. The background water level data for the two wells, as well as hydrographs showing the natural water level trends, are included in Attachment B.

A step test was performed prior to the start of the pumping test to establish the optimum pumping rate. The optimum pumping rate for the Flight-line Area pumping test set-up was determined to be the full capacity of the submersible pump (Gould 1/2 HP, Model 10 EJ), or approximately 20 gallons per minute. The pump was rated at approximately 25 gpm (with the amount of

TABLE 3-1. HEADSPACE ANALYSIS

	HNu_Val	ue (ppm)		
Time Sample Taken	Water Going Into Pool	Water Going Into Sewer	Time Sample Analyzed	Background HNu Reading
0945	20+	2-3	1515	0.1
1030	4.5	3.8	1525	0.0
1130	4.6	3.3	1530	0.0
1315	9.4	2.2	1535	0.0
1430	11.6	7.9	1910	0.0
1530	10.3	6.0	1912	0.0
1630	10.4	7.3	1915	0.0
1630 (D)	10.3	7.5	1918	0.0
1915	12.0	6.8	2120	0.0

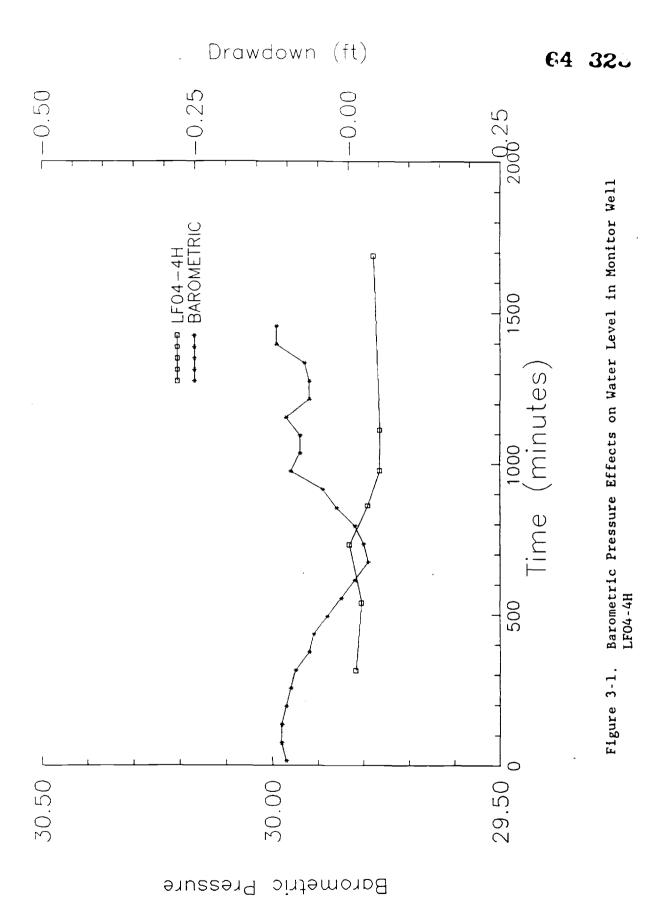
⁽D) - Denotes duplicate sample

hydraulic head encountered in the pumping well); however, travel of discharge water through over 300 feet of polyethylene pipe before ultimate discharge to the sewer system reduced discharge rates proportionately.

The pump test followed the end of the step test by about 16 hours, and measured water levels had recovered to over 99 percent of their pre-step test level. The 4-inch submersible pump (used in pump and step test) was powered by a 3500 watt portable generator.

During both the pumping and recovery tests, water levels in the pumping well (LF04-03) and the near observation well (LF04-02) were recorded using pressure transducers and an automatic data logger (Hermit Model 1000B). The Hermit collected water-level data for the two wells, for both the pump and recovery test, is included in Attachment C. Water levels were also manually measured in surrounding monitor wells with a calibrated Olympic electric water-level probe. The water-level probe was decontaminated prior to each water-level measurement. The water levels in the pumping well and near observation well were also checked regularly with the Olympic meter to verify the accuracy of the Hermit data logger. The manual water-level measurements are provided in Attachment D. The maximum water-level decline observed in the manually measured observation wells was 0.09 feet (LF04-4E). Hydrographs of the water levels in the observation wells during the pump test are also provided in Attachment D.

As seen from the hydrographs, there appears to be a slight water-level rise around 700 minutes into the pump test. The timing of the water-level rise corresponds with a decrease in barometric pressure. Figure 3-1 shows the barometric pressure plotted with the water levels measured in well LFO4-4H. This pressure phenomenon appears to have had a slight effect on the water level of the Upper Zone Aquifer, but the barometric pressure goes back up to roughly the same value as when pumping started by the end of the pump test. The overall trend of water levels does not appear to have been affected significantly by the pressure fluctuations. Unconfined aquifers are naturally less affected by barometric pressure fluctuations than confined aquifers.



4.0 TEST RESULTS

4.1 Analytical Methods and Assumptions

The data obtained during the June 1990 Upper Zone aquifer pumping test were analyzed by several methods. In addition to field plotting of drawdown and distance drawdown measurements, a computer aquifer analysis program was used. The well hydraulics interpretation program used was WHIP $^{\mathbb{N}}$, which has the ability to simulate and analyze both drawdown and recovery tests.

Attempts were initially made to interpret the pump test data using the techniques of Boulton (1963) and Neuman (1975) for unconfined aquifers. These techniques consider the effects of gravity drainage in an unconfined aquifer, which result in a delayed yield of ground water to the well and a corresponding fluctuation in the time-drawdown data curve. As can be seen from Figure 4-1, delayed yield was not pronounced (if evident) in the loglog plot of the near observation well drawdown. Attempts at matching respective portions of the drawdown curve with various Type A and Type B curves met with no success. Therefore, in the analysis of unconfined aquifer data showing no apparent delayed yield, the techniques of Theis and Cooper-Jacob were applied to the data.

The Theis and Cooper-Jacob analyses were used as both field methods and in later data analysis for estimating aquifer parameters. Time versus drawdown for observation wells were plotted on semi-log paper. From this plot, the change in drawdown over a particular log cycle was used in the calculation of aquifer transmissivity and storativity, using the equations:

$$T = \frac{2.3Q}{4\pi\Delta h} \qquad \text{and} \qquad S = \frac{2.25Tt_o}{v^2}$$

where: T - transmissivity

Q - pumping rate

 Δh = the drawdown for one log cycle

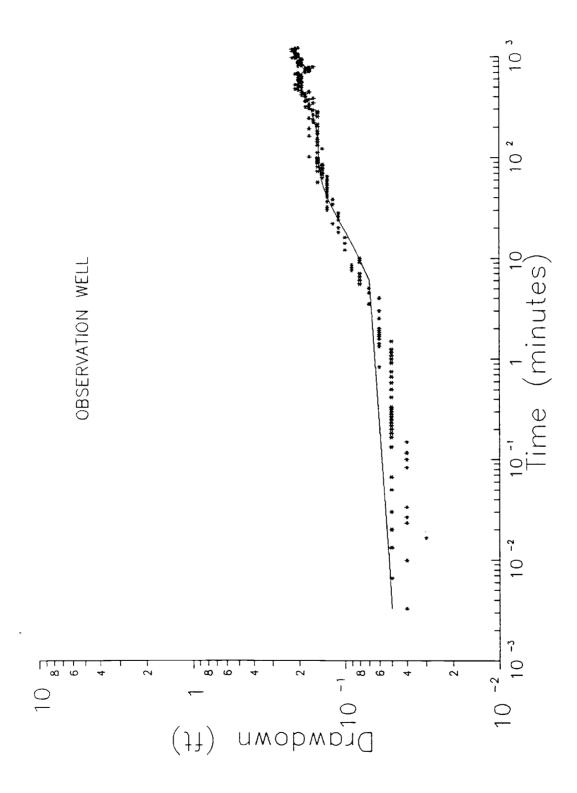


Figure 4-1. Loglog Plot of Observation Well (LF04-02) Drawdown

- S storativity
- t_o time intercept where the drawdown line intercepts the zero drawdown axis
- v radial distance from the pumping well to observation well

The WHIP™ diagnostic procedures also use semilog drawdown (Cooper-Jacob) analyses and Theis recovery analyses to obtain preliminary estimates of the transmissivity and storage coefficient. Theis curves are generated using these values and are graphically compared to the observed data. Portions of the generated curves can be "windowed" so only reliable data are used for the generation of final transmissivity and storage coefficient values.

In addition to standard semilog and loglog plots, the effects of various time transformations on the data as well as first and second derivatives of the drawdowns were performed. Observing the derivative drawdown plots was useful for determining that portion of the test data displaying Theis behavior. Additionally, the Dupuit correction for water table conditions was applied to all computer analyses and the initial estimates of transmissivities and storage coefficients were optimized using an ordinary least squares fitting criterion. This correction minimizes irregularities inherent in field generated data to improve computer aided curve matching techniques and allow greater accuracy in the calculation of aquifer parameters.

Three different computer generated plots and analyses were determined to best represent the Upper Zone aquifer hydraulic properties of transmissivity and storage coefficient. These were the observation well (LF04-02) drawdown and recovery analyses and the pumping well (LF04-03) recovery analysis.

Seven additional monitor wells were measured for response to the pumping well and there was little if any noted.

4.2 Water Level Behavior in Pumping Well and Near Observation Well

The observed maximum drawdown was 3.58 feet in the pumping well and 0.20 feet in the near observation well, located 50 feet north of the pumping well.

4.3 Results

The results of the computer-assisted pump test analyses are presented in Table 4-1. The drawdown and recovery curves for the observation well were analyzed as well as the recovery curve for the pumping well. The average values for the parameters of transmissivity and hydraulic conductivity and a value for storage coefficient are shown on the table. The averaged values are representative of the types of aquifer materials encountered (clean sands and gravels). The WHIP^M generated plots for the analyses are provided in Attachment E.

SUMMARY OF AQUIFER PUMPING TEST RESULTS, FLIGHTLINE AREA, CARSWELL AFB, TEXAS (JUNE, 1990) TABLE 4-1.

Well Number	Type of Test Analyses	Distance From Pumping Well (ft)	Transmissivity	Hydraulic Conductivity	Storage Coefficient (Dimensionless)
LF04-02	Drawdown	50	9771 ft²/day	835 ft/day (2.9 x 10 ⁻¹ cm/sec)	1.2 x 10 ⁻²
	Recovery	50	8260 ft²/day	705 ft/day (2.5 x 10^{-1} cm/sec)	
LF04-03	Recovery	Pumping Well	9501 ft²/day	812 ft/day (2.9 x 10^{-1} cm/sec)	
	-	Average Values	9177 ft²/day	784 ft/day (2.8 x 10 ⁻¹ cm/sec)	1.2 x 10 ⁻²

5.0 REFERENCES

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Well Hydraulics Interpretation Program (WHIP), Version 3.22, by Hydro Geo Chem, Inc., 1430 N. 6th Avenue, Tucson, Arizona, 1987.

ATTACHMENT A

Lithologic Logs and Well Completion Forms

DRILI	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
	ROJECT: CAR				7. TOTAL DEPTH OF HOLE: 37.7 ft BGL	
,, ,,			STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
2 11	CATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill 2-41
				illane !		<u> היסונפ טרוננ פיסו</u>
			ironmental ur	illers, inc.	10. NO. OF SAMPLES TAKEN: 14	
	DLE NO.: L				11. ELEVATION GROUND WATER: 597.45 ft MS	L (6/18/90)
	WE OF GEOL		<u>. E. Fain</u>		12. DATE HOLE ESTABLISHED: 3/28/90	
	CORDINATES				13. SURFACE ELEVATION: 621.00 ft MSL	
<u> </u>	2020510.	50 Y:	397732.54		14. BACKGROUND:	
				 	15. MEASURING POINT ELEVATION: 623.68 ft	MSL
Depth	Graphic	Blow	Soil	ļ		
<u>(Ft.)</u>	Log	Count	Class/Code	Visual Descr	iption	Remarks
0	<i>[///</i>]		U/CLLR	Clay: Dark b	rown, silty, firm, roots, damp,	Full samplers
	Y///			carbonaceous	staining.	unles noted.
1	Y///		1	1		
į	Y/J/J		Ì	1		İ
2	$V//\lambda$		U/CLLR	Clay: As abo	we; at 3.0 ft. going to orange/brown, silty	i
	////		1		- 10% calcareous material.	i
			1	1		! !
ļ			 	ŧ 		1
4			 U/CLLR	Itlave As sha	A48	11 5 60 00000000
4	Y///		O/CEEK	Clay: As abo	ve.	1.5 ft. Recovery
	Y///		ļ	ļ		
	\mathbb{Z}/\mathbb{Z}		!	1		!
	$V//\lambda$		ļ	ļ		
6	V / / X		U/CLLR	Clay: Orange	/brown, very silty, minor very fine grained	ļ
	V//J		1	sand, stiff,	calcareous nodules, carboaceous streaking.	1
			1	1		
	Y ///		1	1		İ
8	Y///		U/CLLR	Clay: As abo	we, increasing calcareous material to 30%.	i
	Y///		i	i	•	i
	Y///		i	i		,
	Y///		i i	1		1
	V / / X		1	1]
	V//X		} 	1		
	\(\delta \delt		l uzenen	100-44 0		
11	0.0.0		U/SDGR	:	evel: Orange, very poorly sorted, cohesive,	
	0.0.0		!	clayey, silt	y, damp, abundant calcareous material.	
	1		1	1		
	1.0.0.0		I			
13	$b \cdot o \cdot o$		U/SDLR	Sand: Orange	e, fine grained, minor larger sizes to	
	1.0.0.0		1	coarse, stig	htly clayey and silty, damp.	
13.5	0.0.0		U/SDLR	Sand: As abo	we, increasing coarseness with depth, 5 -	
	.0.0.		Ì	10% small gr		İ
			i	i		i
	N^{N}		i	i		i
	1.0.0.0		i	i		Ì
16 F	0.0.0		 U/SDLR		eve, gravelly; changing to tan, fine to	1
10.5	0.0.0		0/30LK	•		1
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		I .	imedium grain	ned, loose, quartzose at 18.0 ft., damp.	1
	0.0.0		!	!		!
	1.0.0.0		1	1		ļ
18.5	(p.o.a)		U/SDLR	Sand: As abo	ove, well sorted, medium grained, damp; 0.4	3.5 ft. Recovery
	1.0.0.0		1	ft gravelly	zone at 21.5 - 21.9 ft.	1
	1		1	1		1
	$r \cap \cdot \cap \cdot$			i		i
	0.0.0		1			
	0.0.0) 	1		1
			} 	1		
	0.0.0		} 	1		!

						(1 000 F)
DRILL	ING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHE	ET 2 OF 2 SHEETS
	OJECT: CARS				7. TOTAL DEPTH OF HOLE: 37.7 ft BGL	
<u>i</u>		PHASE II			8. DATUM FOR ELEVATION SHOWN: see lev	rel
2. LO	CATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL	
3. DR	ILLING AGE	NCY: Envi	ronmental Dri	llers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
4. HO	LE NO.: LI	F04-02			11. ELEVATION GROUND WATER: 597.45 f	t MSL (6/18/90)
5. NA	ME OF GEOLS	OGIST: S.	E. Fain_		12. DATE HOLE ESTABLISHED: 3/28/90	
6. CO	ORDINATES (OF HOLE:		_	13. SURFACE ELEVATION: 621.00 ft MSL	·
X:	2020510.	50 <u>Y:</u>	397732.54		14. BACKGROUND:	
<u></u>					15. MEASURING POINT ELEVATION: 623.6	8 ft MSL
Depth	Graphic	Blow	Soil	1		I
(Ft.)	Log	Count	Ctass/Code	Visual Descr	iption	Remarks
23.5			 U/SDLR 	•	:/tan, medium grained, well sorted, 10% quartz; 0.3 ft. gravelly zone at 27 f : 28 ft.	
 			 	 Sand: As abo	ove, 1-3% granule size gravel.	 W. L. measured at 28.1 ft. BLS, 5.0 ft. Recovery
 33.5			 	 Sand: Tan, m gravels to 2	medium grained, quartzose, Loose, wet, 53 25 mm.	
 37 			 U/MARL 	 Limestone: M fissile. 	Marty, weathered sand and gravet intermix	ked, T.D. = 37.7 ft.

RIL	LING LOG	RADIAN	CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 1	OF 2 SHEETS
1. PI	ROJECT: CAR	SWELL AFB,			7. TOTAL DEPTH OF HOLE: 37.6 ft BGL	
	IRP	PHASE II	STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
	OCATION: F				9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
3. DI	RILLING AGE	NCY: Envi	<u>ronmental Dri</u>	illers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
4. H	OLE NO .: L	F04-03			11. ELEVATION GROUND WATER: 597.58 ft MS	L (6/18/90)
<u>5. N</u>	AME OF GEOL	OGIST: S.	B. Blount, S	S. E. Fain	12. DATE HOLE ESTABLISHED: 3/20/90	
6. C	CORDINATES	OF HOLE:			13. SURFACE ELEVATION: 620.50 ft MSL	
Χ:	2020506.	<u>79 Y:</u>	<u> 397683.46</u>		14. BACKGROUND:	
					15. MEASURING POINT ELEVATION: 623.25 ft	MSL
epth	Graphic	Blow	Soil	1		1
<u>ft.)</u>	Log	Count	Class/Code_			Remarks
0	Y///		U/CLAY	Clay: Brown,	soft to firm, semi-plastic, with fine	full recovery
	r///		1	rootlets and	minor carbonaceous streaking and	unless otherwise
	Y///		1	particles, m	oist to wet.	indicated.
	Y///		1	1		}
2	Y//A		U/CLAY	Clay: As abor	ve, firm to stiff (stiffens to base), minor	Too stiff to cut.
	V//A		1	calcareous d	ebris, more abundant carbonaceous staining,	1
	$V//\lambda$		1	very stiff;	3.8 - 4.0 ft.	1
	$V//\lambda$		1	1		1
4	$V//\lambda$		U/CLLR	Clay: Orange	/brown at 4.1 ft; brittle, damp, abundant	Hard pushing.
	V//X		1	calcareous d	ebris, slickensided, calichified with some	1
	V//		1	authigenic m	ineralization (crystals of CaCO3 in shell	}
			ĺ	frags.); ver	y hard, silty.	İ
6			U/CLLR	•	ve, very stiff, slightly sandy and silty.	i
_	Y///	; 	1	1	,,,,,	i
	Y///		1	i		\
	Y///		ł	i		1
8	V///		U/CLLR	Intere As abo	ve, few large CaCO3 pebbles (25 mm),	 1 ft. recovery,
	$V///\lambda$		I O/CEEK		lacareous material with depth, very fine	
	$V//\lambda$		1	grained sand	• •	ST. Rig broken.
	V///		<u> </u>	laisuen seun	•	Continue after
10	V//		l U/CLLR	ICLAND CARRO	then allow advantage dame > 700	repairs. Caliche layer st
10			I OFCELK	•	/brown, silty, cohesive, damp, > 30%	
			!	catcareous m	aterial, stiff.	12 ft., drilling
			ļ.	I		through.
			I.			
	<u>, </u>		1	1		!
12.1			U/SDFN		, fine grained, loose, damp, quartzose,	<u>I</u>
	<u> </u>		Ţ	•	at 14.3 ft. sharp change to tan, very fine	İ
			1	grained sand	, heavily oxidized in laminae.	
			Ţ	İ		!
14.5			U/SAND	Sand: Orange	, fine to medium grained, quartzose, damp,	3 ft. Recovery.
	1		1	loose; grave	lly seam 15 - 15.5 ft.	
	1		1	1		1
	1		1	1		
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	1		1	1		
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19.5			I U/SDLR	Sand: Orange	/tan, fine to medium grained, damp, loose,	6 ft. Recovery.
. , , .			1	:	90% quartz, 1 - 3% small gravel and shells.	•
	P.O.O.		1	1	TVA YOUR LET I - JA MINELL BIOTEL BIRL SHELLS.	1
	10.0.0	!	I I	1		
	K. ~ . ~]	ı	ı		1
	ħ.O.O.		1	i		i

ORILLING LOG	RADIAN CORPORATION		INSTALLATION: CARSWELL AFB, TX SHEET 2	OF 2 SHEETS
1. PROJECT: CARSWE			7. TOTAL DEPTH OF HOLE: 37.6 ft BGL	
	ASE II STAGE 2		8. DATUM FOR ELEVATION SHOWN: sea level	
2. LOCATION: Flig			9. MANUFACTURER'S DESIGNATION OF DRILL:	Mobile Drill B-61
	: Environmental Dri	illers, Inc.	10. NO. OF SAMPLES TAKEN: 14	
4. HOLE NO.: LF04			11. ELEVATION GROUND WATER: 597.58 ft MS	SL (6/18/90)
	ST: S. B. Blount, S	S. F. Fain	12. DATE HOLE ESTABLISHED: 3/20/90	101.01.07
6. COORDINATES OF			13. SURFACE ELEVATION: 620.50 ft MSL	
x: 2020506.79			14. BACKGROUND:	
×	1. 377003.40		15. MEASURING POINT ELEVATION: 623.25 ft	
epth Graphic	Blow Soil	1	TIP HENDORING TOTAL ELEVATIONS OCCUPY	
	- ·	Visual Descr	rintian	Remarks
Ft.) Log	tount (cress/code	I	iption	I REMOTES
0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	U/SDLR	•	e/tan, fine to medium grained, wet, loose, velly zone at 27 ft., quartzose; at 30 ft.	•
29.5	 U/SDLR 	 Sand: As abo	ove, saturated.	 3.2 ft. Recovery.
10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	U/GRVL	 Gravel: Var <10% sand, :	icolored, up to pebble size (30 mm), shells, saturated.	
34.5 0 0 0 0 0 0 0 0 0	U/GRVL	•	above, mainly small pebble size (5 - 10 mm), angular to subrounded, large percentage of	
37.5	U/MARL	Mari: Chalk throughout. 	y gray, indurated, oxidation stained	Sampler refusal a 37.5 ft., drove 1 1/2 in. S.S. 50 blows = 1 in.; T. = 37.6 ft.

COMPLETION LOG	RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
	STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 3/28/90
		10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
CATION: Site LF04		11. ZONE OF COMPLETION: Aquifer
STALLING CO.: Radia	n Corporation	12. SEAL END DEPTH: 20.90 ft
LL NO.: LF04-02		13. MEAS. POINT ELEV.: 623.68 ft MSL
LL OWNER: U.S. AIR	FORCE	14. CASING DIAMETER: 2.00 in
LL TYPE CLASS: MONI		15. CASING MATERIAL: Schedule 40 PVC
RMATION OF COMPLETIO	N:	16. SCREEN BEGIN. DEPTH: 23.10 ft
CATION TYPE: WL		17. SCREEN SLOT SIZE: 0.02 in
REMARKS: 1-10/x24x0	.02" Screen,3-10'x2" Risers,1	-Cut piece (-0.4'),1-Locking Cap, 1-bottom Cap
		TOP OF CASING
	GROUND SURFACE	<u> </u>
†	1	1 1 1
	1	
	CKFILL MATERIAL:	
Ceme	nt-Bentonite Grout	
	l	
		BOREHOLE DIAMETER:
_ [/	\ 8.000 in
BOREHOLE		
DEPTH:	ļ	
37.70 ft	ļ	
	!	SEAL MATERIAL:
ļ	!	Bentonite
		_
!	1 !	
ļ	SEAL LENGTH:	
ļ	2.00 ft	CASING DEPTH:
ļ	1	37.65 ft
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l I		! — ! ! !
l I	; ;	SCREEN LENGTH:
l I		Screen Condin:
i	FILTER PACK	
	LENGTH:	
	16.80 ft	! <u></u> ! !
	10.80 TT	
		BIANK LENGTH
	ļ ļ	BLANK LENGTH:
· ·	1	0.20 ft
į	1 1	
ļ	ļ ļ	

FILTER PACK MATERIAL: 8-20 Silica Sand

COMPLETION LOG	RADIAN CORPORATION	INSTALLATION: CARSWELL AFB
PROJECT: IRP PHASE II	STAGE 2, CARSWELL AFB	9. INSTALLATION DATE: 4/3/90
		10. WELL COMPLETION METHOD: GRAVEL PACK W/SCREEN
OCATION: Site LF04		11. ZONE OF COMPLETION: Aquifer
NSTALLING CO.: Radi	an Corporation	12. SEAL END DEPTH: 19.40 ft
ELL NO.: LF04-03		13. MEAS. POINT ELEV.: 623.25 ft MSL
ELL OWNER: U.S. AIR	FORCE	14. CASING DIAMETER: 6.00 in
ELL TYPE CLASS: MON	ITORING WELL	15. CASING MATERIAL: Schedule 80 PVC
ORMATION OF COMPLETE	ON:	16. SCREEN BEGIN. DEPTH: 22.40 ft
OCATION TYPE: WL		17. SCREEN SLOT SIZE: 0.02 in
. REMARKS: 1x10'x6"	PVC 0.020 screen, 1x5'x6" scre	een, 2x10'x6" PVC riser, 1x5'x6" riser.
		TOP OF CASING
	GROUND SURFACE	<u> </u>
<u>†</u>	ļ .	!!!!
	BACKFILL MATERIAL:	
Ce	ment-Bentonite Grout	
ļ		BOREHOLE DIAMETER:
1	4	\ 14.500 in
BOREHOLE		
DEPTH:		
37.52 ft	 	
 	ļ	Bentonite
] 	
<u> </u>	+	
 	SEAL LENGTH:	
<u> </u>	2.30 ft	CASING DEPTH:
i i		37.42 ft
i	.	
<u>'</u>		
!		
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! 	i i	
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]]		36x26x 22x01x.
! !	FILTER PACK	
] 1	LENGTH:	-
] 1	18.12 ft	
ļ	10.12 11	
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ļ		
l		
1		BLANK LENGTH:
ļ	;	• • • •
	į į	0.76 ft

FILTER PACK MATERIAL: 8-20 Silica Sand

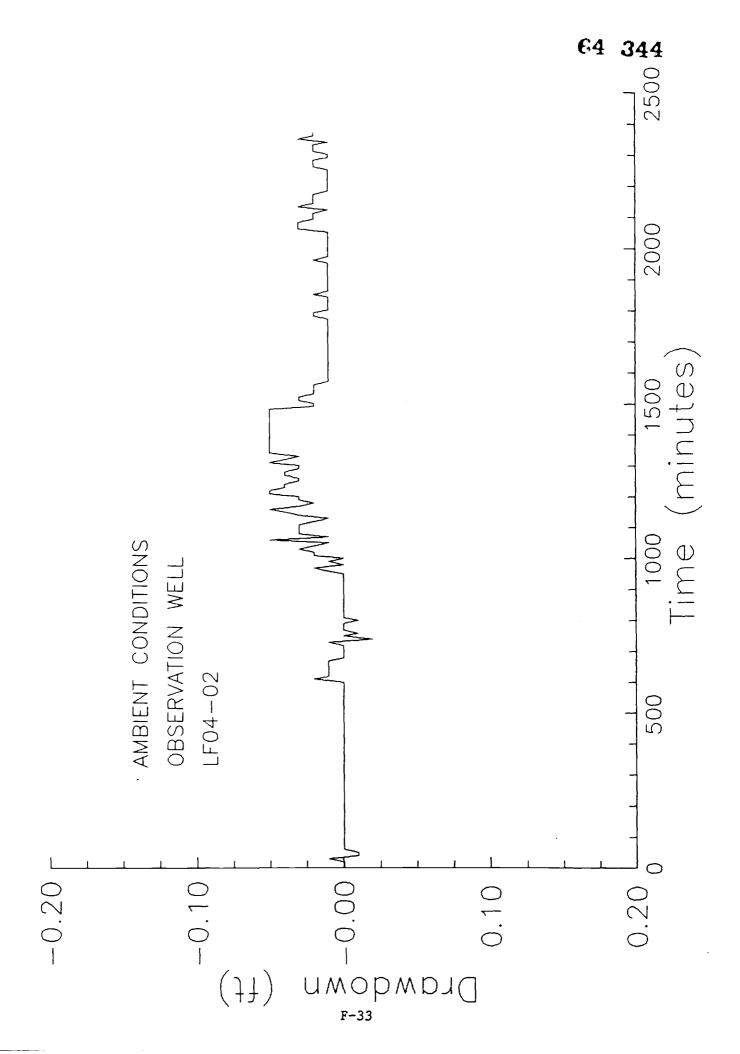
ATTACHMENT B

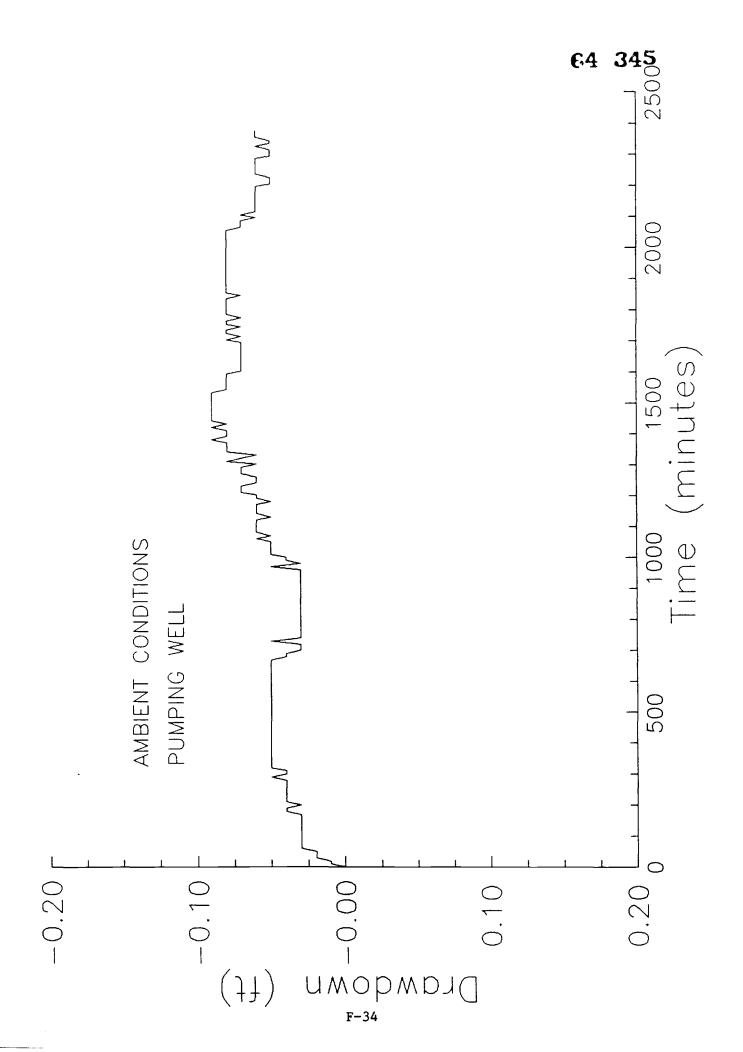
Background Water-Level Data and Hydrographs

Time		Time		Time		Time	
minutes	n	ninutes	r	ninutes		minutes	
0	0	600	-0.05	1200	-0.06	1800	-0.08
. 10	-0.01	610	-0.05	1210	-0.07	1810	-0.08
20	-0.01	620	-0.05	1220	-0.07	1820	-0.08
30	-0.02	630	-0.05	1230	-0.07	1830	-0.08
40	-0.02	640	-0.05	1240	-0.06	1840	-0.07
50	-0.02	650	-0.05	1250	-0.06	1850	-0.08
60	-0.03	660	-0.05	1260	-0.06	1860	-0.08
70	-0.03	670	-0.05	1270	-0.07	1870	-0.08
80		680	-0.04	1280	-0.07	1880	-0.08
	-0.03					1890	-0.08
90	-0.03	690	-0.04	1290	-0.07		
100	-0.03	700	-0.03	1300	-0.06	1900	-0.08
110	-0.03	710	-0.03	1310	-0.08	1910	-0.08
120	-0.03	720	-0.03	1320	-0.07	1920	-0.08
130	-0.03	730	-0.05	1330	-0.06	1930	-0.08
140	-0.03	740	-0.03	1340	-0.08	1940	-0.08
150	-0.03	750	-0.03	1350	-0.08	1950	-0.08
160	-0.03	7 6 0	-0.03	1360	-0.08	1960	-0.08
170	-0.03	770	-0.03	1370	-0.08	1970	-0.08
180	-0.04	780	-0.03	1380	-0.09	1980	-0.08
190	-0.04	790	-0.03	1390	-0.08	1990	-0.08
200	-0.03	800	-0.03	1400	-0.08	2000	-0.08
210	-0.04	810	-0.03	1410	-0.08	2010	-0.08
220	-0.04	820	-0.03	1420	-0.09	2020	-0.08
				1430	-0.03	2030	-0.08
230	-0.04	830	-0.03				
240	-0.04	840	-0.03	1440	-0.09	2040	-0.08
250	-0.04	850	~0.03	1450	-0.09	2050	-0.08
260	-0.04	860	-0.03	1460	-0.09	2060	-0.07
270	-0.04	870	-0.03	1470	-0.09	2070	-0.07
280	-0.04	880	-0.03	1480	-0.09	2080	-0.07
290	-0.05	890	-0.03	1490	-0.09	2090	-0.0€
300	-0.04	900	-0.03	1500	-0.09	2100	-0.07
310	-0.04	910	-0.03	1510	-0.09	2110	-0.06
320	-0.05	920	-0.03	1520	-0.09	2120	-0.06
330	-0.05	930	-0.03	1530	-0.09	2130	-0.06
340	-0.05	940	-0.03	1540	-0.08	2140	-0.06
350	-0.05	950	-0.03	1550	-0.08	2150	-0.0
360	-0.05	960	-0.03	1560	-0.08	2160	-0.0€
370	-0.05	970	-0.05	1570	-0.08	2170	-0.06
380	-0.05	980	-0.03	1580	-0.08	2180	-0.0
							-0.0
390	-0.05	990	-0.04	1590	~0.08	2190	
400	-0.05	1000	-0.04	1600	-0.07	2200	-0.0
410	-0.05	1010	-0.05	1610	-0.07	2210	-0.0
420	-0.05	1020	-0.05	1620	-0.07	2220	-0.0
430	-0.05	1030	-0.05	1630	-0.07	2230	-0.0
440	-0.05	1040	~0.05	1640	-0.07	2240	-0.0
450	-0.05	1050	-0.05	1650	-0.07	2250	-0.0
460	-0.05	1060	-0.06	1660	-0.07	2260	-0.0
470	-0.05	1070	-0.05	1670	~0.07	2270	-0.0
480	-0.05	1080	-0.06	1680	-0.07	2280	-0.0
490	-0.05	1090	-0.06	1690	-0.07	2290	-0.0
500	-0.05	1100	-0.06	1700	-0.08	2300	-0.0
510	-0.05	1110	-0.06	1710	-0.07	2310	-0.0
520	~0.05	1120	-0.06	1720	-0.08	2320	-0.0
530			-0.05	1730	-0.08	2330	-0.0
	-0.05	1130					
540	-0.05	1140	-0.06	1740	-0.07	2340	-0.0
550	-0.05	1150	-0.06	1750	-0.08	2350	-0.0
560	-0.05	1160	-0.06	1760	-0.08	2360	-0.0
570	-0.05	1170	-0.06	1770	-0.07	2370	-0.0
580	-0.05	1180	-0.05	1780	-0.08		
590	-0.05	1190	-0.06	1790	-0.08		

Time	•	Time		Time		Time	
minutes 0		minutes 600		minutes	0.02	minutes	-0.01
10	0		0 -0.02	1200	-0.03	1800 1810	-0.01
20	0 0	610 620	-0.02 -0.01	1210 1220	-0.05 -0.05	1820	-0.01
30	-0.01	630	-0.01 -0.01	1230	-0.05 -0.04	1830	-0.01
40	0.01	640	-0.01 -0.01	1240	-0.04	1840	-0.01
50	0.01	650	-0.01	1250	-0.04	1850	-0.02
60	0.01	660	-0.01	1260	-0.03	1860	-0.01
70	0	670	-0.01	1270	-0.03	1870	-0.01
80	0	680	0.01	1280	-0.04	1880	-0.01
90	0	690	0	1290	-0.03	1890	-0.01
100	0	700	0	1300	-0.03	1900	-0.01
110	0	710	0	1310	-0.05	1910	-0.01
120	0	720	0	1320	-0.04	1920	-0.01
130	0	730	-0.01	1330	-0.03	1930	-0.01
140	0	740	0.02	1340	-0.05	1940	-0.01
150	0	750	0	1350	-0.05	1950	-0.01
160	0	760	0.01	1360	-0.05	1960	-0.02
170	0	770	0.01	1370	-0.05	1970	-0.01
180	0	780	0	1380	-0.05	1980	-0.01
190	0	790	0	1390	-0.05	1990	-0.01
200	0	800	0.01	1400	-0.05	2000	-0.01
210	0	810	0	1410	-0.05	2010	-0.01
220	0	820	0	1420	-0.05	2020	-0.01
230	0	830	0	1430	-0.05	2030	-0.01
240	0	840	0	1440	-0.05	2040	-0.01
250	0	850	0	1450	-0.05	2050	-0.01
260	0	860	0	1460	-0.05	2060	-0.03
270	0	870	0	1470	-0.05	2070	-0.03
280	0	880	0	1480	-0.05	2080	-0.03
290	0	890	0	1490	-0.02	2090	-0.02
300	0	900	0	1500	-0.02	2100	-0.02
310	0	910	0	1510	-0.03	2110	-0.02
320	0	920	0	1520	-0.03	2120	-0.01
330	0	930	0	1530	-0.02	2130	-0.03
340	0	940	0	1540	-0.02	2140	-0.02
35 0	0	950	0	1550	-0.02	2150	-0.02
360	0	960	-0.01	1560	-0.02	2160	-0.02
370	0	970	-0.02	1570	-0.01	2170	-0.02
380	0	980	0	1580	-0.01	2180	-0.01
390	0	990	-0.01	1590	-0.01	2190	-0.01
400	0	1000	0	1600	-0.01	2200	-0.01
410	0	1010	-0.02	1610	-0.01	2210	-0.01
420	0	1020	-0.02	1620	-0.01	2220	-0.01
430	0	1030	-0.03	1630	-0.01	2230	-0.01
440	0	1040	-0.02	1640	-0.01	2240	-0.01
450	0	1050	-0.01	1650	-0.01	2250	-0.01
460	0	1060	-0.05	1660	-0.01	2260	-0.02
470	0	1070	-0.01	1670	-0.01	2270	-0.02
480	0	1080	-0.03	1680	-0.01	2280	-0.02
490	0	1090	-0.03	1690	-0.01	2290	-0.01
500	0	1100	-0.03	1700	-0.01	2300	-0.01
510	0	1110	-0.03	1710	~0.01	2310	-0.02
520	0	1120	-0.02	1720	-0.01	2320	-0.02
530	0	1130	-0.01	1730	-0.01	2330	-0.02
540	0	1140	-0.03	1740	-0.01	2340	-0.01
550	0	1150	-0.04	1750	-0.01	2350	-0.03
560	0	1160	-0.05	1760	-0.01	2360	-0.02
570	0	1170	-0.03	1770	-0.01	2370	-0.02
580	0	1180	-0.02	1780	-0.02		
590	0	1190	-0.03	1790	-0.02	F-32	
					_	1-72	

64 343





ATTACHMENT C

Hermit Collected Water-Level Data for Pump and Recovery Tests

minutes	wdown		Time	Drawdown	Time	Drawdown	Time	Drawdown	Time
0.0000 0.58 5.5 3.65 110 3.94 660 0.0033 0.42 6.0 3.67 120 3.94 670 0.0066 0.50 6.5 3.67 120 3.94 670 0.0099 0.51 7.0 3.69 140 3.95 690 0.0136 0.63 8.0 3.70 150 3.95 700 0.0200 0.63 8.5 3.71 170 3.97 710 0.0233 0.65 9.0 3.72 180 3.96 730 0.0266 0.68 9.5 3.72 190 3.98 740 0.0300 0.71 10 3.73 200 3.96 750 0.0500 0.88 14 3.77 220 3.97 770 0.0500 0.88 16 3.78 230 3.98 780 0.0831 1.09 18 3.79 240 3.99 790	ft.	S	minutes	ft.	minutes	ft.	minutes	ft.	minutes
0.0033	4.05	<u> </u>	660	3.94	110	3.65		0.58	0.0000
0.0099	4.03)	670	3.94	120	3.67	6.0		0.0033
0.0133 0.54 7.5 3.70 150 3.95 700 0.0166 0.63 8.0 3.70 160 3.97 710 0.0200 0.63 8.5 3.71 170 3.97 720 0.0233 0.65 9.0 3.72 190 3.98 740 0.0300 0.71 10 3.73 200 3.96 750 0.0303 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 760 0.0500 0.88 16 3.78 230 3.98 780 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 280 4.00 830 <td>4.05</td> <td>)</td> <td>680</td> <td>3.95</td> <td>130</td> <td>3.67</td> <td>6.5</td> <td>0.50</td> <td>0.0066</td>	4.05)	680	3.95	130	3.67	6.5	0.50	0.0066
0.0166 0.63 8.0 3.70 160 3.97 710 0.0200 0.63 8.5 3.71 170 3.97 720 0.0233 0.65 9.0 3.72 180 3.96 730 0.0300 0.71 10 3.73 200 3.96 750 0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830	4.06)	690	3.95	140	3.69	7.0	0.51	0.0099
0.0166 0.63 8.0 3.70 160 3.97 710 0.0200 0.63 8.5 3.71 170 3.97 720 0.0233 0.65 9.0 3.72 180 3.96 730 0.0300 0.71 10 3.73 200 3.96 750 0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830	4.05	3	700	3.95	150	3.70	7.5	0.54	0.0133
0.0200 0.63 8.5 3.71 170 3.97 720 0.0233 0.65 9.0 3.72 180 3.96 730 0.0300 0.71 10 3.73 200 3.96 750 0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840	4.06	0	710	3.97			8.0		0.0166
0.0233 0.65 9.0 3.72 180 3.96 730 0.0266 0.68 9.5 3.72 190 3.98 740 0.0300 0.71 10 3.73 200 3.96 750 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1500 1.40 26 3.82 280 4.00 830 0.1500 1.41 26 3.82 280 4.00 850 0.2166 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.85 310 4.01 860	4.05	2	720	3.97			8.5		0.0200
0.0266 0.68 9.5 3.72 190 3.98 740 0.0300 0.71 10 3.73 200 3.96 750 0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 280 4.00 830 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 870	4.05	o	730	3.96					1
0.0300 0.71 10 3.73 200 3.96 750 0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1500 1.40 26 3.82 280 4.00 830 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2066 1.65 34 3.86 320 4.01 870	4.06								1
0.0333 0.75 12 3.75 210 3.97 760 0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1533 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1533 1.54 30 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870	4.05								1
0.0500 0.88 14 3.77 220 3.97 770 0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 340 4.01 890	4.05								1
0.0666 0.98 16 3.78 230 3.98 780 0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.01 860 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 890 0.2666 1.82 40 3.86 350 4.01 90	4.06								1
0.0833 1.09 18 3.79 240 3.99 790 0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 890 0.2666 1.82 40 3.86 350 4.01 990 0.2833 1.85 42 3.87 360 4.01 920 0.3166 1.94 46 3.88 380 4.02 940	4.06								1
0.1000 1.17 20 3.81 250 3.98 800 0.1166 1.26 22 3.82 260 3.98 810 0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 890 0.2666 1.82 40 3.86 350 4.01 890 0.2833 1.85 42 3.87 360 4.01 910 0.3000 1.90 44 3.88 380 4.02 930	4.07								
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0.1333 1.34 24 3.82 270 3.98 820 0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 890 0.2500 1.76 38 3.86 350 4.01 990 0.2666 1.82 40 3.86 350 4.01 900 0.2833 1.85 42 3.87 360 4.01 910 0.3166 1.94 46 3.88 380 4.02 930 0.3333 1.99 48 3.87 390 4.02 950	4.06								1
0.1500 1.40 26 3.82 280 4.00 830 0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 880 0.2500 1.76 38 3.86 340 4.01 890 0.2666 1.82 40 3.86 350 4.01 900 0.2833 1.85 42 3.87 360 4.01 910 0.3000 1.90 44 3.86 370 4.01 920 0.3166 1.94 46 3.88 380 4.02 930 0.3333 1.99 48 3.87 390 4.02 950	4.06								1
0.1666 1.47 28 3.84 290 3.99 840 0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 880 0.2500 1.76 38 3.86 340 4.01 890 0.2666 1.82 40 3.86 350 4.01 900 0.2833 1.85 42 3.87 360 4.01 910 0.3000 1.90 44 3.86 370 4.01 920 0.3166 1.94 46 3.88 380 4.02 930 0.3333 1.99 48 3.87 390 4.02 940 0.4167 2.16 50 3.87 400 4.02 950	4.06								I
0.1833 1.54 30 3.84 300 4.00 850 0.2000 1.59 32 3.85 310 4.01 860 0.2166 1.65 34 3.86 320 4.01 870 0.2333 1.70 36 3.86 330 4.01 890 0.2500 1.76 38 3.86 340 4.01 890 0.2666 1.82 40 3.86 350 4.01 990 0.2833 1.85 42 3.87 360 4.01 910 0.3000 1.90 44 3.86 370 4.01 920 0.3166 1.94 46 3.88 380 4.02 930 0.3333 1.99 48 3.87 390 4.02 940 0.4167 2.16 50 3.87 400 4.02 950 0.5000 2.30 52 3.88 410 4.03 960	4.07								1
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0.3000 1.90 44 3.86 370 4.01 920 0.3166 1.94 46 3.88 380 4.02 930 0.3333 1.99 48 3.87 390 4.02 940 0.4167 2.16 50 3.87 400 4.02 950 0.5000 2.30 52 3.88 410 4.03 960 0.5833 2.42 54 3.88 420 4.01 970 0.6667 2.50 56 3.88 430 4.02 980 0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.04 1040 <td>4.08</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td>	4.08								1
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0.3333 1.99 48 3.87 390 4.02 940 0.4167 2.16 50 3.87 400 4.02 950 0.5000 2.30 52 3.88 410 4.03 960 0.5833 2.42 54 3.88 420 4.01 970 0.6667 2.50 56 3.88 430 4.02 980 0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.5833 3.10 74 3.89 520 4.05 1070 </th <td>4.08</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td>	4.08								1
0.4167 2.16 50 3.87 400 4.02 950 0.5000 2.30 52 3.88 410 4.03 960 0.5833 2.42 54 3.88 420 4.01 970 0.6667 2.50 56 3.88 430 4.02 980 0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060<	4.08								Y
0.5000 2.30 52 3.88 410 4.03 960 0.5833 2.42 54 3.88 420 4.01 970 0.6667 2.50 56 3.88 430 4.02 980 0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.5800 3.05 76 3.90 530 4.05 1080	4.08								l .
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0.6667 2.50 56 3.88 430 4.02 980 0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5800 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.04 11	4.13								
0.7500 2.57 58 3.88 440 4.03 990 0.8333 2.62 60 3.89 450 4.03 1000 0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1	4.11								1
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0.9167 2.69 62 3.88 460 4.04 1010 1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05	4.08								l .
1.0000 2.74 64 3.88 470 4.03 1020 1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 114	4.07	_							1
1.0833 2.80 66 3.88 480 4.03 1030 1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.07								L
1.1667 2.85 68 3.89 490 4.04 1040 1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.10								
1.2500 2.91 70 3.89 500 4.04 1050 1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.09								ì
1.3333 2.96 72 3.89 510 4.03 1060 1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.08								
1.4166 3.01 74 3.89 520 4.05 1070 1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.08								
1.5000 3.05 76 3.90 530 4.05 1080 1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.10								
1.5833 3.10 78 3.91 540 4.03 1090 1.6667 3.14 80 3.89 550 4.05 1100 1.7500 3.17 82 3.91 560 4.04 1110 1.8333 3.20 84 3.91 570 4.04 1120 1.9167 3.24 86 3.91 580 4.05 1130 2.0 3.27 88 3.91 590 4.05 1140	4.09								1
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2.5 3.41 90 3.92 600 4.03 1150	4.10						88		
	4.10								
3.0 3.50 92 3.92 610 4.04 1160	4.12	30	116	4.04	610	3.92	92		1
3.5 3.56 94 3.93 620 4.04 1170	4.10	70	117	4.04	620	3.93	94	3.56	3.5
4.0 3.59 96 3.93 630 4.04 1180	4.10	30	118	4.04	630	3.93	96	3.59	4.0
4.5 3.61 98 3.93 640 4.05 1190	4.09	€	119	4.05	640	3.93	98	3.61	4.5
5.0 3.64 100 3.93 650 4.03 1200	4.08	20	120	4.03	650	3.93	100	3.64	5.0

Time	Drawdown	Time	Drawdown	Time	Drawdown	Time	Drawdown
minutes	ft.	minutes	ft.	minutes	ft.	minutes	ft.
0.0000	0.05	5.5	0.08	110	0.15	660	0.19
0.0033	0.04	6.0	0.08	120	0.14	670	0.18
0.0066	0.05	6.5	0.08	130	0.15	680	0.18
0.0099	0.04	7.0	0.08	140	0.15	690	0.19
0.0133	0.05	7.5	0.09	150	0.15	700	0.18
0.0166	0.03	8.0	0.09	160	0.17	710	0.18
0.0200	0.05	8.5	0.09	170	0.15	720	0.19
0.0233	0.04	9.0	0.08	180	0.15	730	0.19
0.0266	0.04	9.5	0.08	190	0.17	740	0.2
0.0300		10	0.08	200	0.15	750	0.19
0.0333		12	0.1	210	0.15	760	0.2
0.0500		14	0.1	220	0.16	770	0.19
0.0666		16	0.1	230	0.16	780	0.18
0.0833		18	0.11	240	0.17	790	0.22
0.1000		20	0.11	250	0.15	800	0.22
0.1166		22	0.12	260	0.16	810	0.22
0.1333		24	0.11	270	0.15	820	0.22
0.1500		26	0.11	280	0.15	830	0.22
0.1666		28	0.11	290	0.16	840	0.23
0.1833		30	0.13	300	0.16	850	0.23
0.2000		32		310	0.17	860	0.22
0.2166		34	0.12	320	0.16	870	0.23
0.2333		36		330	0.16	880	0.23
0.2500		38		340	0.15	890	0.23
0.2666		40		350		900	0.23
0.2833		42		360		910	0.23
0.3000		44		370		920	0.23
0.3166		46		380		930	0.23
0.3333		48		390		940	
0.3333		50		400		950	
0.5000		52		410		960	,
0.5833		54		420		970	
0.6667		56		430		980	
0.7500		58		440		990	
0.8333		60		450		1000	
0.833		62		460		1010	
1.0000		64		470		1020	
1.0833		66		480		1030	
1.1667		68		490		1040	
1.2500		70		500		1050	
1.3333		72		510		1060	
1.416		74		520		1070	
1.5000		76		530		1080	
1.583		78		540		1090	
1.666		80				1100	
		82				1110	
1.750		84				1120	
1.833		80				1130	
1.916		81				1140	
2.		94				1150	
2.						1160	
3.		98				1170	
3.		9-				1180	
4.		9				1190	
4.		9				1200	
5.	0 0.07	10	0 0.17	650	0.18	1200	0.24

Pumping well recovery test

Time	Drawdown	Time	Drawdown	Time	Drawdown
(minutes)	(Ft)	(minutes)	(Ft)	(minutes)	(Ft)
0.0000	4.00	2.0	0.88	76	0.58
0.0033	4.01	2.5	0.84	78	0.58
0.0066	3.98	3.0	0.82	80	0.58
0.0099	3.95	3.5	0.80	82	0.58
0.0133	3.58	4.0	0.79	84	0.58
0.0166	3.84	4.5	0.77	86	0.58
0.0200	3.86	5.0	0.76	88	0.58
0.0233	3.81	5.5	0.75	90	0.58
0.0266	3.77	6.0	0.74	92	0.57
0.0300	3.74	6.5	0.73	94	0.57
0.0333	3.70	7.0	0.72	96	0.57
0.0500	3.56	7.5	0.72	98	0.57
0.0666	3.42	8.0	0.71	100	0.57
0.0833	3.31	8.5	0.70	110	0.56
0.1000	3.22	9.0	0.70	120	0.56
0.1066	3.17	9.5	0.70	130	0.56
0.1333	3.12	10	0.69	140	0.55
0.1500	3.08	12	0.68	150	0.55
0.1666	3.03	14	0.67	160	0.54
0.1833	2.98	16	0.66	170	0.54
0.2000	2.93	18	0.66	180	0.54
0.2166	2.88	20	0.65	190	0.54
0.2333	2.83	22	0.65	200	0.54
0.2500	2.78	24	0.64	210	0.53
0.2666	2.72	26	0.64	220	0.53
0.2833	2.67	28	0.63	230	0.53
0.3000	2.62	30	0.63	240	0.53
0.3166	2.56	32	0.63	250	0.53
0.3333	2.51	34	0.62	260	0.53
0.4167	2.24	36	0.62	270	0.52
0.5000	2.02	38	0.61	280	0.53
0.5833	1.85	40	0.61	290	0.52
0.6667	1.70	42	0.61	300	0.51
0.7500	1.56	44	0.61	310	0.53
0.8333	1.45	46	0.61	320	0.53
0.9167	1.35	48	0.60	330	0.51
1.0000	1.27	50	0.60	340	0.51
1.0833	1.20	52	0.60	350	0.52
1.1667	1.15	54	0.60	360	0.51
1.2500	1.10	56	0.60	370	0.51
1.3333	1.06	58	0.60	380	0.51
1.4166	1.03	60	0.59	390	0.51
1.5000	0.99	62	0.59	400	0.51
1.5833	0.96	64	0.59	410	0.51
1.6667	0.94	66	0.59	420	0.48
1.7500	0.92	68	0.59	430	0.49
1.8333	0.91	70	0.58	440	0.49
1.9167	0.89	72	0.58	450	0.49
		74	0.58	460	0.49

Γ	Time	Drawdown	Time	Drawdown		Time	Drawdown
l	(minutes)	(ft.)	(minutes)	(ft.)		(minutes)	(ft.)
H	0.0000	0.24	2.0	0.23		76	0.19
l	0.0033	0.25	2.5	0.23		78	0.19
	0.0066	0.24	3.0	0.23		80	0.19
	0.0099	0.24	3.5	0.23	1	82	0.19
	0.0133	0.25	4.0	0.23		84	0.19
l	0.0166	0.24	4.5	0.23		86	0.19
١	0.0200	0.24	5.0	0.23		88	0.19
Ì	0.0233	0.25	5.5	0.22		90	0.19
	0.0266	0.24	6.0	0.23		92	0.19
1	0.0300	0.24	6.5	0.23		94	0.19
	0.0333	0.25	7.0	0.23		96	0.18
1	0.0500	0.24	7.5	0.23		98	0.18
	0.0666	0.24	8.0	0.23	l	100	0.18
١	0.0833	0.24	8.5	0.23	ļ	110	0.18
1	0.1000	0.24	9.0	0.23		120	0.17
1	0.1000	0.24	9.5	0.23	1	130	0.17
1	0.1333	0.24	10	0.23		140	0.17
	0.1500	0.24	12	0.23		150	0.14
ı	0.1666	0.24	14	0.23	- 1	160	0.13
-	0.1833	0.23	16		-	170	0.13
	0.2000	0.23	18			180	0.13
1	0.2166	0.24	20		1	190	0.14
1	0.2333		22			200	0.13
1	0.2500		24		Ì	210	0.12
1	0.2666		26		}	220	0.12
١	0.2833		28		1	230	0.12
	0.3000		30		ł	240	0.12
	0.3166		32		1	250	0.12
1	0.3333		34		1	260	0.13
۱	0.4167		36		ł	270	0.12
	0.5000		38		l	280	
-	0.5833		40		1	290	
ļ	0.6667		42			300	
	0.7500		44			310	
	0.8333		46		İ	320	
	0.9167		48			330	• •
	1.0000		50			340	
	1.0833		52		1	350	
	1.1667		54		ļ	360	
	1.2500		56]	370	
!	1.3333		58		ł	380	
	1.4166		60			390	
	1.5000		62		1	400	
	1.5833		64		}	410	
	1.6667		66		}	420	
	1.7500		66		}	430	
	1.7300		70		}	440	
	1.9167		72			450	
	1.316/	0.23	7.			460	
				+ 0.19		400	0.1

ATTACHMENT D

Hand Monitored Water-Level Data and Hydrographs of the Hand-Measured Water-Level Data

wner 💆	ARSW	ELL,	Address	SWL AFB		Co	unty		_ State	
tec	21	lune	1990		Measured by	Ste	ve F	Fair , 5	cott	Bloomt
I No.	LF04	-02	Distan	ce from pumping well	I	Type of				
ump uratio	on: Date <u>4</u> off: Date n of aquife	<u> </u>	me <u>6745 (t)</u> Time 6 <u>347 (t')</u> Wery <u>460</u>	Water Static water level _ Measuring point _ Elevation of measur			Dep Prev	Q measured th of pump/aii vious pumping	r line	
Date		Time Since Pump On	Water	Remarks	Date	Clock Time	Time Since Pump On	Water Level		Remarks
121	0704		26.27	,						
	1044	179	26.35						1	
	1325	340	26.36							
	1705	560	26.40						<u> </u>	
	2012	747	26.41							
_	2220	875	26.44							
/22	2419	994	26.44							_
	0239	1134	26.45	!						
	1215	1710	26.32	relevery		ļ	!		İ	
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Owner .	C'APZSU	IELL.	Address <u>CR</u>	SWL AFB		Co	ounty	<i></i>		State	
Date	2/	June	199	70	Measured b	y Ste	re.	Fa	in, 500	# Blook	
Well No.	LF	04-4	D Distan	ice from pumping well		_ Type of	test	<i>j</i> >.	mping	Test No	
				sured with							
				1			_				
Pumn	on: Date (ime Data	me <u>0745 (t)</u>	Water Static water level	Level Data			U	_	arge Data	
			ime 0347 (t')				-			line	
Duration	on of aquite	er test:		Measuring point			-			Yes No _	
Pum	ping <u>/20</u>	Z Reco	very <u>460</u>	Elevation of measuri	ng point			Dura	ation	End	
Date	Clock Time	Time Since Pump On	Water Level	Remarks	Date	Clock Time	SI	me nce ip On i	Water Lavel	Remarks	
6/21	0645		18.13							İ	
	0900	75	18.13								
	1257	312	18.13								
	1415	390	18.12								·
	1545	480	13.12								
	1645	540	18.11								
<u>_</u> _	1954	729	18.13								
	ZZOZ	958	18.15								
		974									
6/22			18.15				<u> </u>				
	1150	1685	18.17								
	:	1									
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Owner 4	"ARSWE	16_	Address <u>CRS</u>	WL AFB		Co	ounty		State 7×
Date	21	June	1990	_ 	Measured b	, <u>St</u>	eve t	Fain, Su	IT Blount
								_	Test No
Measurii	ng equipir	nent <u>M</u>	and meas	und with	E-line				
								Pleat	
Time Data Pump on: Date €-⊋1 Time ₽745 (t) Static water level How Q measured									•
Pump	off: Date	6-22 T	ime <u>0347(t')</u>	Measuring point _			- } `		line
ì	on of aquif		very <u>460</u>	Elevation of measuri	ng point		_ 1	_	Yes No
Fulli	Jilig 7	Time	<u> </u>			i	Time	ration	End
Date		Since Pump On	Water	Remarks	Date	Clock Time	Since Pump On	Water Level	Remarks
14/21	0642	-	21.40	·		1735	590	21.45	
	0745	<u> — </u>		Start Tist		1805	620	21.46	
<u> </u>	0800	15	21.40			1830	645	21.46	
	0815	30	21.41			1905	480	21.46	
	0830	45	21.41			1955	730	21.46	
	0845	60	21.41			2059	744	21.46	
	0900	75	21.41	<u> </u>		2200	B 55	21.48	
	0930	105	21.11	i		2357	972	21.49	<u> </u>
	1000	135	21.41	:		1150	1106	21.49	
	1030	165	2112			0339	1194	21.49	
	1100	195	21.42			1147	1682	21.49	Mount
	1130	275	21.42	!					
	ì	1	21.43						
	-	1	21.43						
			21.44	1					
	•		21.44	[·	
	1	380	21.44	1					
	ī	410	21.44	1 .					‡
		i	21.45						
			21.45						
	-	511		i					
			21.45	1					İ
	-		21-45	1	-				

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Page	_/	of	1

	_			SUL AFB					
ate <u> </u>	2//	une	1990		Measured by	54	eve 1	Fuin S	att Blount
II No.	LFO	4-4F	Distance	ce from pumping we	E-110	Type of	test <u>Pu</u>	mpiny	Test No
			777.439				<u> </u>		
omp,		ime Data e-2/ Til	me <u>87 45</u> (t)	Static water level	Level Data		_ How C		narge Data
ump	off: Date	6-22 T	ime 03 47(t')	Measuring point			Depth	of pump/air	line
	on of aquifo		very 460	Elevation of measu	ring point		_ }	_	Yes No
Date		Time Since Pump On	Water	Remarks	Date	Clock Time	Time Since Pump On I	Water Level	Remarks
121	0700		27.03					_	
	0909	84	27.03						
	1314	329	27.02						
	1700	555	27.01						
	2009	864	27.02						
	2217	872	27.04						
	2416	991	27.06						
	0232	1127	2707	! 					<u> </u>
		<u> </u>	27.07	·					
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Owner <u>Carswell</u> Ad	idress			c	ounty		_ State			
Date 21 June 19	90	м	leasured by	, Ste	ve Fa	in Sec	it Blunst			
Well No. LF04-46	Distanc	ce from pumping well _		_ Type of	test Pur	mping Te	Test No			
Measuring equipment						• /				
					<u> </u>					
Time Data Pump on: Date 6/2/ Time	0745 (t)	Water La Static water level			How	Discharge Data How Q measured				
Pump off: Date 422 Tim		Measuring point				Depth of pump/air line				
Duration of aquifer test:		Elevation of measuring			l	Previous pumping? Yes No				
Pumping 1202 Recove	ery <u>460</u>					ation	End			
Clock Since Date Time Pump On t	Water Level	Remerics	Date	Clock Time	Since Pump On I	Water Level	Remarks			
6/21:0653 -	23.76									
1304 319	23.74						<u> </u>			
1650 545	23.74									
2001 736	23.74									
2209 864	23.74			_						
6/22 2406 981	23.77									
0222 1117	23.78									
1158 1693	23.78	recovery					<u> </u>			
	<u>:</u>				<u> </u>		1			
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AQUIFER TEST DATA

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Vell No.	LFO	4-4H	Distan	ce from pumping well		_ Type of	test 5	Pu.n	ping Tes	Test No.	
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Pump o		me Data	me 0745 (t)	Static water level				How C		narge Data	
			ime 0347(t')	Measuring point			1			tine	
	of aquife		Hick	Elevation of measuring p						Yes No _	
Pumbi	ng /20		very 460						ion	End	
Date		Time Since Pump On		Remarks	Date	Clock Time		on i	Water Level	! Remarks	
2/21	0656		17.19				1				
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	1645	540	17.16	inducent fewell)							
			17.14								
	2207	862	17:17				<u> </u>				
1/22	2403	978	17.19					<u></u>			
:	0219	1114	17.19				1				
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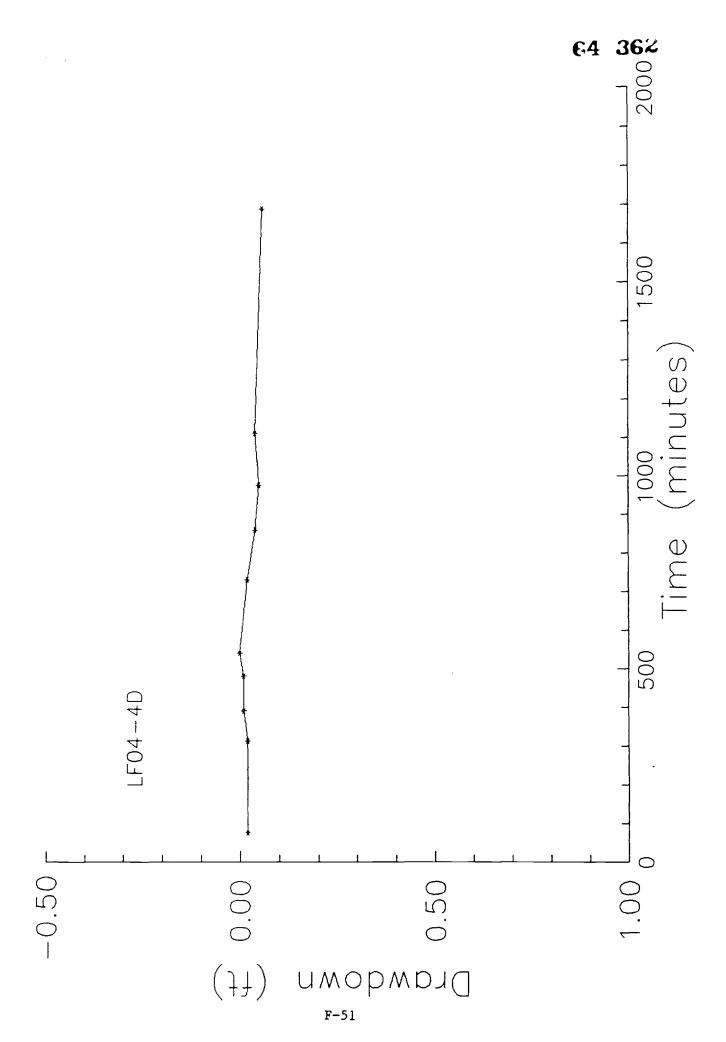
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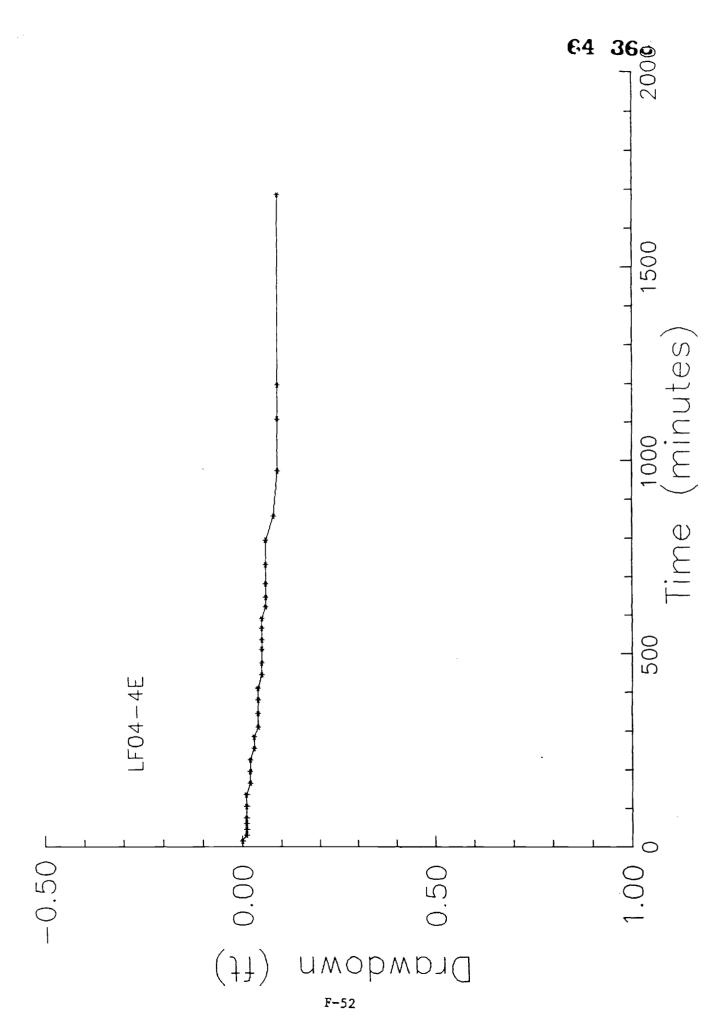
Owner CAPSWELL Address CR.	SWL	Co	ounty	_ State
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Well No Distan	ce from pumping well	Type of	test Pumpins	Test No
Measuring equipment Hand Meas	wied w Eli	16		
Time Data	Water Lev	and Date	Ole	
Pump on: Date 6-21 Time 6745(t)	Static water level		T .	charge Data
Pump off: Date $6-22$ Time $0347(t')$	Measuring point		_	r line
Duration of aquifer test: Pumping 1202 Recovery 460	Elevation of measuring	point	İ	? Yes No
Time ; Clock Since Water Date Time Pump On Level	Remarks	Clock Date Time	Time	Remarks
6/21:0658 - 25.68				
1311 326 25.67	1			
1657 552 25.67				
2006 741 25.67	i			
2215 870 2568]			
2413 988 2570				
0229 1124 25.71	1			
1206 1701 25.71	secovery			
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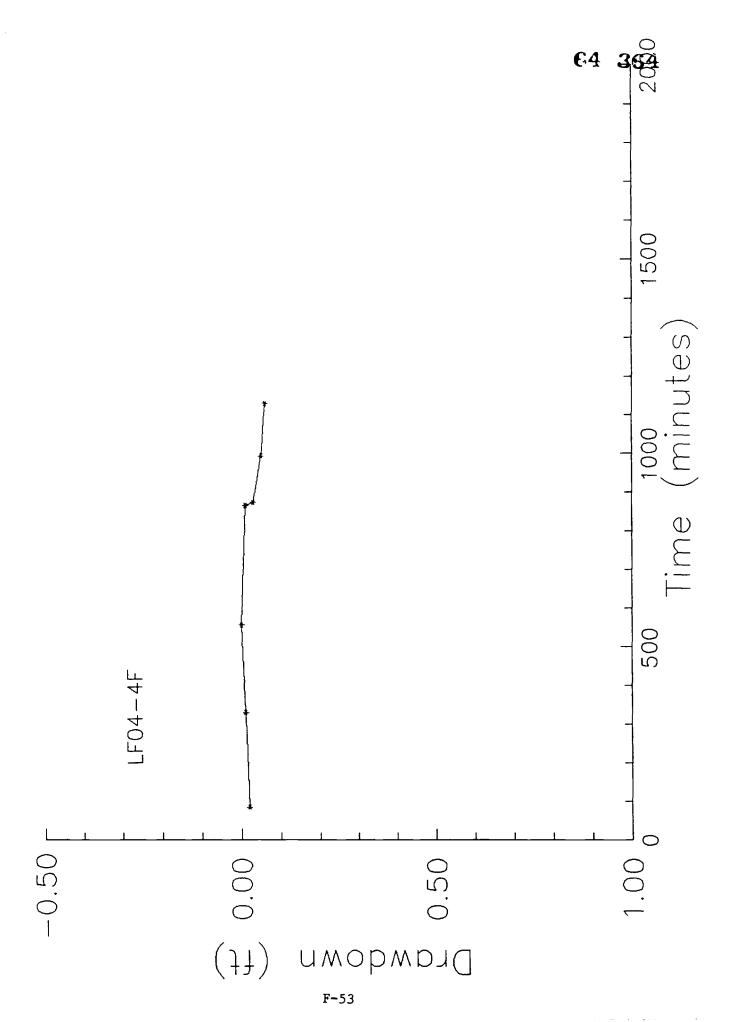
64 361 Page _____ of ____

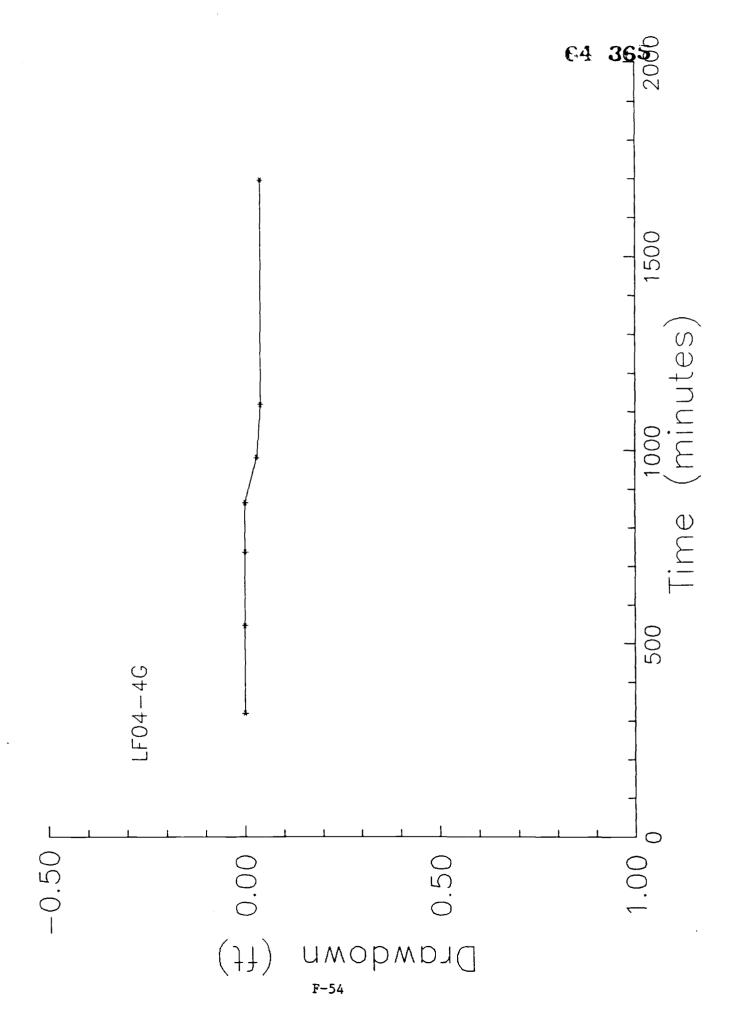
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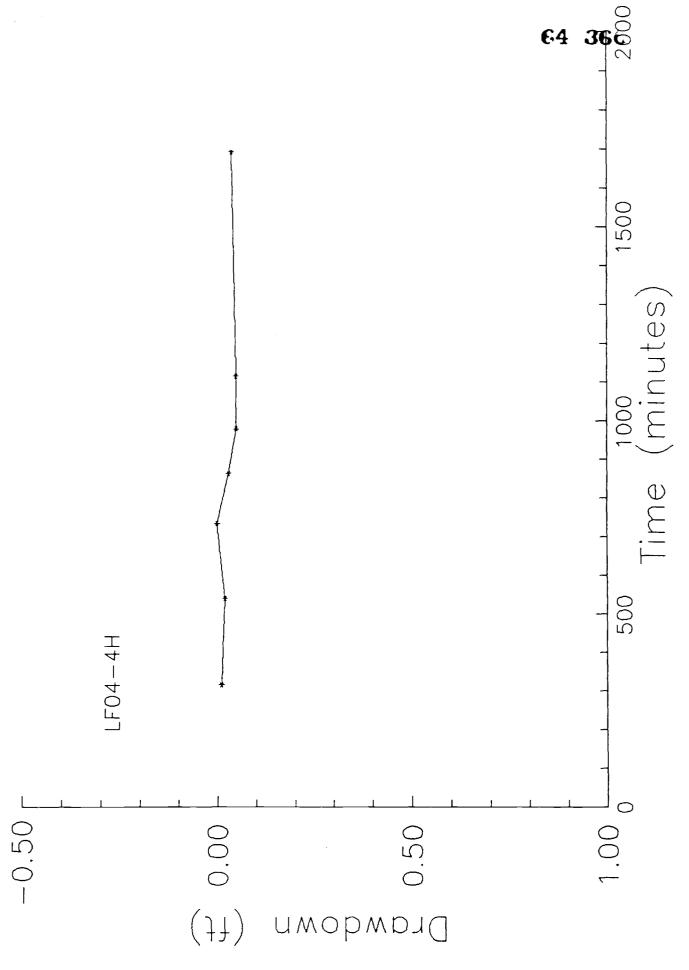
	-			WL AFB		C	ounty		State
Dat e	6-	21-	- 90	N	Measured b	y Ste	ve Fain	, 500	H Blount
			•				test Du	Turdu	Test No
Measurin	ig equipm	ent _ <i>K</i>	land Ni	Prasured wy	/ E-	ling			
Pump Duratio	Ti on: Date off: Date on of aquife	6-22 Ter test:	me <u>0745 (t)</u> ime <u>8377 (t')</u> very <u>460</u>	Water L Static water level Measuring point Elevation of measurin			— Depth Previou	measured of pump/air li us pumping?	ne No
Date	Clock Time	Time Since Pump On	Water	Remarks	Date	Clock	Time Since Pump On I	Water Level	Remarks
6-21	0655		21.90						
			21.89						
	1655	550	21.89						
	2003	738	21.99			<u> </u>			<u> </u>
	2213	808	21.90						
	2410	985	71.92						
	6225	1120	21.92					<u> </u>	
	1202	1697	21.93	Lewery				<u>_</u>	
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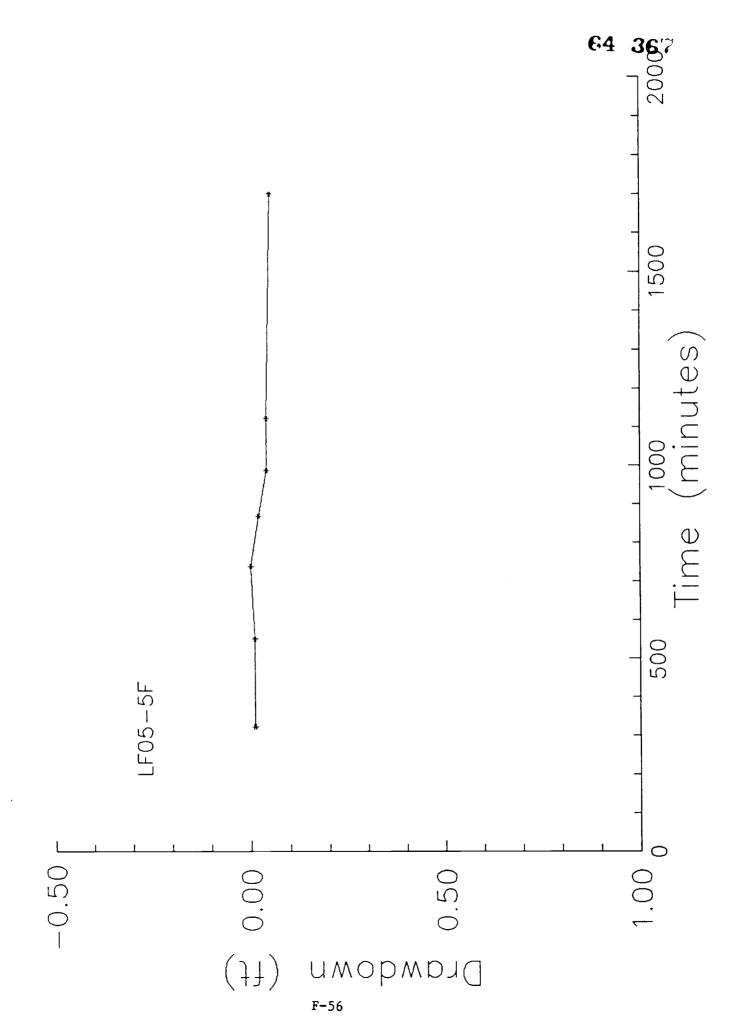


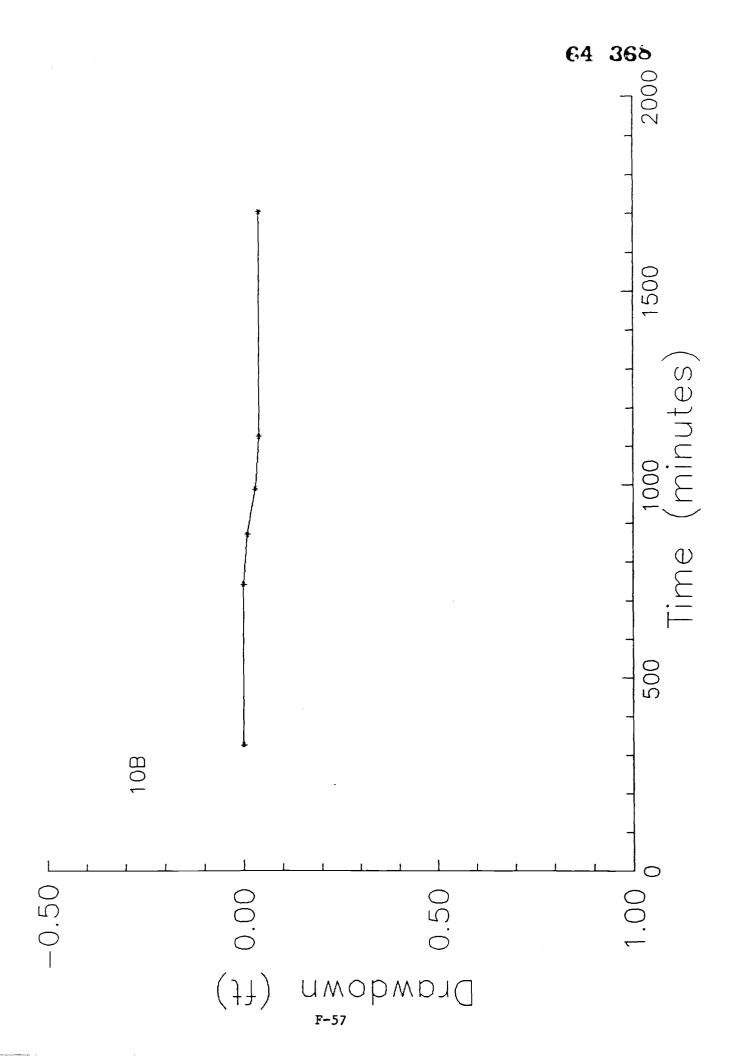






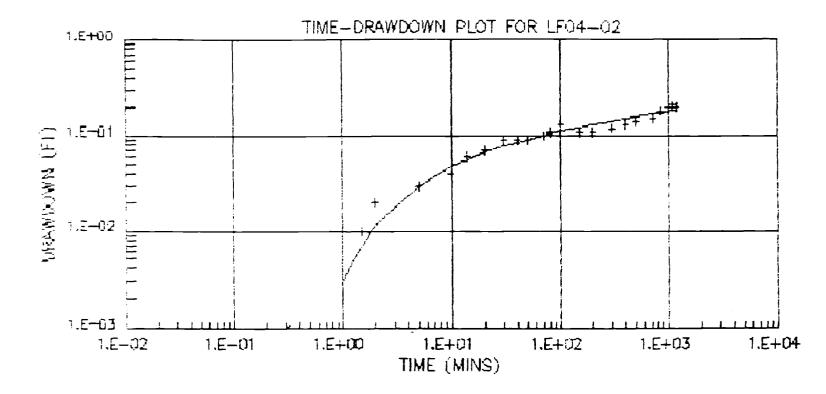






ATTACHMENT E

WHIP™ Plots Used in Analysis of Pump and Recovery Tests

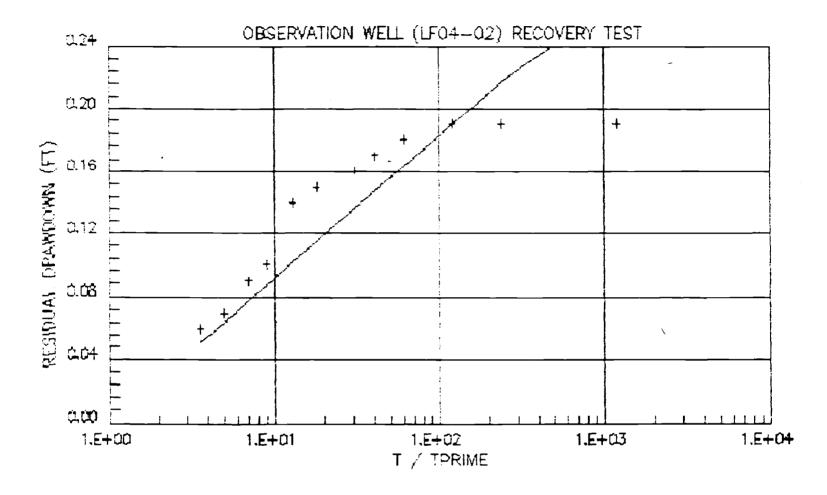


Variables

Saturated thickness = 11.7 ft
Maximum drawdown (pumping well) = 3.5 ft
r = 50 ft
Q = 18.3 gpm
Pump well radius = 0.25 ft
Effective casing radius = 0.7 ft

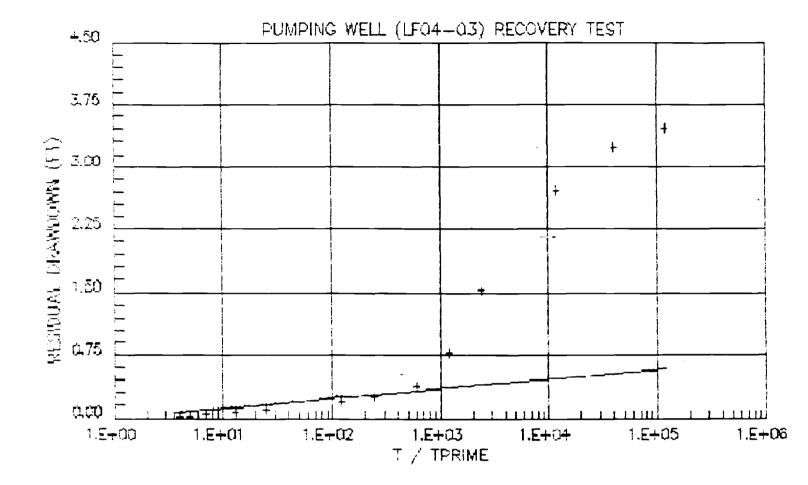
Results

Transmissivity = $9771 \text{ ft}^2/\text{day}$ Storage coefficient = 1.2×10^{-2} (Results have Dupuit correction applied and have been optimized with seven iterations by the Levenberg-Marquardt Minimization Algorithm).



${\tt Results}$

Transmissivity = $8260 \text{ ft}^2/\text{day}$ (Result has been optimized with seven iterations by the Levenberg-Marquardt Minimization Algorithm).



Windowed data (2,100) on T/TPrime plot used in analysis.

Results

Transmissivity = $9501 \text{ ft}^2/\text{day}$ (Result has been optimized with seven iterations by the Levenberg-Marquardt Minimization Algorithm).

APPENDIX G

DPM Evaluation Worksheet for the Flightline Area

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

	FACE WATER PATHWAYS	Score (circle	Multiplier	Product (score x mult.)	Max. score
: .	Have contaminants been detected in surface water? If yes, assign score of 100 and proceed to item 10. If no, assign score of 0 and proceed to item 2.	0 100	ì	100	100
Pat	hway characteristics				
2.	Distance to nearest surface water	0 1 2 3	4		12
3.	Net precipitation	0 1 2 3	1		3
4.	Surface erosion potential	0 1 2 3	4		12
5 .	Rainfall intensity	0 1 2 3	4		12
٤.	Surface permeability	0 1 2 3	3		9
7.	Sum of items 2 through 6				48
8.	Normalized score (multiply item 7 x 100/48)				
9.	Flooding potential	0 1 2 3	8		24
10.	Adjusted pathways score If item 1 is 100, enter 100. If item 1 is 0, enter sum of items 8 and 9. If sum exceeds 100, enter 10			100	
11.	Waste containment effectiveness factor (Table 2)			1.0	
12.	Final score for surface water pathways (multiply i	tem 10 x it	em 11)	100	

COMMENTS ON SURFACE WATER PATEWAYS

Known surface water contamination

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

GROUNDWATER PATEWAYS

<u> Dbse</u>	rved releases		rele	<u>Multiplier</u>	Product (score x mult.)	Max. score
13.	Have contaminants been detected in groundwater? If yes, assign score of 100 and proceed to item 20. If no, assign score of 0 and proceed to item 14.	0	100	1	100	100
Path	way characteristics					
14.	Depth to seasonal high groundwater from base of waste or contaminated zone	0 1	2 3	9		27
15.	Permeability of the unsaturated zone	0 1	2 3	5		15
16.	Infiltration potential	0 1	2 3	5		15
17.	Sum of items 14 through 15					57
18.	Normalized score (multiply item 17 x 100/57)					
19.	Potential for discrete features in the unsaturated zone to "short-circuit" the pathway to the water table	0 1	2 3	5		15
20 .	Adjusted pathways score. If item 13 is 100, enter If item 13 is 0, enter sum of items 18 and 19. If sum exceeds 100, enter 100.	100.			100	
21.	Waste containment effectiveness factor (Table 5)				1.0	
22.	Final score for groundwater pathways (multiply item	20 x	item	21)	100	

COMMENTS ON GROUNDWATER PATHWAYS

Known ground-water contamination

0 1 2 4 6 Contaminant: _____

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

CONTAM	MINANT HAZARD SURFACE WATER				
contam	ntaminants have been detected in surface water (score of 100 in item 1 minants have not been detected (score of 0 in item 1), complete items intaminants, as appropriate.), complete i 29 through 32	tems 23 thro . Attach Ba	ugh 28. If zard Worksheet	or list
		Score (circle	Result	Logarithm (base 10)	
23.	Sum of human health hazard quotients (from column 10 of Hazard Worksheet)	U	2.9x10 ⁷	7.5	
24.	Human health hazard score	0 1 2 4 (6)			
25.	Normalized human health hazard score (multiply item 24 x 100/6)		100		
25.	Sum of ecological hazard quotients (enter the larger of the sums of column 11 or 12 of Hazard Worksheet)		9.97	1.0	
27.	Ecological hazard score	0 1 2 3	50.0		
28.	Normalized ecological hazard score (multiply item 27 x 100/5)	4 3 0			
29.	Maximum human health hazard index	0 1 2 3 4 5 6 7 8 9	Contamin	ant:	
30.	Normalized human health hazard score (multiply item 29 x 100/9)				
31.	Maximum ecological hazard index	0 1 2 4 6	Contamin	ent:	
32.	Normalized ecological hazard score (multiply item 31 x 100/6)				
MATHCC	1INANT HAZARD GROUNDWATER				
nave r	ntaminants have been detected in groundwater (score of 100 in item 13) not been detected (score of 0 in item 13), complete items 39 through 4 minants, as appropriate.	•	zard Workshe	et or list of	e minants
33.	Sum of human health hazard quotients (from column 10 of Hazard Worksheet)		1.2x10 ¹¹	11.1	
34,	Human health hazard score	0 1 2 4 6			
35,	Normalized human health hazard score (multiply item 34 x 100/6)		100		
36.	Sum of ecological hazard quotients (enter the larger of the sums of column 11 or 12 of Hazard Worksheet)		293.9	2.5	
37.	Ecological hazard score	0 1 2 3 4 3 6			
38.	Normalized ecological hazard score (multiply item 37 x 100/6)	7 <i>0</i> °	83.3		
39.	Maximum human health hazard index	0 1 2 3 4 5 6 7 8 9	Contamin	ant:	
-3	Sormalized human health hazard score (multiply item 39 x 100/9)				

41. Maximum ecological hazard index

~2. Normalized ecological hazard score (multiply item 41 x 100/6)

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

N HEALTH RECEPTORS SURFACE WATER PATHWAY	Score (circle one)	Multiplier	Product Max. (score x score mult.)
Population that obtains drinking water from potentially affected surface water body(ies) within 3 miles (4.8 km) downstream	0 1 2(3)	3	9 9
Water use of nearest surface water body(ies)	0 1 2 3	3	9 9
Population within 1000 ft (305 m) of the site	0 1 2 3	1	3 3
Distance to the nearest installation boundary	0 1 2 (3)	1	3 3
Land use and/or zoning within 1 mile (1.6 km) of the site	0128)	1	<u>3</u> 3
Sum of items 43 through 47			27 27
Final score for human health receptors on surface water pathways (multiply item $48 \times 100/27$)		100	
OGICAL RECEPTORS SURFACE WATER PATHWAYS			
Importance/sensitivity of biota/habitats in potentially affected surface water bodies nearest the site	0 1 (2 3	5	10 15
	(i) 3	1	<u>0</u> 3
Presence of "critical environments" within 1 mile (1.6 km) of the site	•		
	·		10 18

COMMENTS ON SURFACE WATER RECEPTORS

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

HUMAN HEA	LTE RECEPTORS GROUNDWATER PATHWAY	Score (circle one)	Multiplier	Product Max. (score x score mult.)
54.	Estimated mean groundwater travel time from current waste location to nearest downgradient water supply well(s)	0)123	9	
55.	Estimated mean groundwater travel time from current waste location to any downgradient surface water body that supplies water for domestic use or for food chain agriculture	0 1(2)3	5	10 15
5 6 .	Groundwater use of the uppermost aquifer	0 1(2)3	4	8 12
57.	Population potentially at risk from groundwater contamination	0 6 9 12 18 24 27 36	1	27 36
58.	Population within 1000 ft (305 m) of the site	0 1 2 (6)	1	<u>3</u> 3
59.	Distance to the nearest installation boundary	0 1 2 (3)	1	_33
60.	Sum of items 54 through 59			51 96
61.	Final score for human health receptors on groundwater pathways (multiply item 60 x $100/96$)			53.1
ECOLOGICA	L RECEPTORS GROUNDWATER PATHWAYS			
62.	Estimated mean groundwater travel time from current waste location to any downgradient habitat or natural area	0 1 2 3	3	<u>6</u> 9
63.	Importance/sensitivity of downgradient biota/habitats that are confirmed or suspected groundwater discharge points	0 1 🕄 3	3	<u>6</u> 9
64.	Presence of "critical environments" within 1 mile (1.6 km) of the site	6) 3	1	<u>0</u> 3
65.	Sum of items 52 through 64			12 21
66.	Final score for ecological receptors on groundwater pathways (multiply item 65 x 100/21)			57.1

COMMENTS ON GROUNDWATER RECEPTORS (attach additional pages if needed)

- 54. No downgradient wells.
- 55. Travel time 0.2 ft/day. 1,000 ft to surface water. 13.9 days.

Site identification: Flightline Area (Sites LF04, LF05, WP07 and FT09)

SCORING SUMMARY SHEET

		<u>Pat</u>	thways scor	<u>•</u>	Contaminant hazard score		Receptors score		Overall score
67.	Surface water/humam health scores	(100 1tem 12	x	100 item 25/30	x	100)	/10.000 =	_100
6 8 .	Surface water/ecological scores	(100 item 12	x	50 item 28/32	x	55_6) 1tem 53	/10,000 =	27_8
69.	Groundwater/human health scores	(100 item 22	x	100 item 35/40	x		/10.000 =	53_1
70.	Groundwater/ecological scores	(100	x	83.3 item 38/42	x	57.1)	/10,000 =	47.6

OVERALL SITE SCORE:

71.
$$(\frac{100}{1 \tan 67})^2 \times 5 + (\frac{27.8}{1 \tan 68})^2 + (\frac{53.1}{1 \tan 69})^2 \times 5 + (\frac{47.6}{1 \tan 70})^2 = \frac{67.13}{6.65}$$

72. Overall site score =
$$67,136.653.464 = 19,381.25$$

FLIGHT LINE AREA -- GROUND WATER

CONT. CONC. HEALT NAME (UG/L) BMAR	CONC. (UG/L)		H AQUATIC < BMARK		BIOACC BMARK	TERRE BIOACC W INTAKE F INTAKE TOTAL BMARK BMARK (UG/DAY) (UG/DAY) INTAKE	F INTAKE (UG/DAY)	TOTAL	HEALTH QUOTIEN		TERRE HAZ QUOTIENT
TETRACHLOROETH	30000		5280		44	00009	8580	5.1E+08	5.1E+08 1.3E+08		**************************************
TRICHLOROETHEN	4400000	42	45000	0	17	8800000	486200	4.28E+12	1.02E+11		0
VINYL CHLORIDE	170000	1000	381000	0	7.2	340000	7956	2.71E+09	2705040	0.446194	0
CIS-1,2-DCE	730000	2.6	135000	2.0E+08	7.2	1460000	34164	4.99E+10	1.92E+10	5.407407	0
ARSENIC	53		360	100	280	106	96.46	10224.76	255619	0.147222	0.53
CHROMIUM	200	0.016	16	100	200	400	260	104000	6500000	12.5	8
IRON	61000	150	400	2000	100	122000	39650	4.84E+09	32248666	152.5	12.2
LEAD	90	100	34	2000	300	180	175.5	31590	315.9	2.647058	0.018
MANGANESE	2000	0.25	320	200	400	10000	13000	1.3E+08	5.2E+08	14.28571	25
MERCURY	6.2	0.4	2.4	0	63000	12.4	2538.9	31482.36	78705.9	2.583333	0
11 11 11 11 11 11 11 11 11 11 11 11 11			Ħ				Ĥ		M 64 11 81 11 14		
								TOTALS	1.22E+11	293.9765	39.748

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FINAL PAGE

ADMINISTRATIVE RECORD

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ADMINISTRATIVE RECORD

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